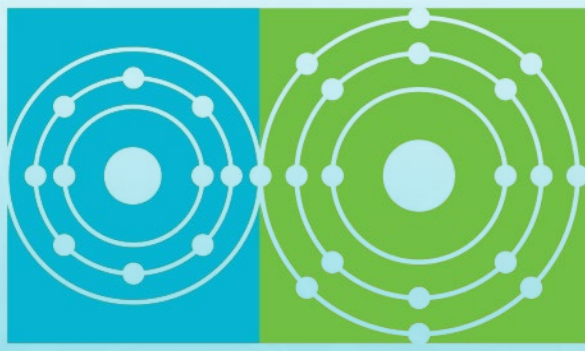




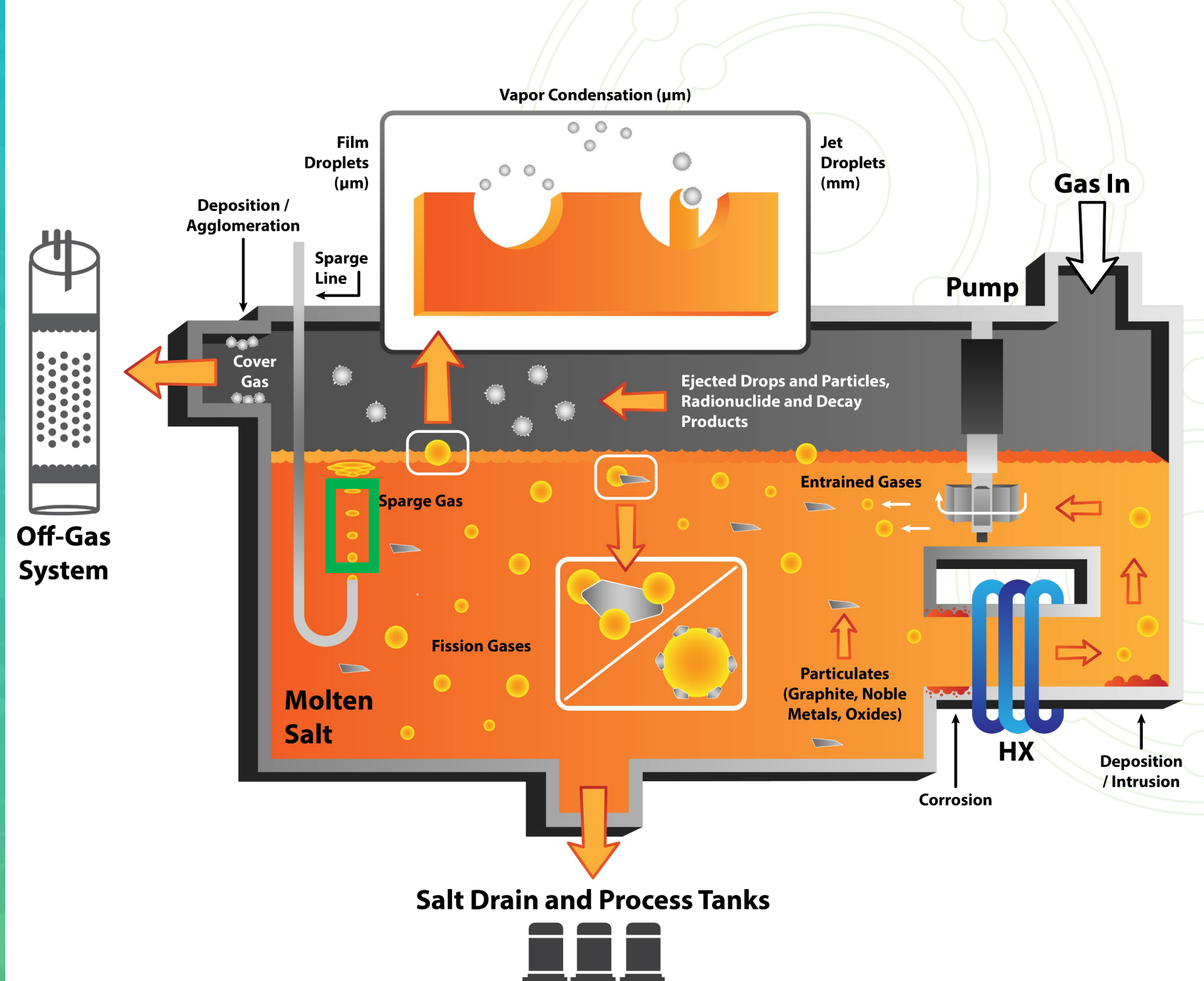
**Molten Salt Reactor**  
P R O G R A M

# Optical Measurements of Gas Bubble Rise Velocity and Aerosols in Molten Salt

Daniel Orea, Kevin Robb, Joanna McFarlane, Hunter Andrews, Zechariah Kitzhaber  
Oak Ridge National Laboratory

# MSR Gas and Particle Transport Phenomena

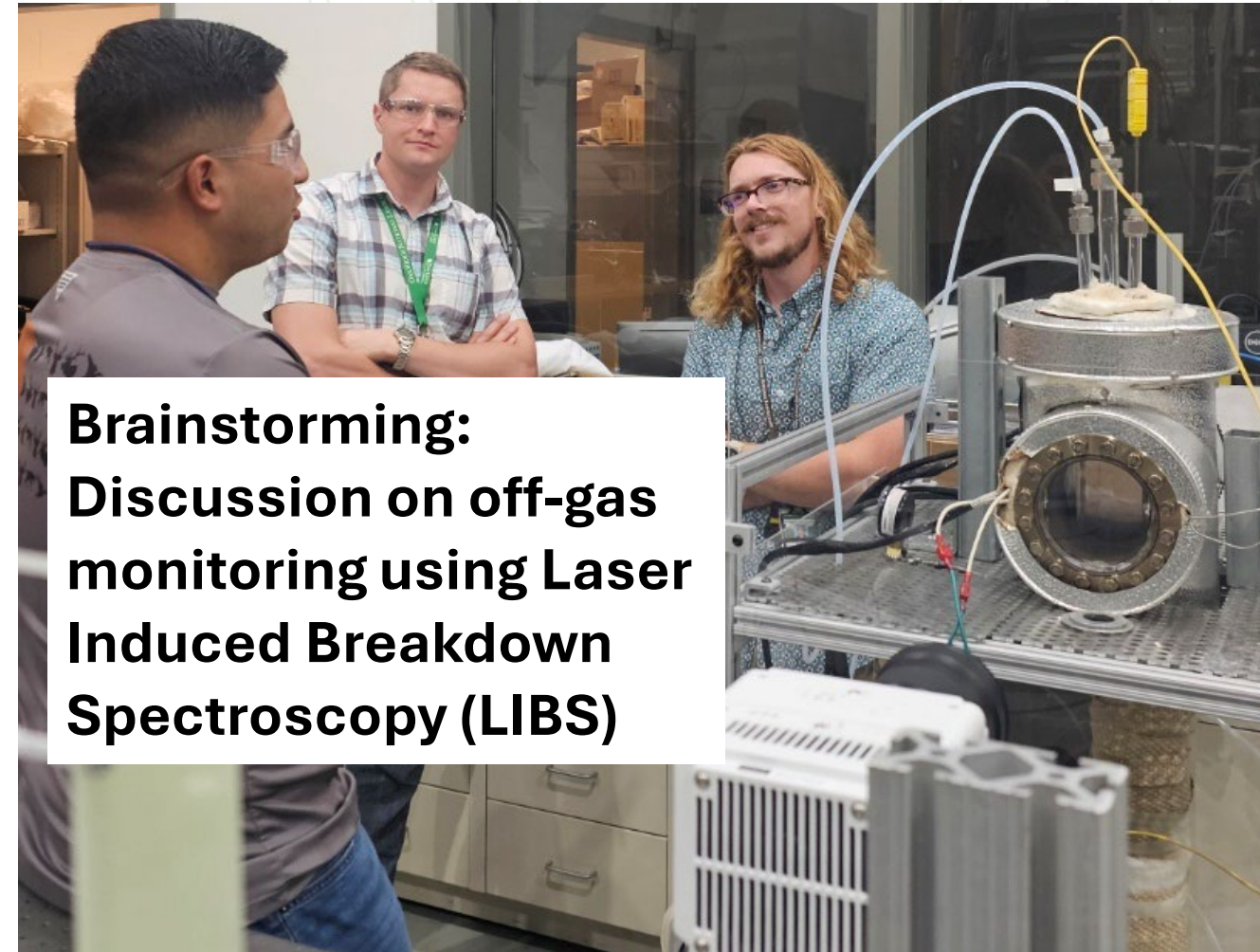
- The gas, particle behavior and gas-particle interactions are complex phenomena
- Experimental measurements in prototypic environments require careful planning





# Importance of Gas Transport

- Gas transport is important for the safe operation of MSR with regards to fission species transport and removal.
- The goal of the test series is to collect data on gas transport through molten salt, particularly, bubble size and rise velocity.
- Non-intrusive optical measurements deployed to visualize the salt.
- Data will be used for model development / validation of radionuclide transport, and to provide information for licensing requirements regarding MSRs.



