

Pronghorn enhancements for MSR applications

ART-MSR Review Meeting

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Mauricio Tano, Ramiro Freile, Mengnan Li, Victor Coppe Leite, Peter German, David Reger,
Guillaume Guidicelli

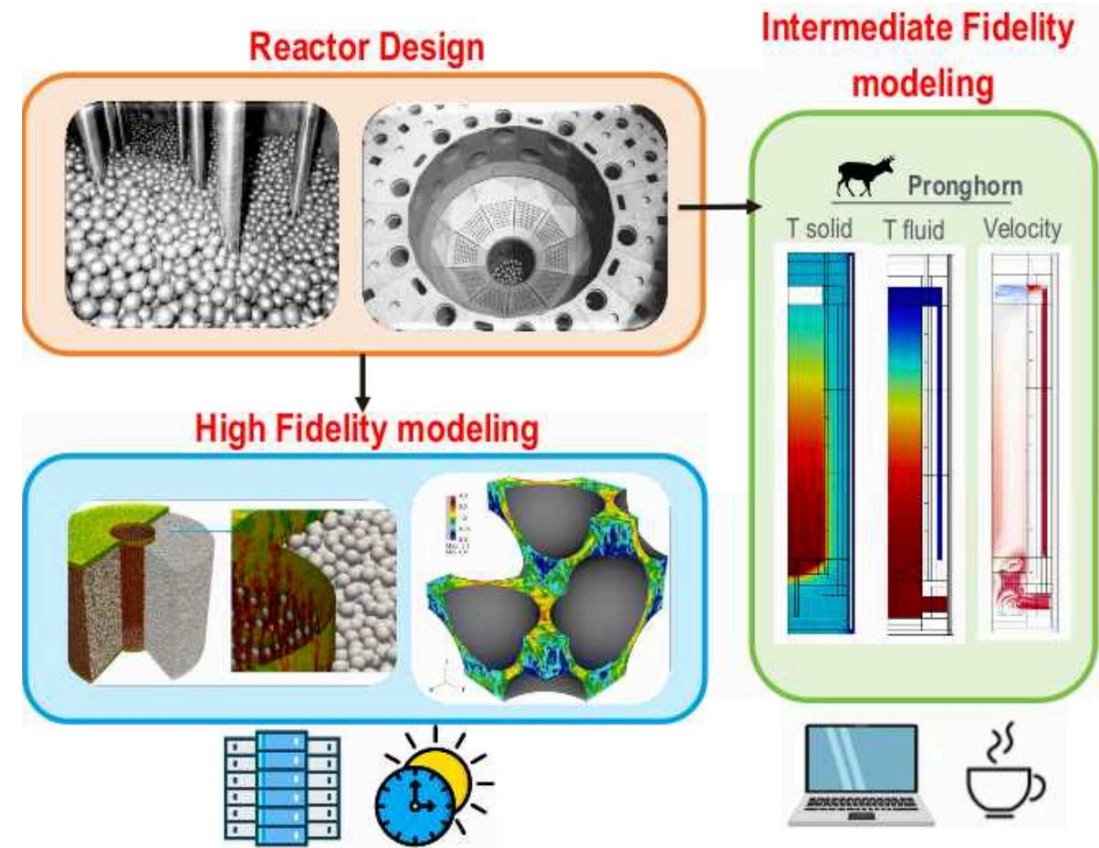


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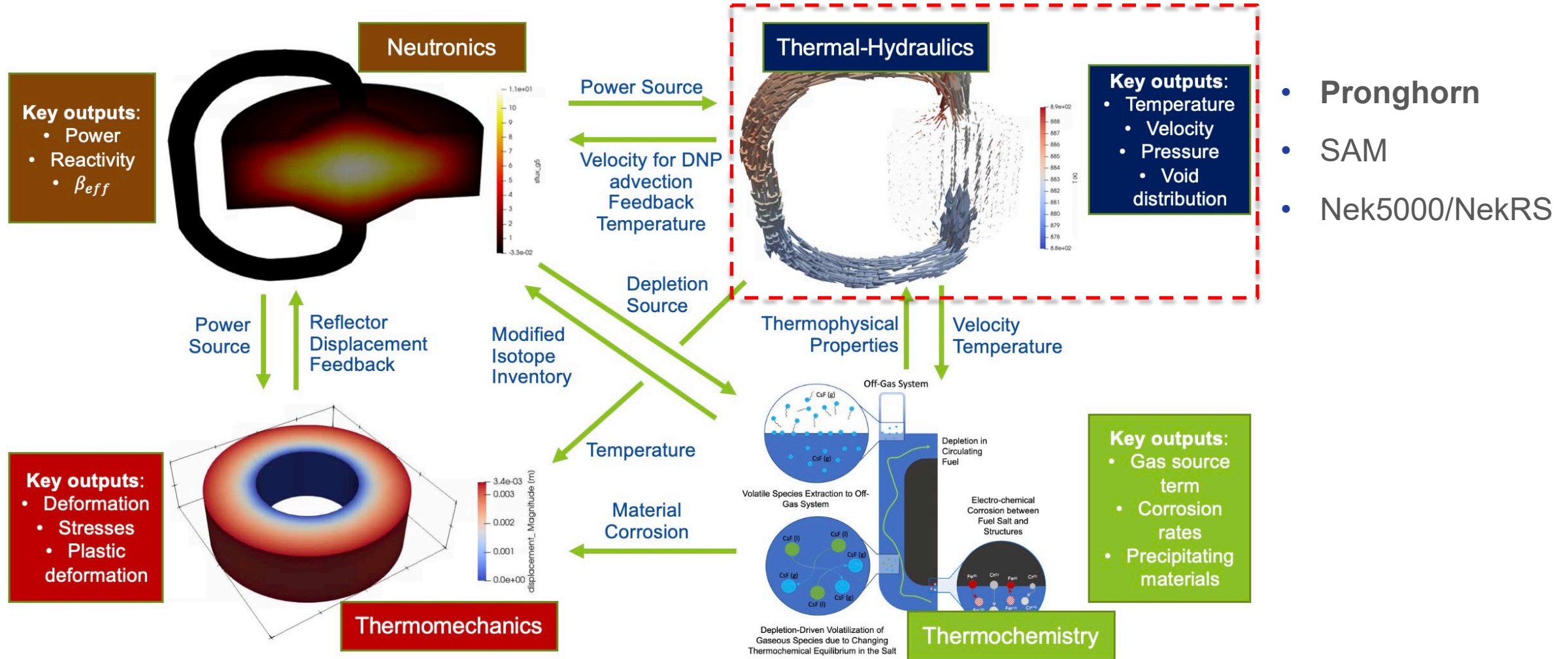
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Pronghorn

- **Pronghorn:** Intermediate-fidelity multidimensional coarse-mesh CFD code
- Capabilities:
 - Coarse-mesh CFD with finite volume discretization
 - Incompressible or weakly compressible flows
 - Porous flow modeling with a wide range of correlations
 - **RANS turbulence modeling with several turbulence models**
 - **Two-phase flow modeling**
 - Straightforward coupling to neutronics and other physics within the MOOSE framework
 - Level of resolution appropriate for full core modeling



Pronghorn's Role in MSR Multiphysics Framework



Key TH Improvements in Pronghorn for MSR Modeling

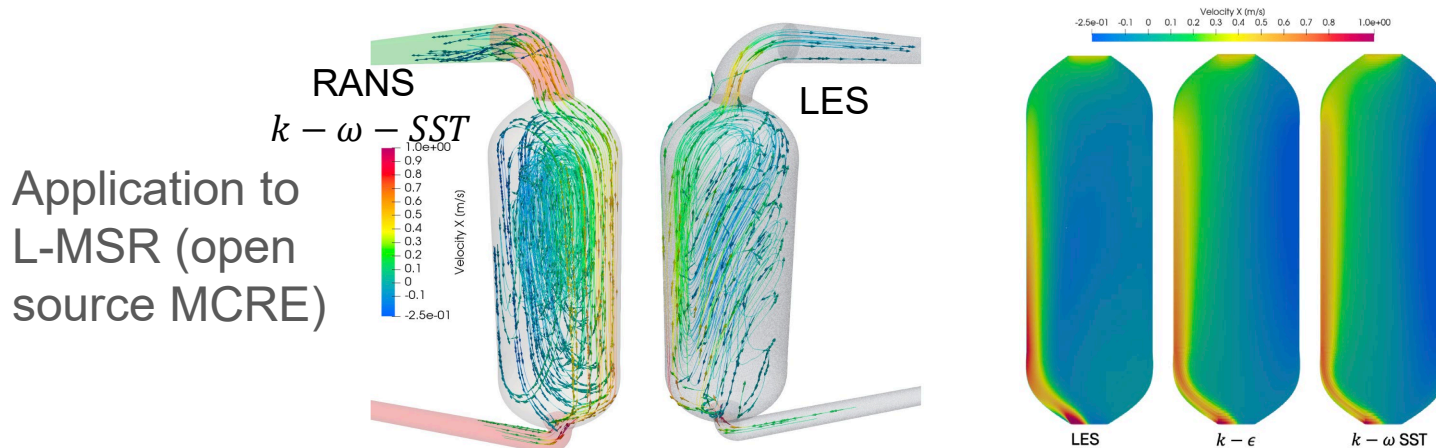
#	Issue Description	Solution
1	Two-equation RANS Turbulence Modeling: calibrating the mixing length model requires significant effort to reach high-accuracy solutions and is cumbersome for routine engineering applications	• State-of-the-art two-equation $k - \epsilon$ and $k - \omega - SST$ models with equilibrium and non-equilibrium wall treatment implemented and validated in MOOSE-NS • HOLO approach
2	Near-Wall Turbulence Modeling: inaccuracies are observed when comparing Pronghorn models with MCRE experiments due to roughness and curvature in walls	• Wall functions with curvature and roughness corrections implemented and validated in MOOSE • Adapted wall functions for corrosion profiles
3	Two-phase Flow Modeling: the effect of void fraction during routine multiphysics transients and accidental void entrainment, which are part of MSR design and safety bases, cannot be modeled	• Multi-D generalization of mixture drift-flux model developed and validated in MOOSE • Working prototype of multiphase Euler-Euler mixture
4	Pronghorn-SAM Coupling: for extended MSR support, Pronghorn-SAM coupling needs to be demonstrated for transients with weak-compressibility effects and flow reversal	• Domain overlapping action in BlueCRAB extended to deal with compressibility and Pronghorn code extended to deal with flow reversal



Two-equations RANS Turbulence Modeling

Model	Implementation	Near-wall Treatment	Corrections	Solvers Supported	Near-wall temperature modeling
$k - \epsilon$	Standard (Jones and Launder)	Two-layer stepwise treatment. Preferred high y^+	Durbin production limiting	Linear and Nonlinear	Yes
$k - \omega - SST$	Wilcox	Two-layer blended. Supports both low and high y^+	Free-shear, vortex-stretching, and low-Reynolds number modifications	Linear	Yes

- Models validated for:
 - Turbulent channel [1] $Re_\tau = 395$ and $Re_\tau = 590$
 - Backward Facing Step [2] $Re_h = 36,000$
 - Swirling Flow in a Bent Pipe [3] $Re = 50,000$
- Near-wall corrections for roughness and transverse curvature



	Number of elements	Pressure Drop [Pa]	
		$k - \epsilon$	$k - \omega$ SST
Coarse	~26K	3850	3950
Medium	~208K	3050	3100
Fine	~1664K	2815	2840