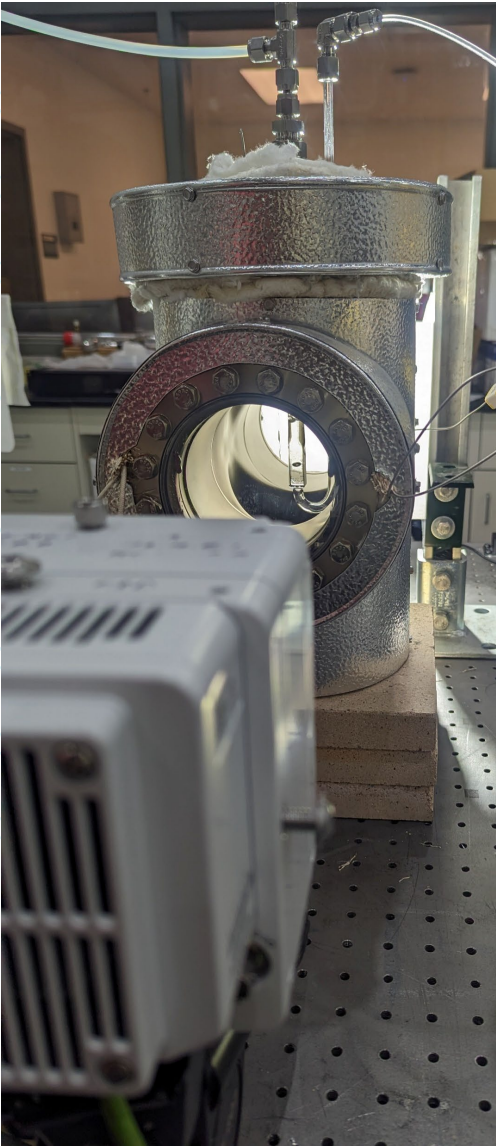
**Brainstorming:  
Discussion on off-gas  
monitoring using Laser  
Induced Breakdown  
Spectroscopy (LIBS)**