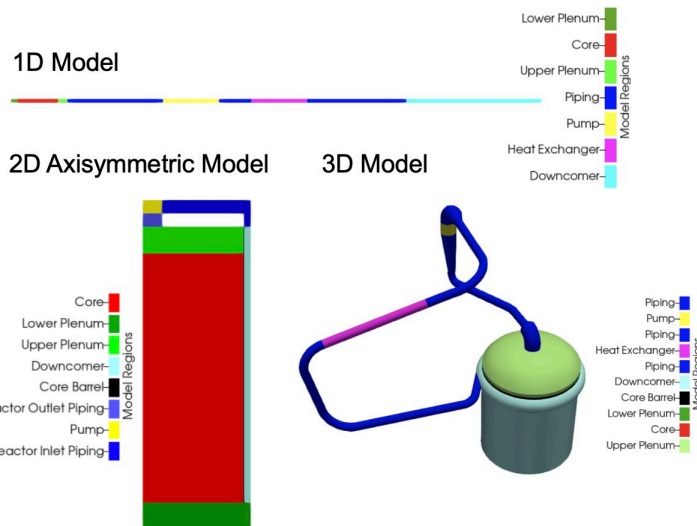
	LES	$k - \epsilon$	$k - \omega$ SST
Pressure Drop [Pa]	2780	2815 ± 135	2840 ± 136

- Mansour, N.N., Kim, J., Moin, P. (1988). Reynolds-stress and dissipation-rate budgets in a turbulent channel flow. J. Fluid Mech., Vol. 194, pp. 15-44
- Le, H., Moin, P., Kim, J. (1997). Direct numerical simulation of turbulent flow over a backward-facing step. J. Fluid Mech., Vol. 330, pp. 349-374.
- So, R.M.C., Anwer, M. (1993). Swirling turbulent flow through a curved pipe. Part 2: Recovery from swirl and bend curvature. Exp. Fluids, Vol. 14, pp. 169-177.

Two-Phase Flow Modeling

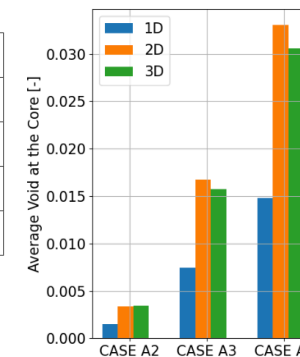
Model	Modifications	Solvers Supported	Compatible with wall functions
Drift flux model in porous media formulation	- Generalization to multi-D flows - Porous media support	Linear and Nonlinear	Yes

Application to MSRE



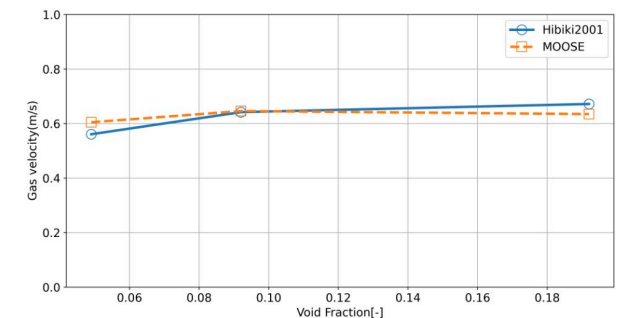
Model	Pressure Drop [kPa]	Effective Multiplication Factor
Expected	63.5 [86]	1.02132 [8]
1D Model	58.1	1.01739
2D axisymmetric Model	63.6	1.02223
3D Model	63.6	1.02211

Case / Reactivity Introduced [pcm]	1D Model	2D axisymmetric Model	3D Model
Case A1 - No void fraction (Reference Case)	-	-	-
Case A2 - Low Void Fraction	-6.2	-82.0	-56.0
Case A3 - Best-estimate Void Fraction	-30.8	-410.7	-263.6
Case A4 - High Void Fraction	-61.3	-824.1	-535.8

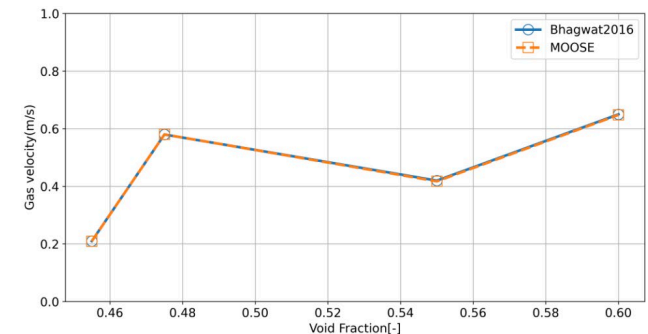


Models validated for:

- Vertical Air-Water Pipe [6] $\alpha \in [0.049, 0.192]$



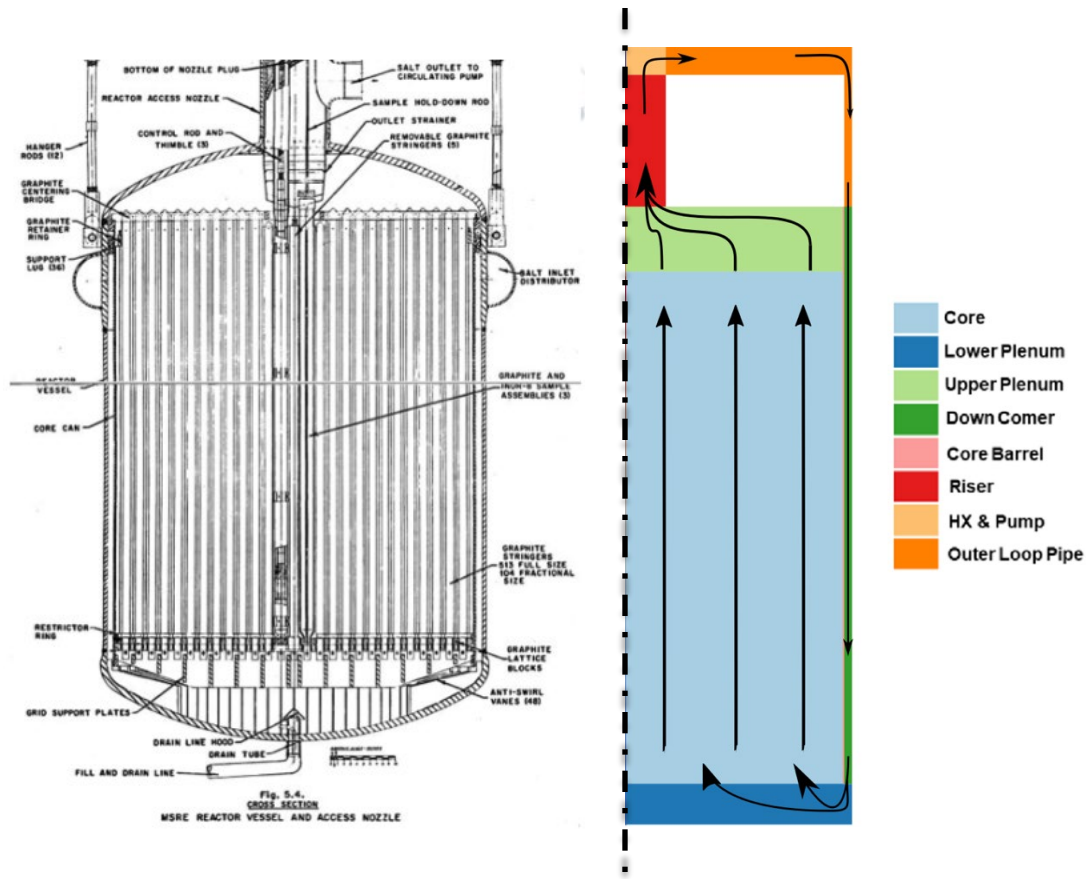
- Horizontal Air-Water Pipe [7] $\alpha \in [0.455, 0.600]$



6. Ishii, M., & Hibiki, T. (2010). *Thermo-fluid dynamics of two-phase flow*. Springer Science & Business Media.

7. Hibiki, T., Ishii, M., & Xiao, Z. (2001). Axial interfacial area transport of vertical bubbly flows. *International Journal of Heat and Mass Transfer*, 44(10), 1869-1888.

Multiphysics Validation for MSRE



MSRE core (left) [Robertson, 1965] and 2-D R-Z model (right)

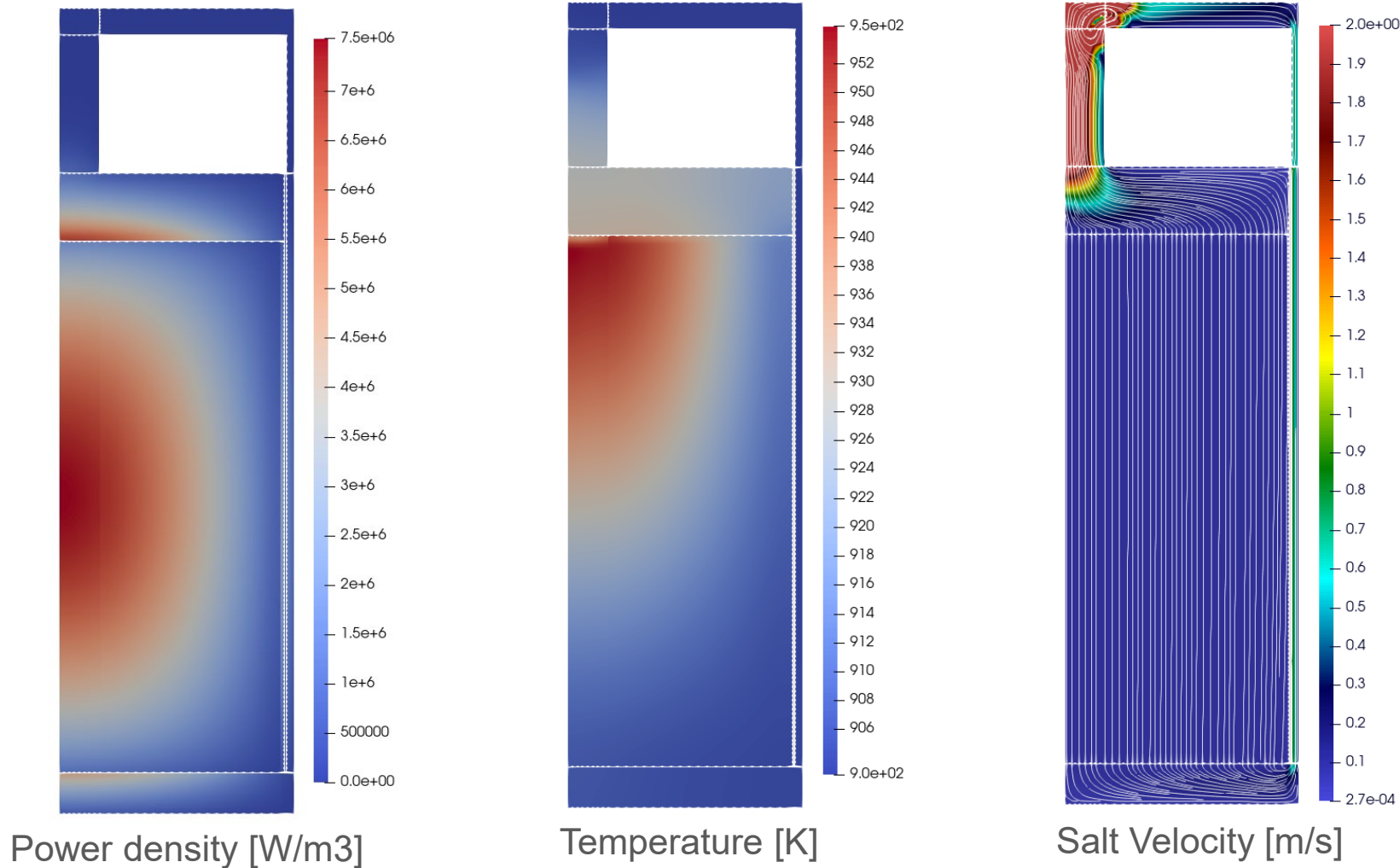
Isotope	²³⁵ U Fuel Loading	²³³ U Fuel Loading
Li-7	2.634E-01	2.618E-01
F-19	5.948E-01	5.936E-01
Be-9	1.179E-01	1.229E-01
U-233	–	4.977E-04
U-234	–	3.118E-05
U-235	1.203E-03	3.778E-06
U-238	2.443E-03	1.069E-06
Zr-90	1.042E-02	1.085E-02
Zr-91	2.273E-03	2.366E-03
Zr-92	3.474E-03	3.616E-03
Zr-94	3.521E-03	3.665E-03
Zr-96	5.673E-04	5.904E-04