Left to Right) Daniel Orea, Zechariah Kitzhaber, Hunter Andrews



# Molten Salt Visualization Progress

Where we started



Flow Cell Improvements

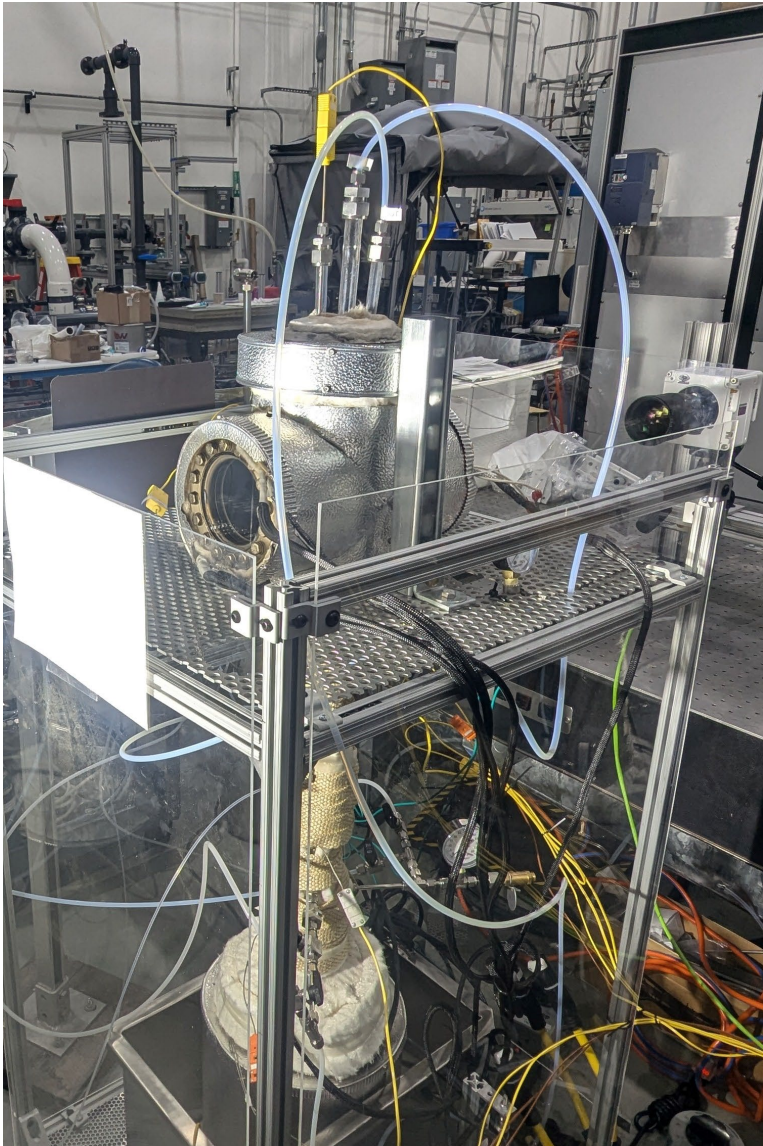


ORNL Scientific Glassblower: Carlos Rodriguez Flores

10 mL to 1,000 mL

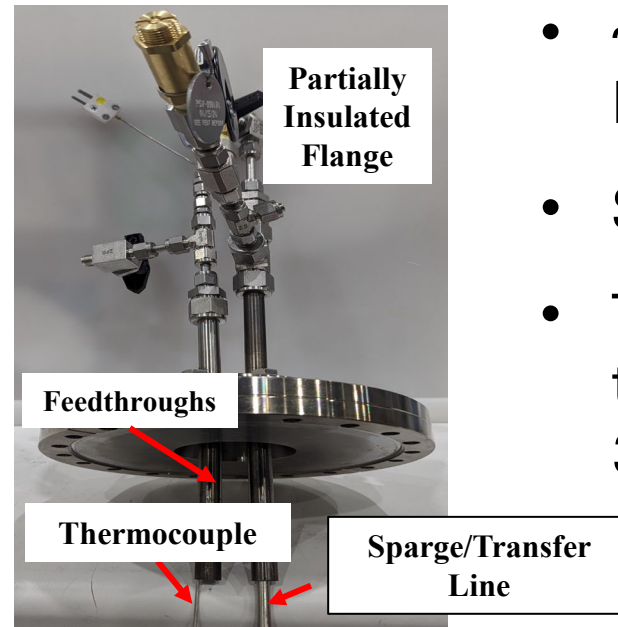


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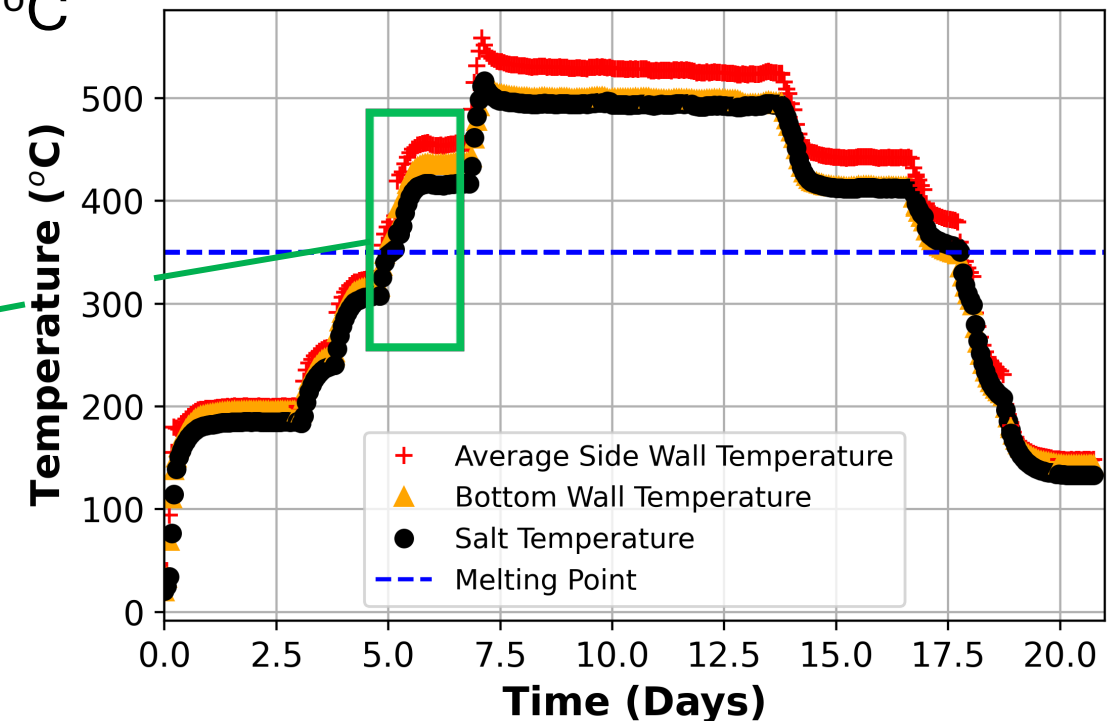
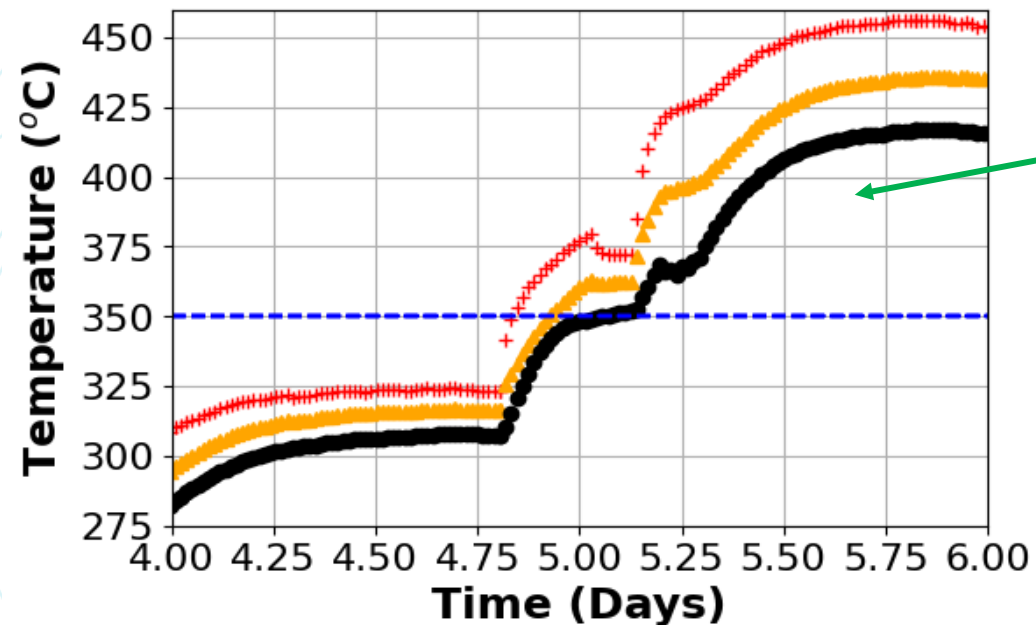