Relative isotopic atomic fractions during the ²³³U and ²³⁵U loads of MSRE

Parameter [Units]	Fuel Salt	Graphite
Density [kg/m ³]	2,263 – 0.478 (T[K] – 923.0)	1,860.0
Thermal Conductivity [W/(m.K)]	1.4	40.1
Specific Heat [J/(kg.K)]	1868.0	1757.3
Dynamic Viscosity [Pa.s]	0.008268	–

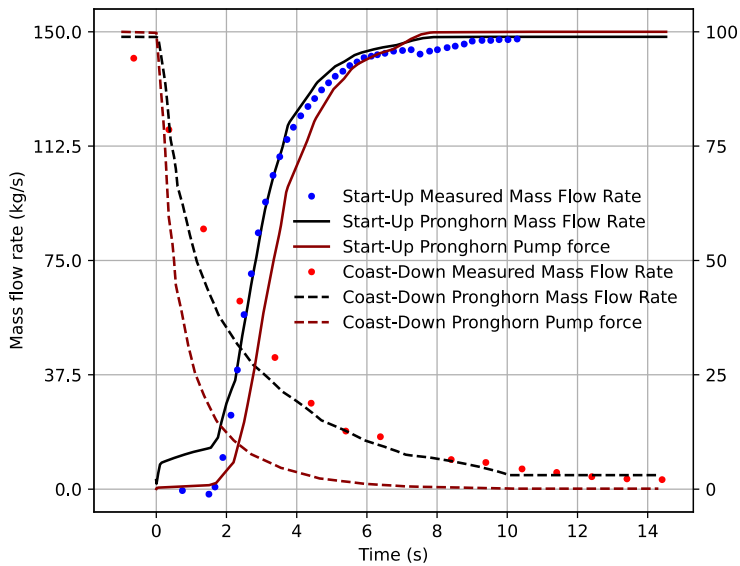
Thermophysical properties of the fuel salt and the moderator

Steady-State Fields

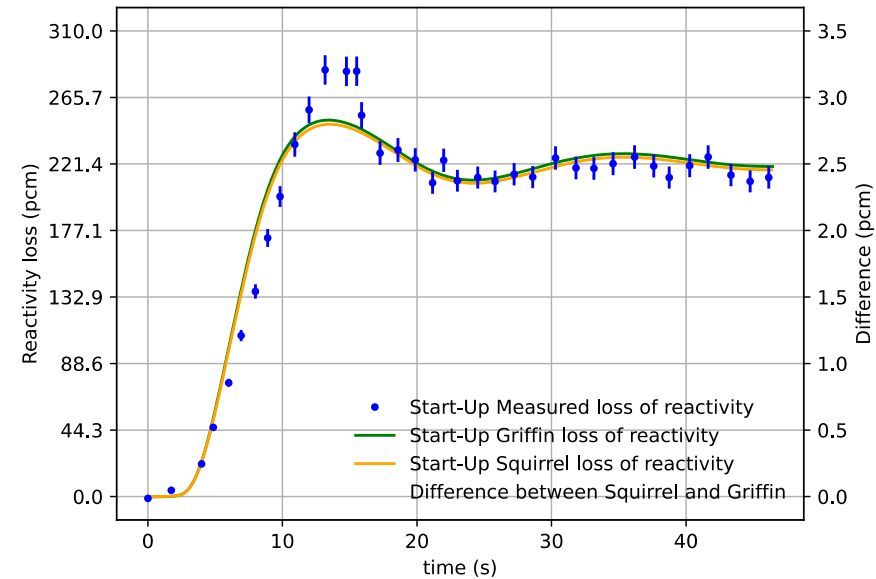


Takeaway: reasonable fields obtained for steady-state operation in Griffin-Pronghorn MSRE model

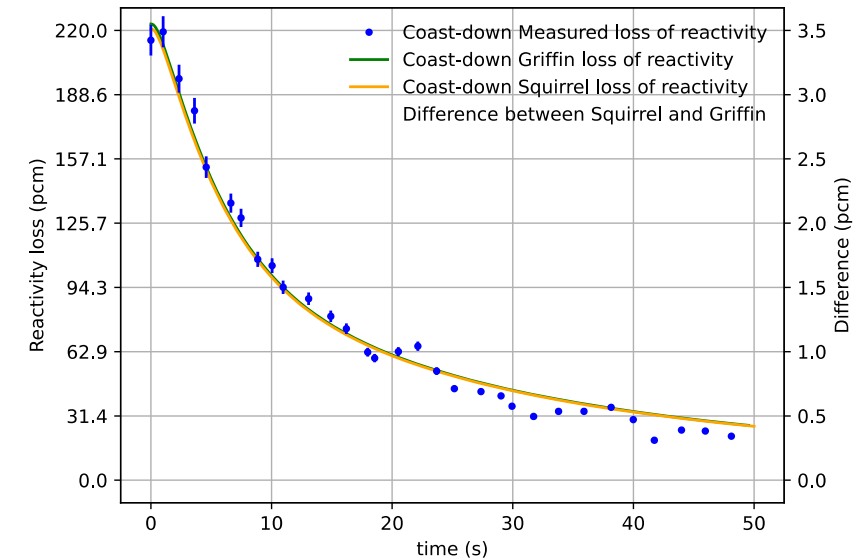
Pump Startup and Coast-Down Transients



Mass flow rate comparison during pump startup and coast-down [Prince et al., 1968]



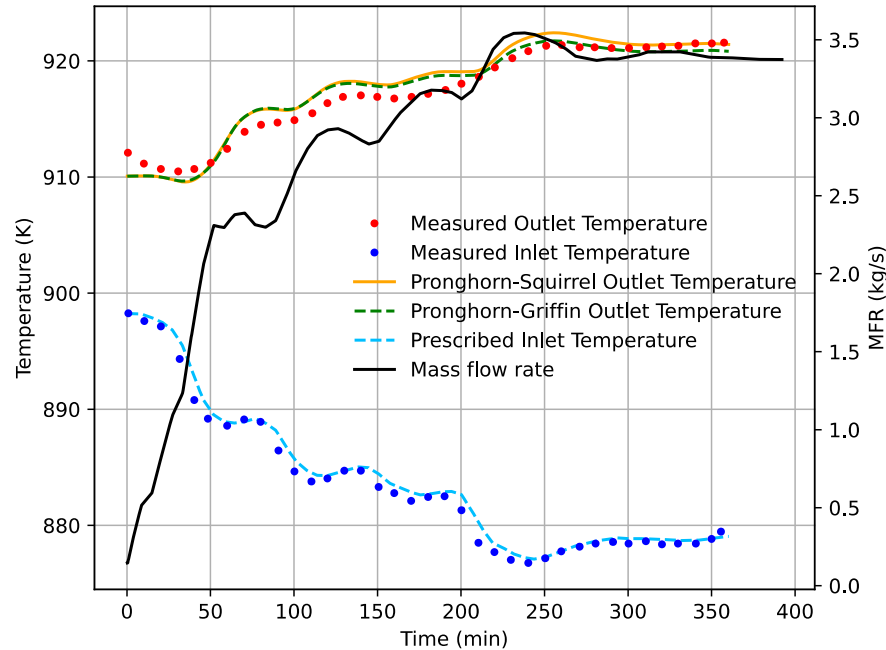
Comparison of reactivity loss during pump start-up transient [Prince et al., 1968]



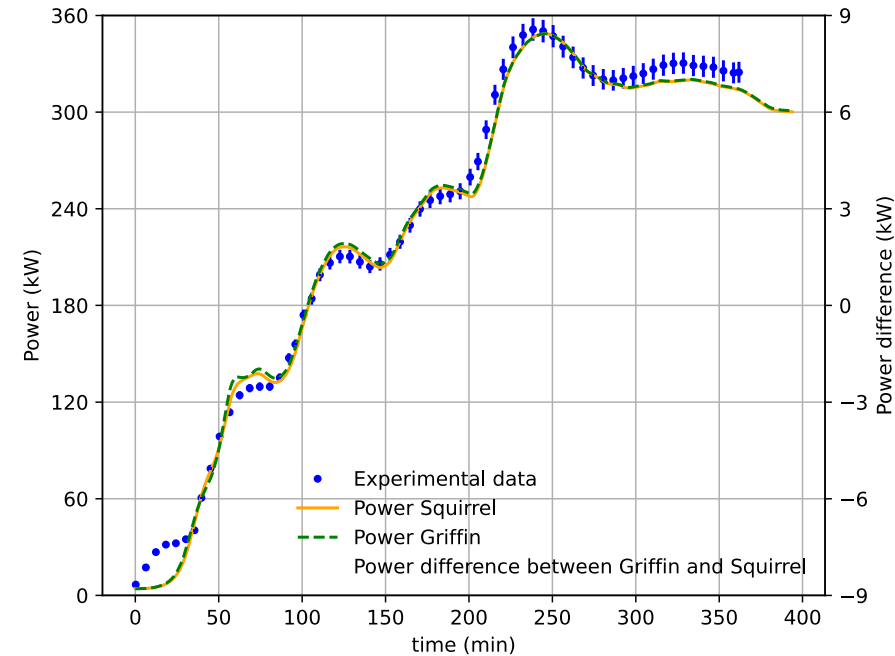
Comparison of reactivity loss during pump coast-down transient [Prince et al., 1968]

Takeaway: Griffin-Pronghorn MSRE multiphysics model validated for transient flow rate and zero-power pump start-up and shutdown

Natural Convection Transient



Mass flow rate and temperature evolution during the natural circulation test [Prince et al., 1968]



Reactor power evolution during the natural circulation test [Prince et al., 1968]

Takeaway: Griffin-Pronghorn MSRE multiphysics model validated for temperature and power evolution in transition to natural convection transient

Pronghorn-SAM Domain-Overlapping Coupling 1/2

- MOOSE Action developed to couple Pronghorn and SAM*
- The key principle is to automatically generate pipe components in SAM that represent the overlapped Pronghorn component and to match Pronghorn calculated values in SAM:
 - Match pressure drop → Friction factors set in SAM
 - Match enthalpy/temperature rise → heat source set in SAM
 - Adjust passive scalar concentration → volume source set in SAM
- The main components of the coupling action are
 - Geometric description of the coupled boundaries and their area and length
 - Boundary where Pronghorn pressure is pinned
 - Enthalpy function for temperature coupling
 - Passive scalar decay constants
 - Execution parameters, including solution method, coupling start time, and equations of state