# Secondary Vessel Commissioning



- ~2 kg of molten salt was mixed inside a glove box
- Salt eutectic loaded into crucible and furnace
- Temperature measurements confirmed phase-transition at expected melting temperature of 350°C



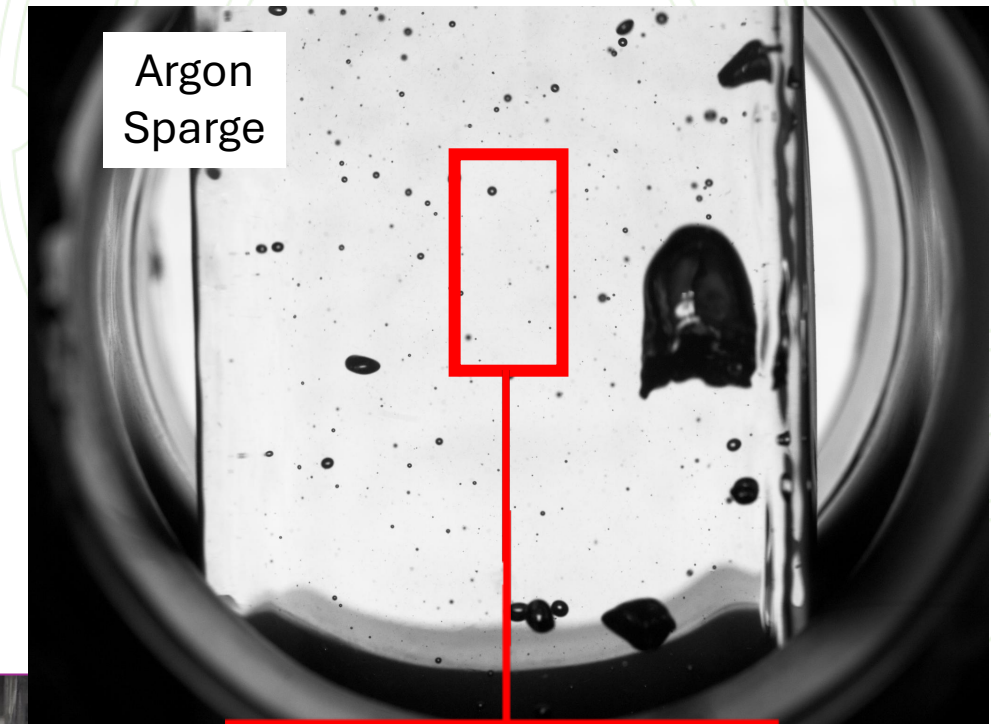
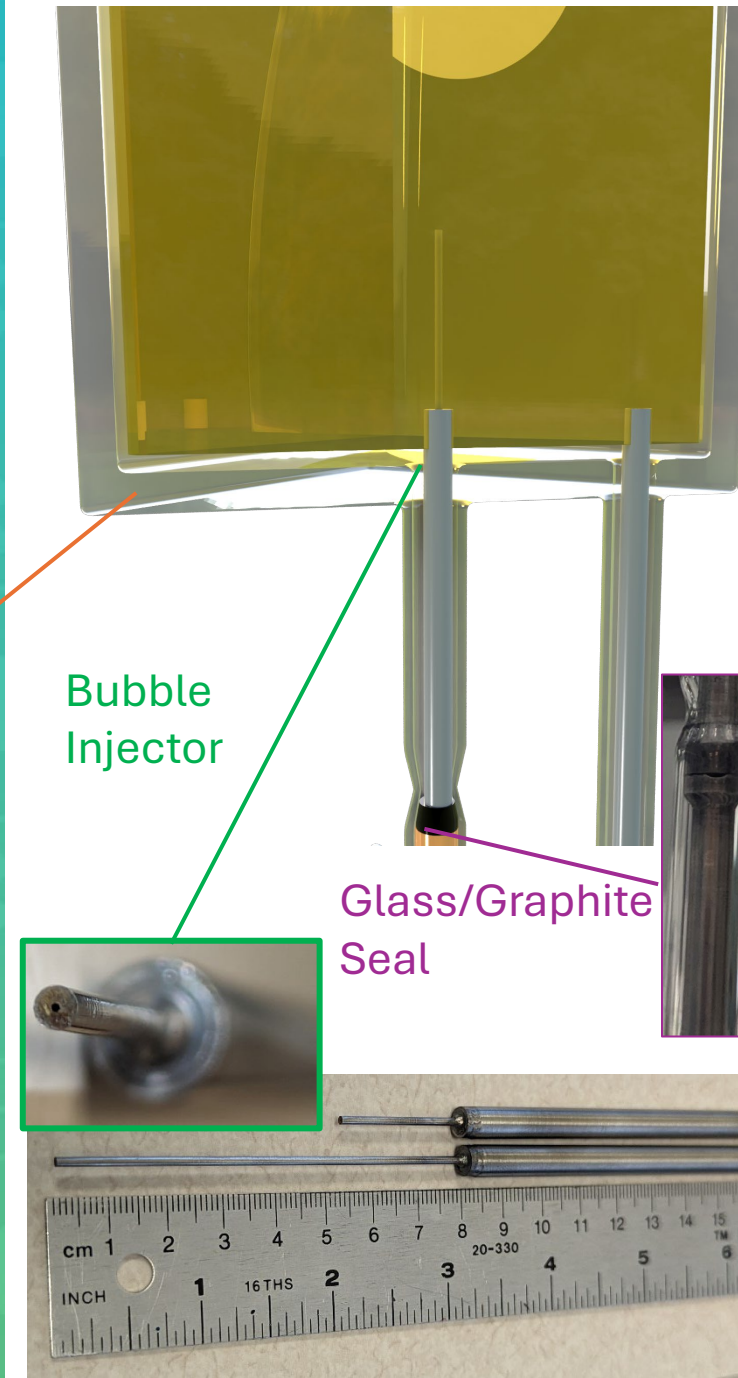
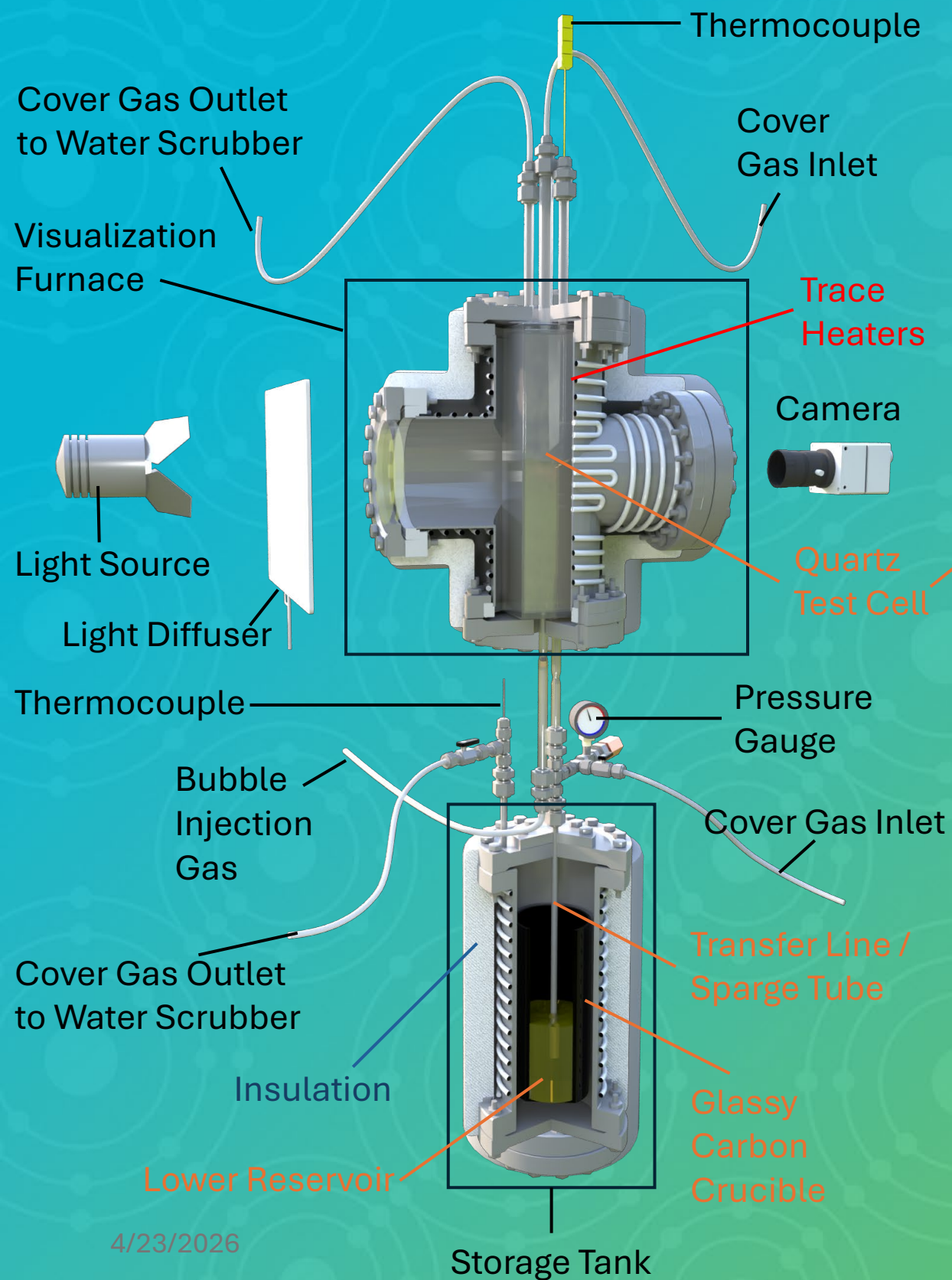
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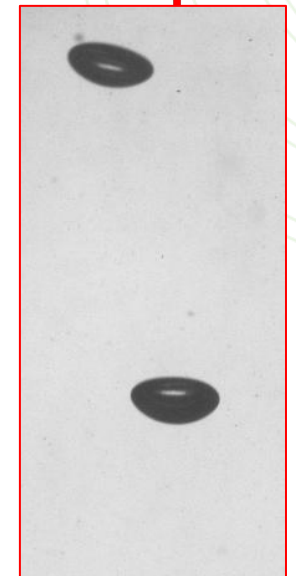
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Office of Nuclear Energy