Example of Domain Overlapping Coupling Action for MSRE

```
[OverlappingDomainCoupling]

### Coupled geometry
boundaries = 'downcomer_inlet pump_outlet'
component_names = 'downcomer core'
component_orientation = 'in out'
component_area = '0.1589 0.3512'
component_length = '1.8015 1.8015'
connected_component_names = 'pipe3_s2 pipe1_s1'
subapp_filename = 'MSRE_SAM_TH_v3.i'

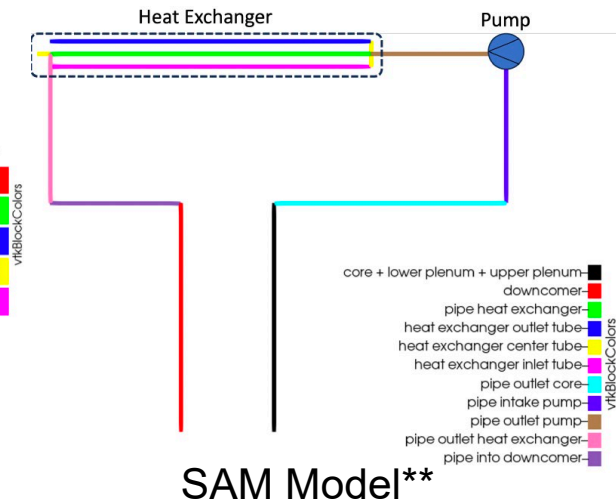
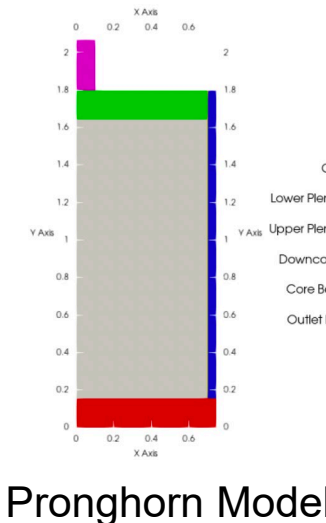
### Hydraulics coupling
pinned_pressure_value = pinned_pressure_top
pinned_pressure_boundary = 'pump_outlet'
initial_pinned_pressure = '${p_outlet}'
reference_pressure = reference_plane_pressure
reference_enthalpy = reference_plane_enthalpy

### Thermal coupling
enthalpy_function = cp_temp
boundary_temperature_names = 'T_downcomer T_core'
initial_boundary_temperatures = '${T_inlet} ${T_inlet}'
```

```
### Passive scalar coupling
passive_scalar_names = 'c1 c2 c3 c4 c5 c6'
system_level_passive_scalar_names = 'c1 c2 c3 c4 c5 c6'
boundary_passive_scalar_names = 'from_sam_ps_dc_c1 from_sam_ps_top_c1;
                                from_sam_ps_dc_c2 from_sam_ps_top_c2;
                                from_sam_ps_dc_c3 from_sam_ps_top_c3;
                                from_sam_ps_dc_c4 from_sam_ps_top_c4;
                                from_sam_ps_dc_c5 from_sam_ps_top_c5;
                                from_sam_ps_dc_c6 from_sam_ps_top_c6'
passive_scalar_decay_constant = '${lambda1_m} ${lambda2_m} ${lambda3_m};
                                ${lambda4_m} ${lambda5_m} ${lambda6_m}'
initial_boundary_passive_scalar_value = '0 0; 0 0; 0 0; 0 0; 0 0; 0 0'
passive_scalar_iteration_type = simple

### Execution
hydrodynamic_iteration_type = simple
thermal_iteration_type = simple
passive_scalar_iteration_type = simple
startup_time = 0.5
eos = fuel_salt_eos
execute_multiapp_on = 'TIMESTEP_BEGIN'
```

MSRE Model



SAM Model**

*) Schunert, S., Tano, M. E., & Mohammad Jaradat, M. K. (2023). *Overlapping Domain Coupling of Multidimensional and System Codes in NEAMS-Pronghorn and SAM* (No. INL/RPT-23-72874-Rev000). Idaho National Laboratory (INL), Idaho Falls, ID (United States).

**) Model developed by Jun Fang and Tingzhou Fei (ANL)



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Pronghorn-SAM Domain-Overlapping Coupling 2/2

- Demonstration:

- Pronghorn-SAM coupling demonstrated for MSRE
- For steady-state operation, the coupling methodology has been demonstrated and verified for the full reactor model.

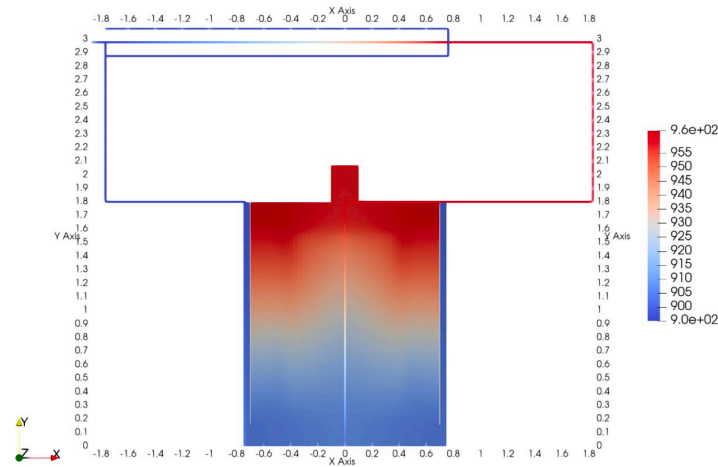
- Key limitation:

- 1D to multiD boundary condition in Pronghorn imposed from SAM models where flow assumptions must be made.
- The user must still carefully select the boundary where the coupling is performed to avoid the effects of these boundary conditions.

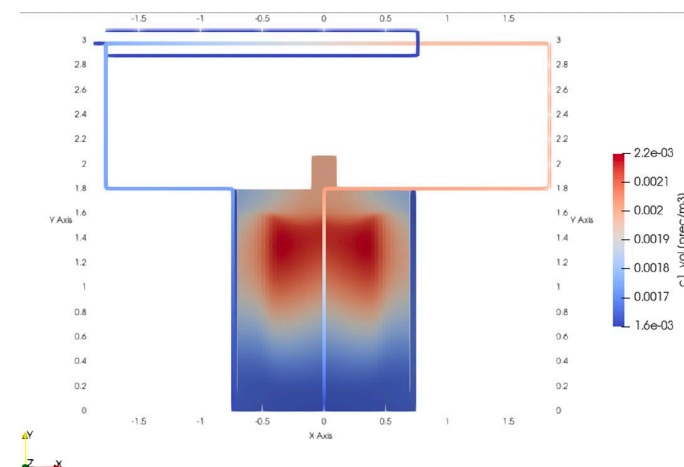
- Coupling validation:

- The transient model has been validated for reactivity insertion transients in MSRE.
- Pronghorn SAM results showed improved performance due to the higher resolution of the Pronghorn model.