# Molten Salt Visualization Apparatus



Argon Sparge



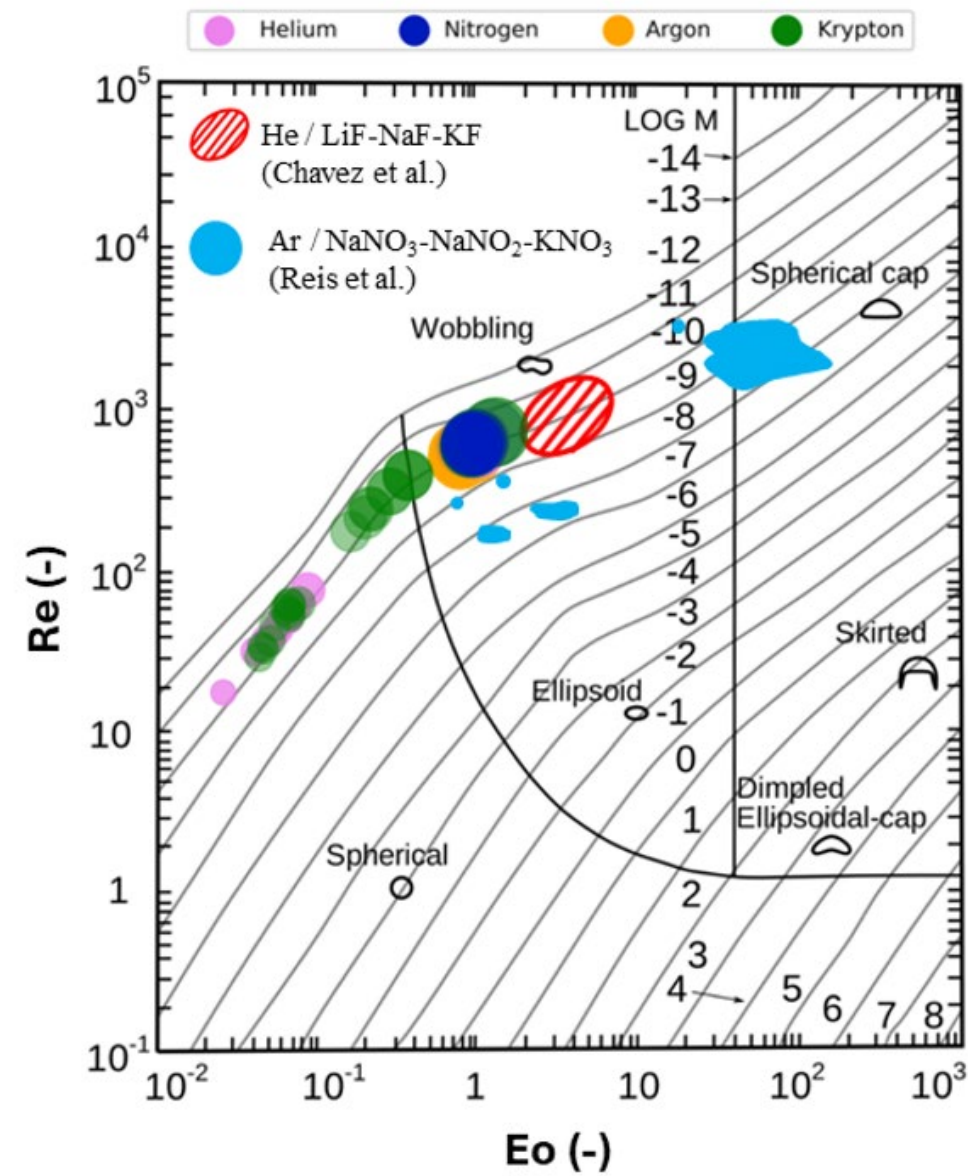
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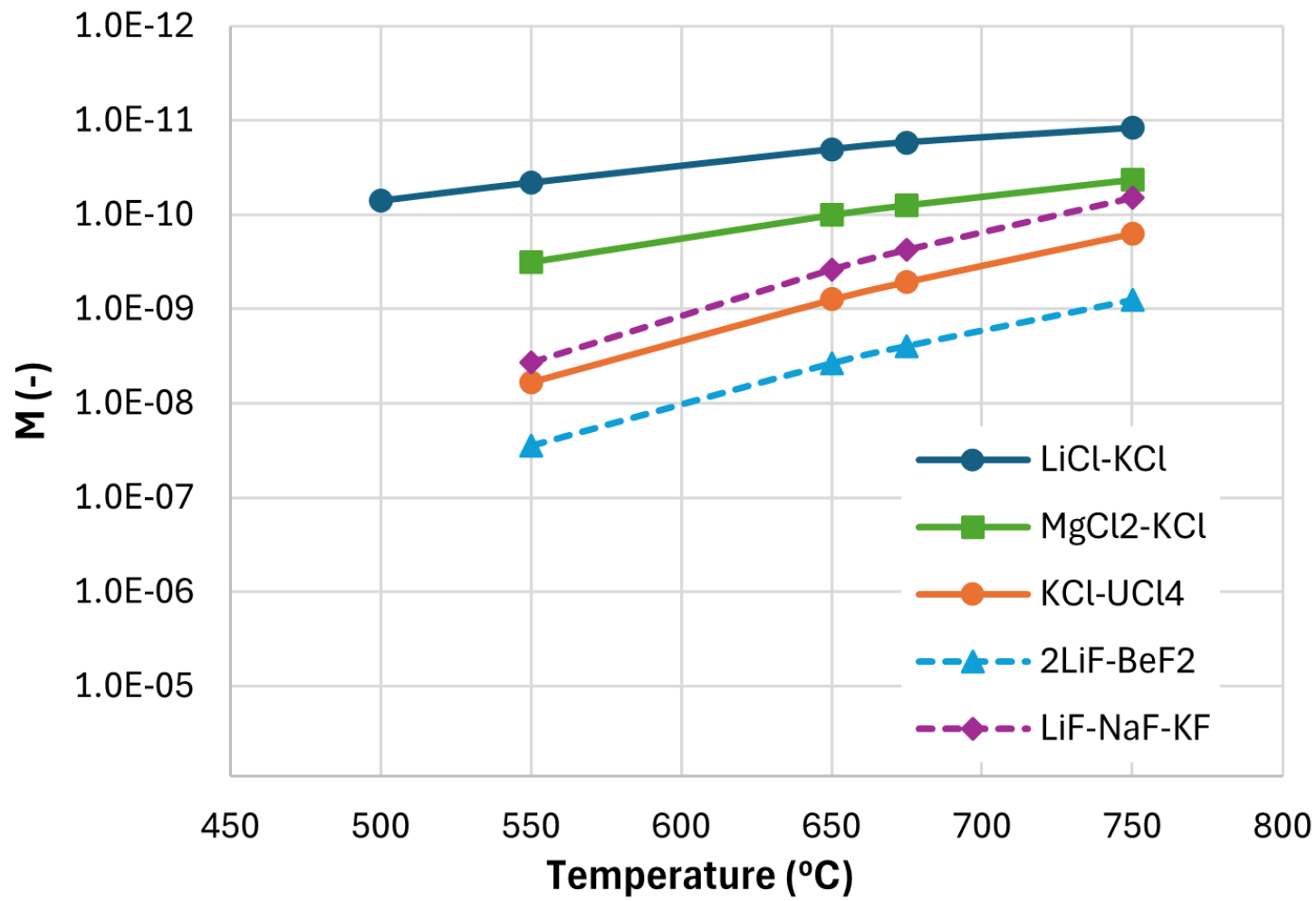
# Bubble Behavior in Molten Salt



$$Eo = \frac{\Delta \rho g D^2}{\sigma_l}$$

$$Re = \frac{\rho_l V D}{\mu_l}$$

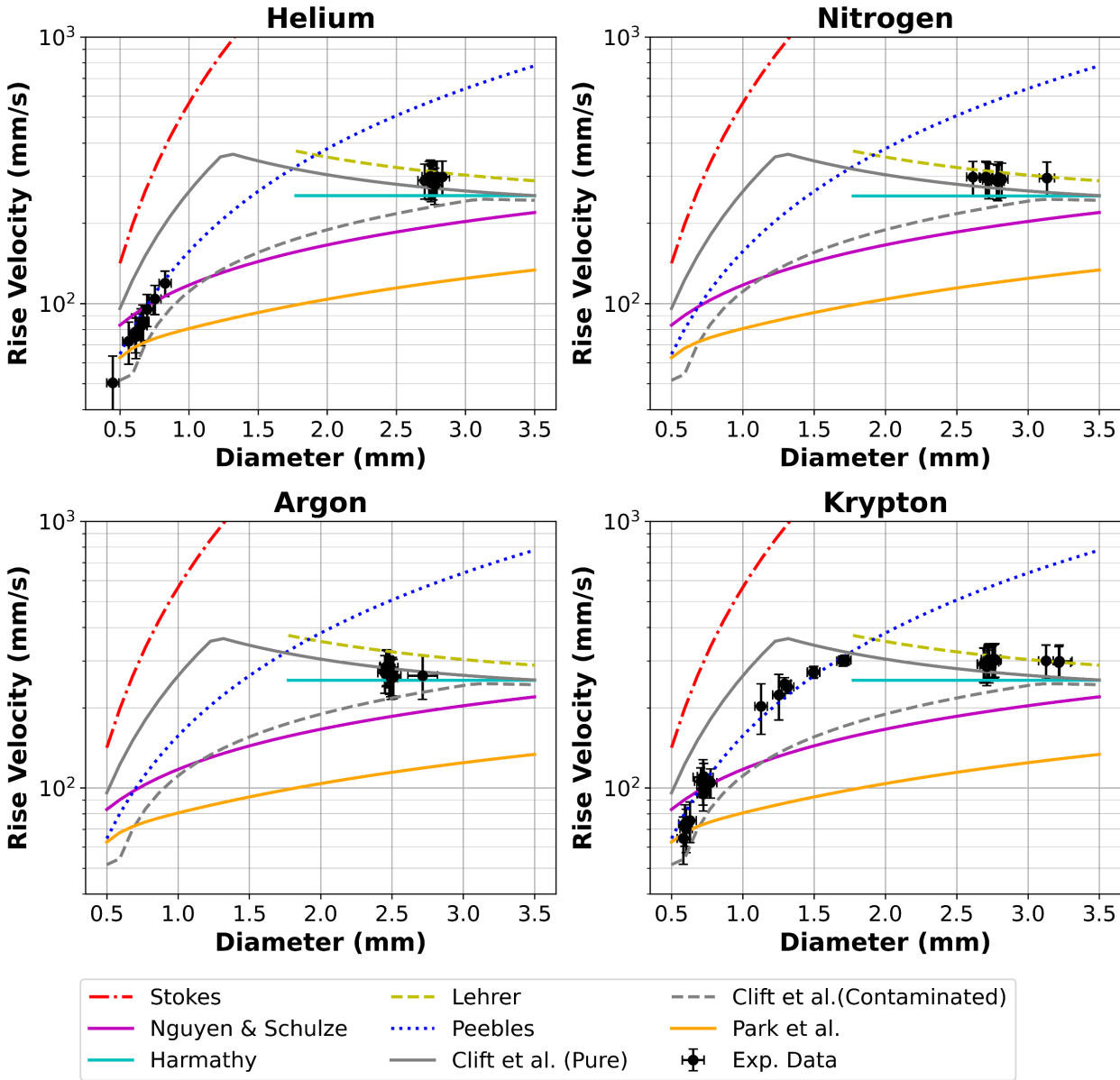
$$Mo = \frac{\Delta \rho g \mu^4}{\rho_l^2 \sigma_l^3}$$





# Bubble Rise Velocity

| Reference                        | Model                                                                            | Notes                                                                                                                                                                                                                                                                                           |
|----------------------------------|----------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| Stokes [22]                      | $V_T = 2\rho_l g R_{eq}^2 / 9\mu_l$                                              | Assumes a rigid sphere                                                                                                                                                                                                                                                                          |
| Nguyen & Schulze [23]            | $V_T = 18V_{stk} \left( \frac{4a^2 Ar^{2b-1} Mo^{0.46b}}{3k} \right)^{1/2-2b}$   | if $12,332 \leq Ar \leq 3.158 Mo^{-0.46}$ ; $a = 1$ , $b = 0$<br>if $3.158 Mo^{-0.46} \leq Ar \leq 29.654 Mo^{-0.46}$ ; $a = 1.14$ , $b = 0.176$<br>if $29.654 Mo^{-0.46} \leq Ar \leq 506.719 Mo^{-0.46}$ ; $a = 1.36$ , $b = 0.280$<br>if $506.719 Mo^{-0.46} \leq Ar$ ; $a = 0.62$ , $b = 0$ |
| Harmathy [24]                    | $V_T = 1.53 [\Delta\rho g \sigma / \rho_l^2]^{1/4}$                              | $Re > 500$                                                                                                                                                                                                                                                                                      |
| Lehrer [25]                      | $V_T = \sqrt{3\sigma / \rho_l D_{eq} + \Delta\rho g D_{eq} / 2\rho_l}$           | $Re > 476$                                                                                                                                                                                                                                                                                      |
| Peebles [26]                     | $V_T = 0.136 g^{0.78} (\rho / \mu)^{0.52} D_{eq}^{1.28}$                         | $2 < Re < 1,200$                                                                                                                                                                                                                                                                                |
| Clift et al. (pure) [20]         | $V_T = 1.909 g^{0.5} \left( \frac{\sigma_l}{\rho_l} \right)^{0.5} D_{eq}^{-0.5}$ | $Re > 1,200$                                                                                                                                                                                                                                                                                    |
|                                  | $V_T = 0.138 g^{0.82} (\rho / \mu)^{0.639} D_{eq}^{1.459}$                       | $D_{eq} < 1.3 \text{ mm}$                                                                                                                                                                                                                                                                       |
|                                  | $V_T = \sqrt{\frac{2.14\sigma_l}{\rho_l D_{eq}} + 0.505 g D_{eq}}$               | $D_{eq} > 1.3 \text{ mm}$                                                                                                                                                                                                                                                                       |
| Clift et al. (contaminated) [20] | $V_T = \frac{\mu}{\rho D_{eq}} Mo^{-0.149} (J - 0.857)$                          | $H = (4/3) Eo Mo^{-0.149} (\mu_l / \mu_{water})^{-0.14}$<br>if $H > 59.3$ ; $J = 3.42 H^{0.441}$<br>if $2 < H \leq 59.3$ ; $J = 0.94 H^{0.757}$<br>if $H \leq 2$ ; $J = Re Mo^{0.149} + 0.857$                                                                                                  |
| Park et al. [27]                 | $V_T = 1 / \sqrt{1/V_{vis}^2 + 1/V_{in}^2 + 1/V_{spheroid}^2}$                   | $V_{vis} = g \rho_l D_{eq}^2 / 12 \mu_l$<br>$V_{in} = 0.14425 g^{5/6} (\rho_l / \mu_l)^{2/3} D_{eq}^{3/2}$<br>$V_{spheroid} = \sqrt{2.14 \mu_l / \rho_l D_{eq} + 0.505 g D_{eq}}$                                                                                                               |



Orea, D., Robb, K., & McFarlane, J. (2025). Comparative study between experimental measurements and model predictions of bubble rise velocity in molten LiCl-KCl. *Nuclear Engineering and Design*, 443, 114247.

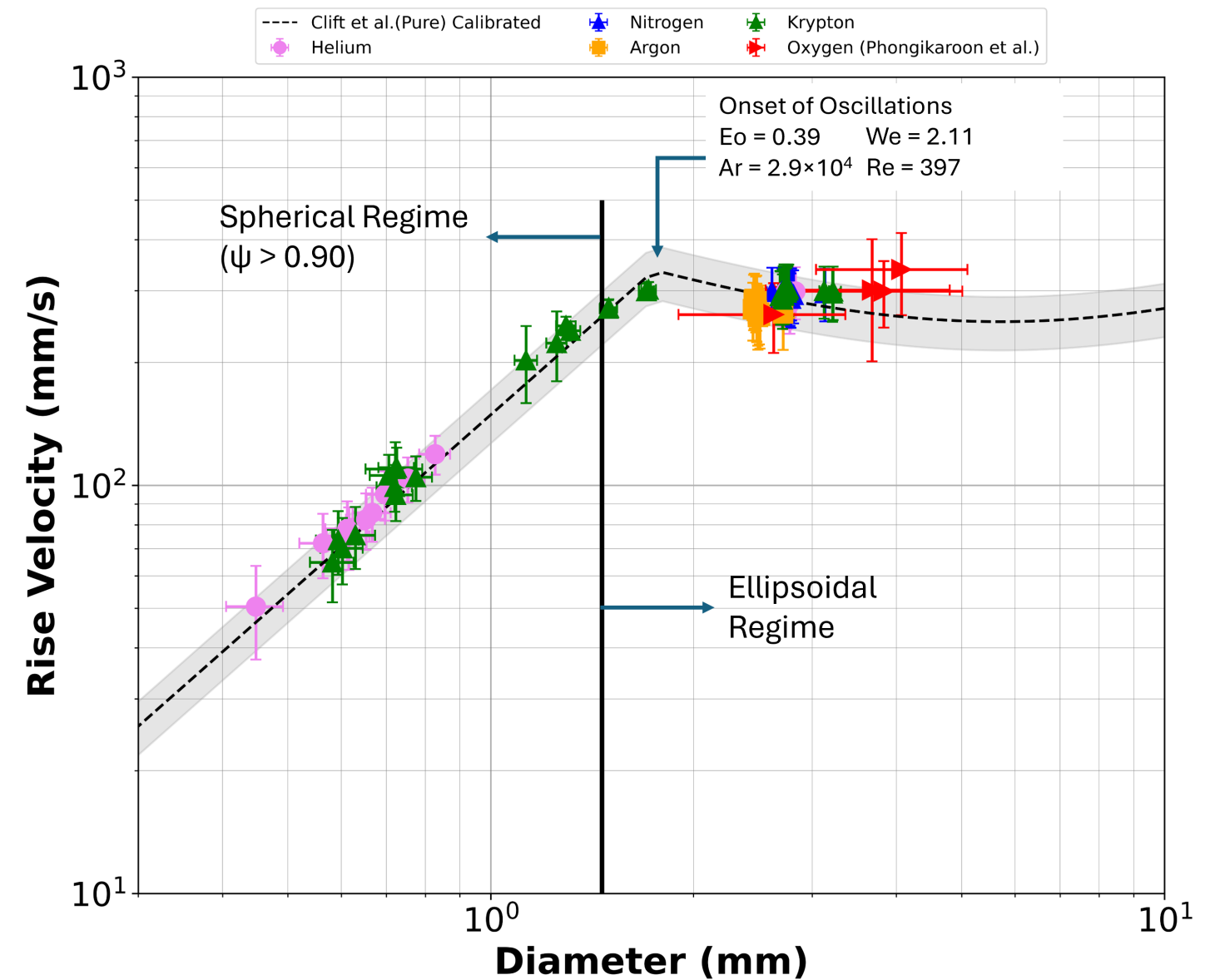
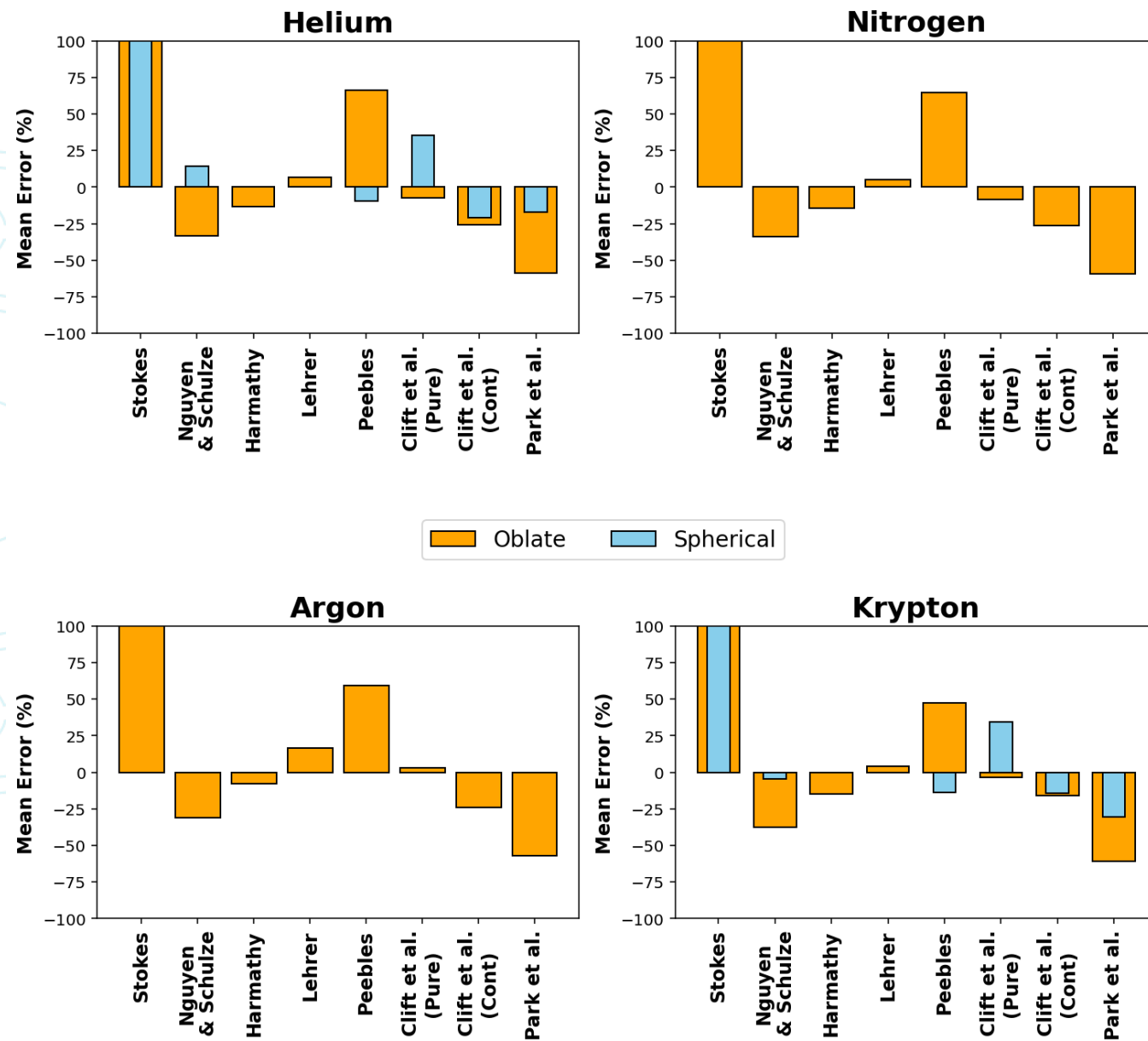