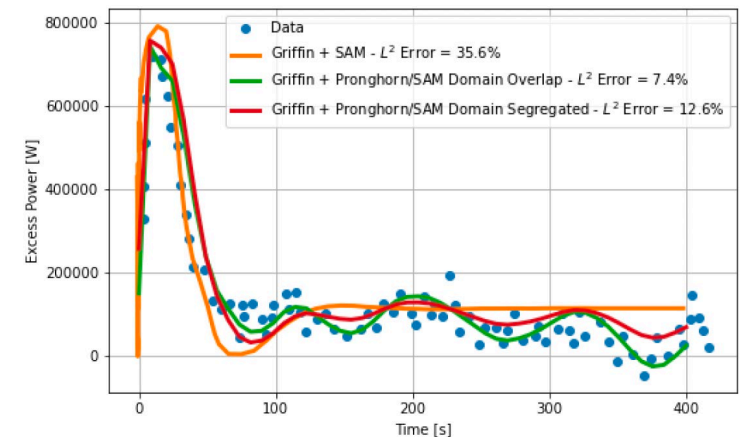
Temperature Field



Delayed neutron precursor concentration for group 1 ($\lambda_1 = 1.3336 \times 10^{-2} 1/s$)

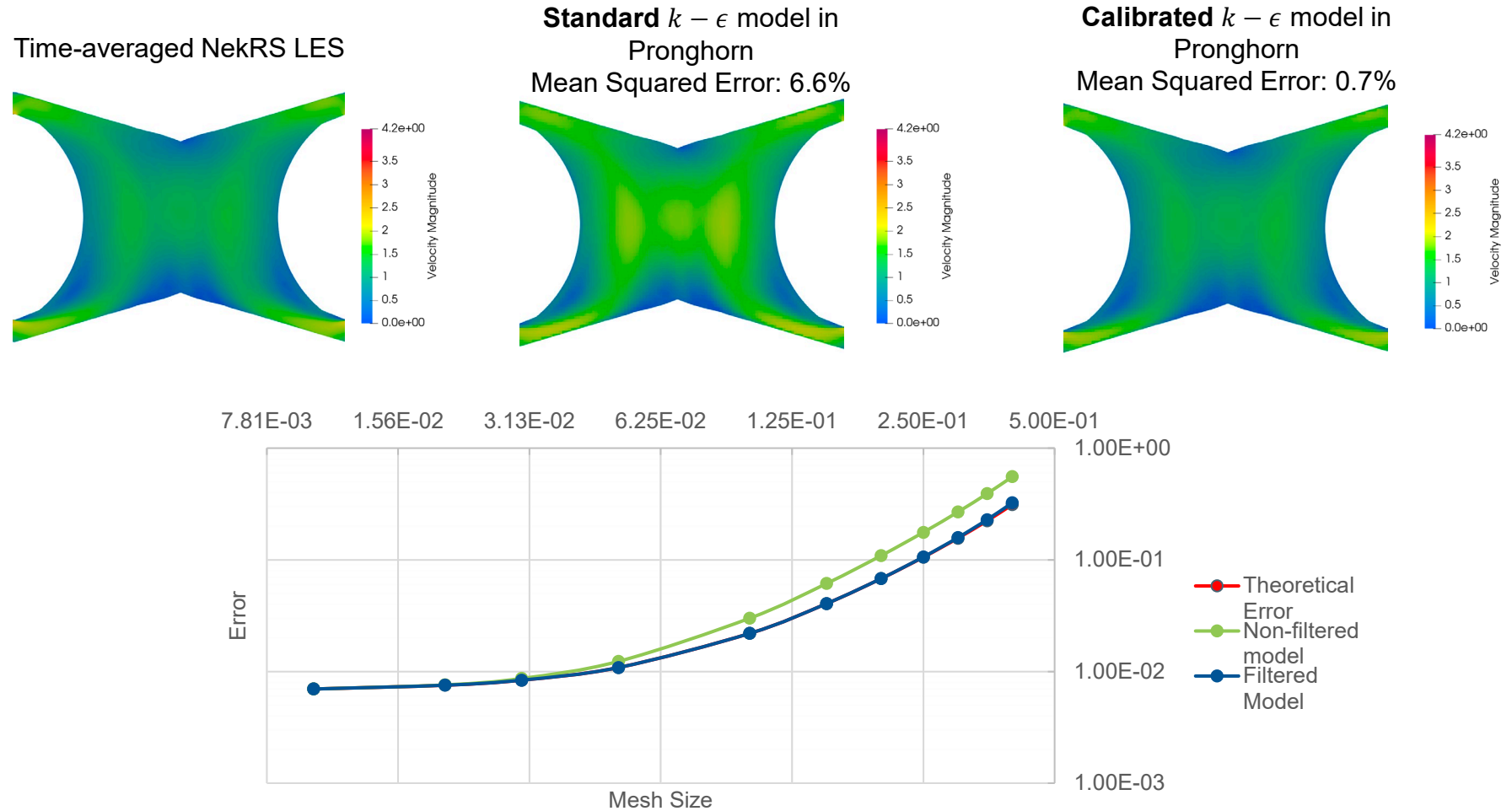


Reactivity Insertion Transient at 5MW of thermal power



Pronghorn-Nek High-to-Low (HOLo) Coupling

- Pronghorn RANS turbulent closures implemented as *Functors*, which allows for a simple calibration from higher-fidelity models
- Pronghorn implements an inverse Kalman filter for advection, allowing to obtain good performance advection in coarse meshes
- Example for the Molten Salt Fast Reactor (MSFR) core in the right figures



Summary

- Pronghorn has been extended to model pool-like MSRMs with coarse-mesh for engineering-scale modeling
- Additions included:
 - Two-equations $k - \epsilon$ and $k - \omega - SST$ RANS turbulence models
 - Near wall modeling for rough walls and swirling flow
 - Two-phase, drift-flux, multi-dimensional modeling
 - Domain-overlapping coupling with SAM
- Current work is targeting:
 - Coupling with Saline for modeling molten salt flows with diverse composition due to varying burnup
 - Two-phase Euler-Euler modeling for accounting for sloshing and larger void fraction transport
 - Continue improving domain-overlapping for cases with large body forces, weak-compressibility, and porosity jumps
 - Validation (salt spill, corrosion modeling, etc.)
 - Coarser computational meshes



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