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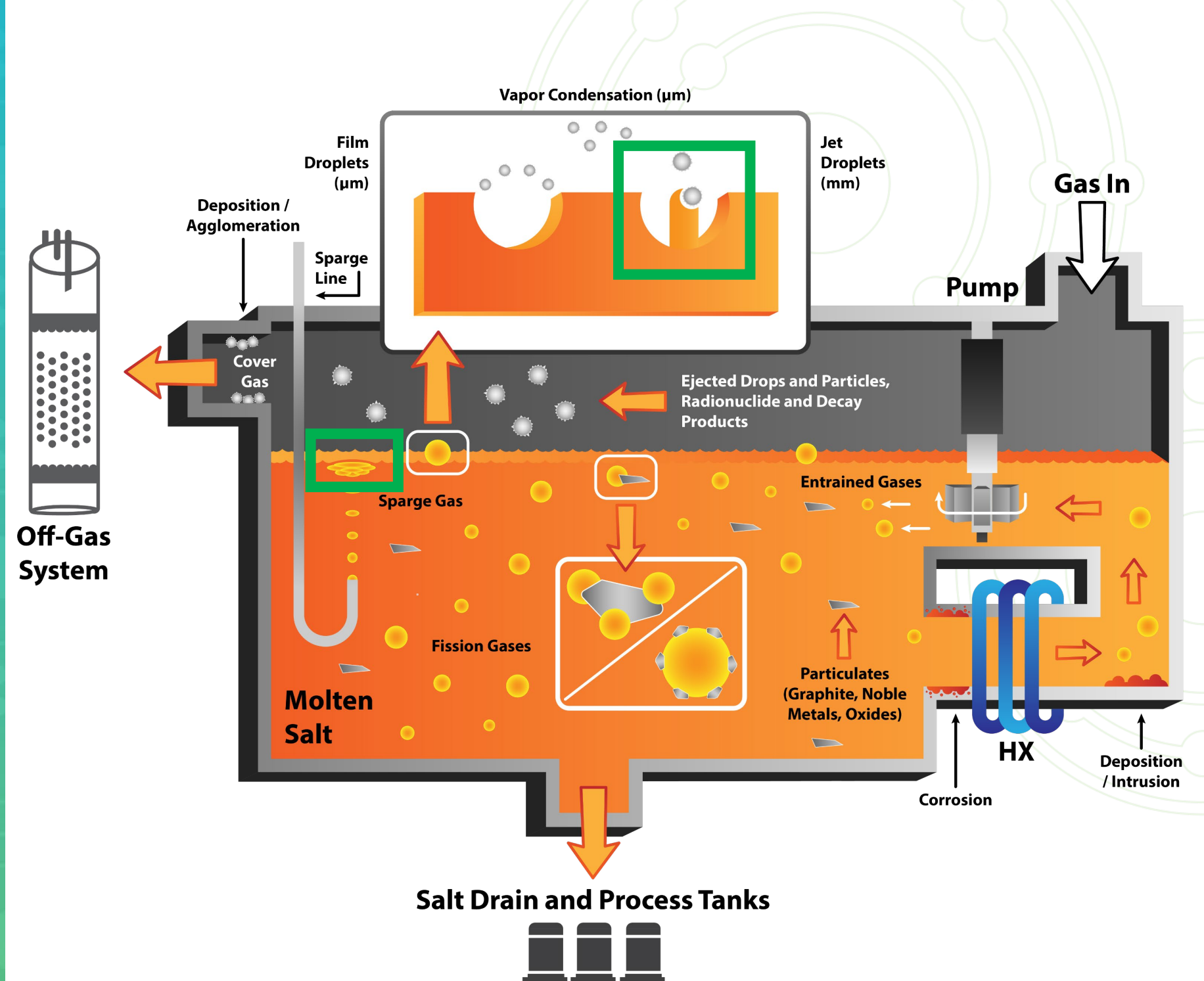
# Bubble Rise Velocity (cont'd)





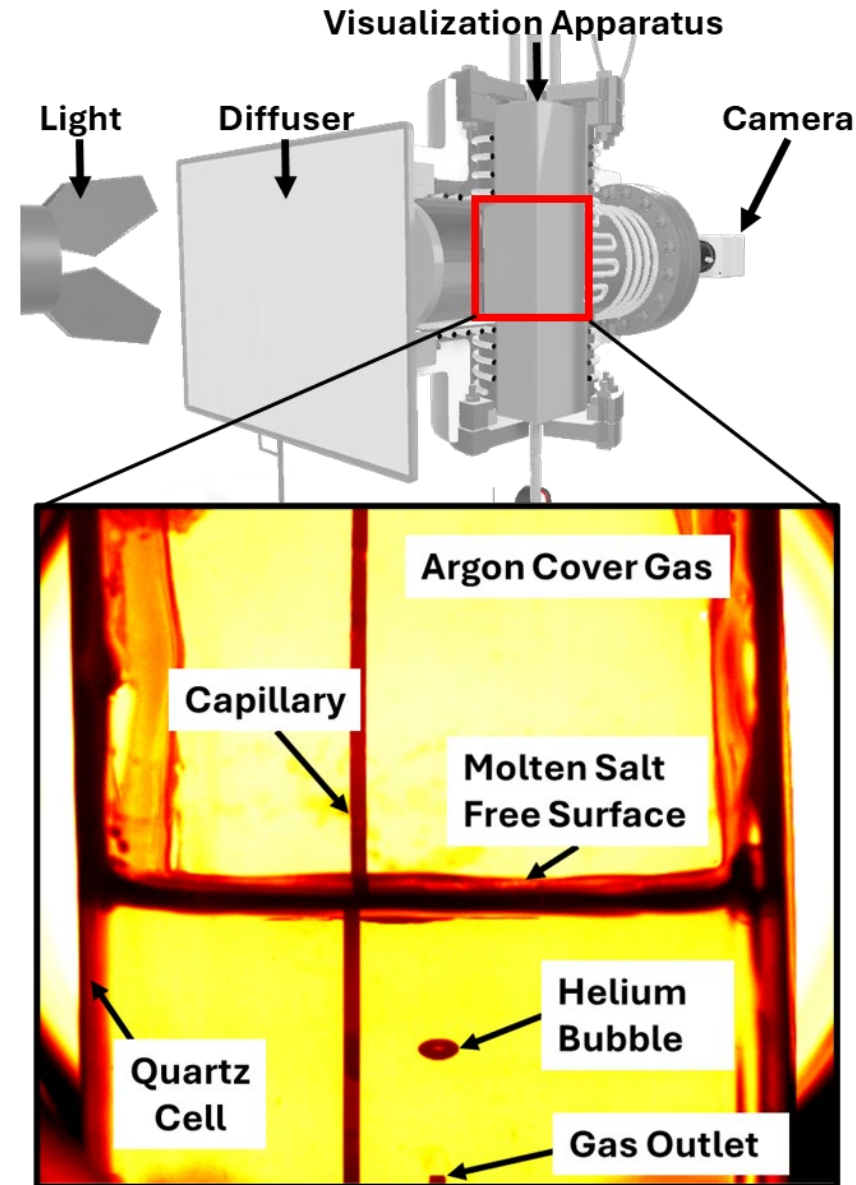
# MSR Gas and Particle Transport Phenomena

- Aerosol/particulate size drives entrainment and deposition in cover-gas/off-gas systems
- Bubble bursting at the free surface is a mechanical aerosol source (film and jet droplets)



# Jet Droplets Produced via Bubble Bursts

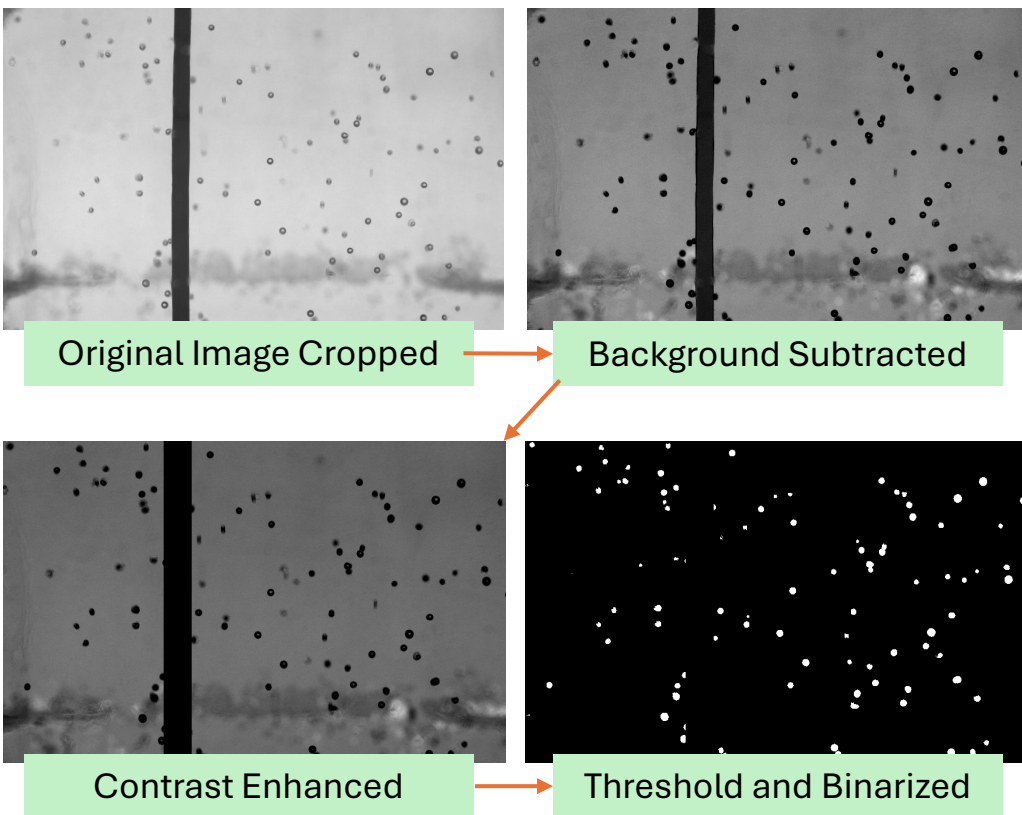
- Molten salt @ 500 °C
  - Liquid level dropped to be in frame
- Bubble injection:
  - Helium through 0.55 mm ID capillary
  - 25 mm below liquid surface
  - Gas injection rates = 2.5 / 5.0 / 10.0 sccm
- Imaging:
  - Phantom VEO 440 at 30 Hz
  - 128.9 seconds per test





# Aerosol Image Post-Processing and Tracking

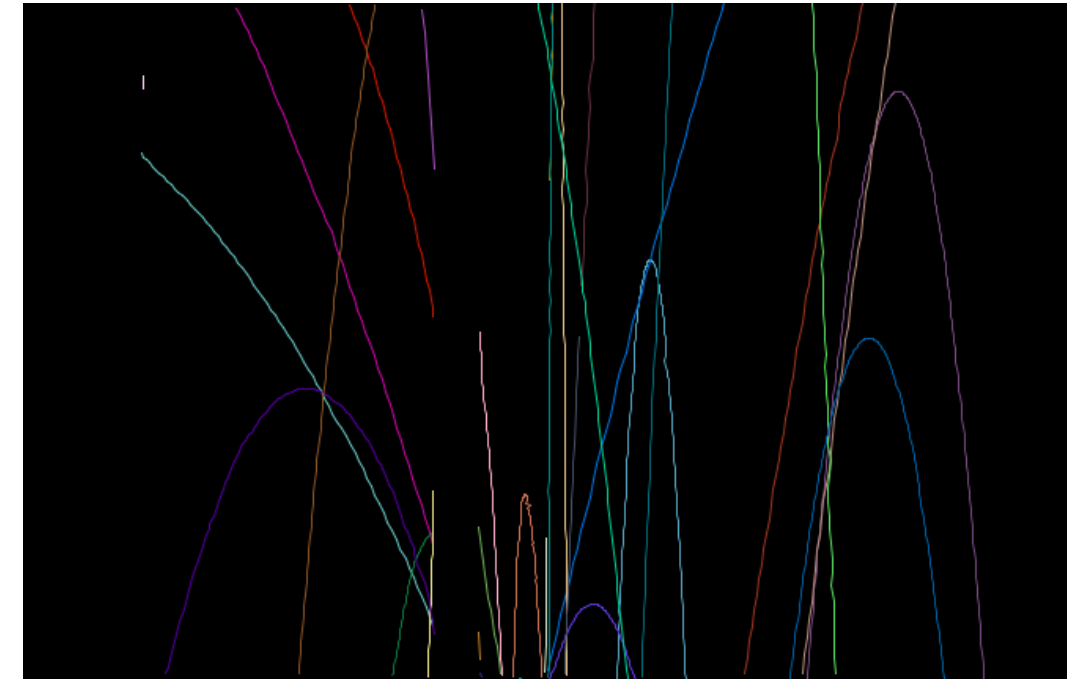
## Representative Post-Postprocessing



## Individual Aerosol Tracking

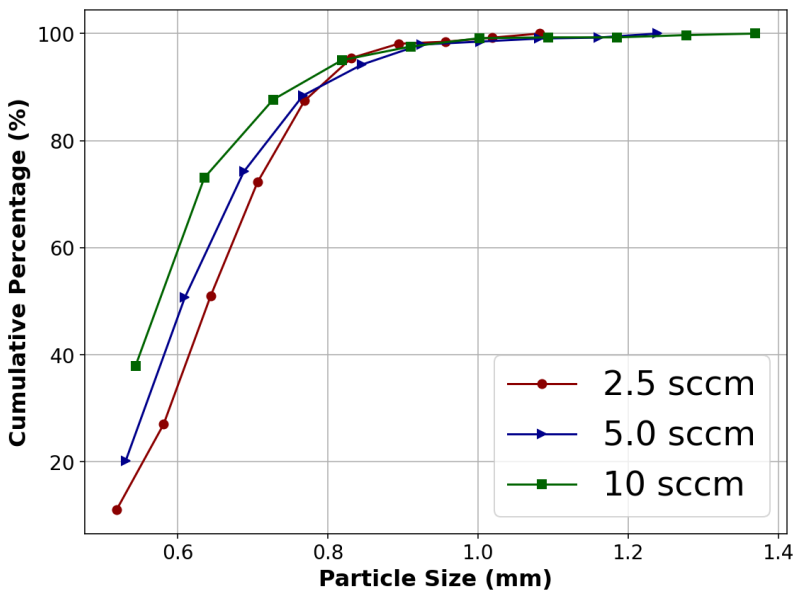
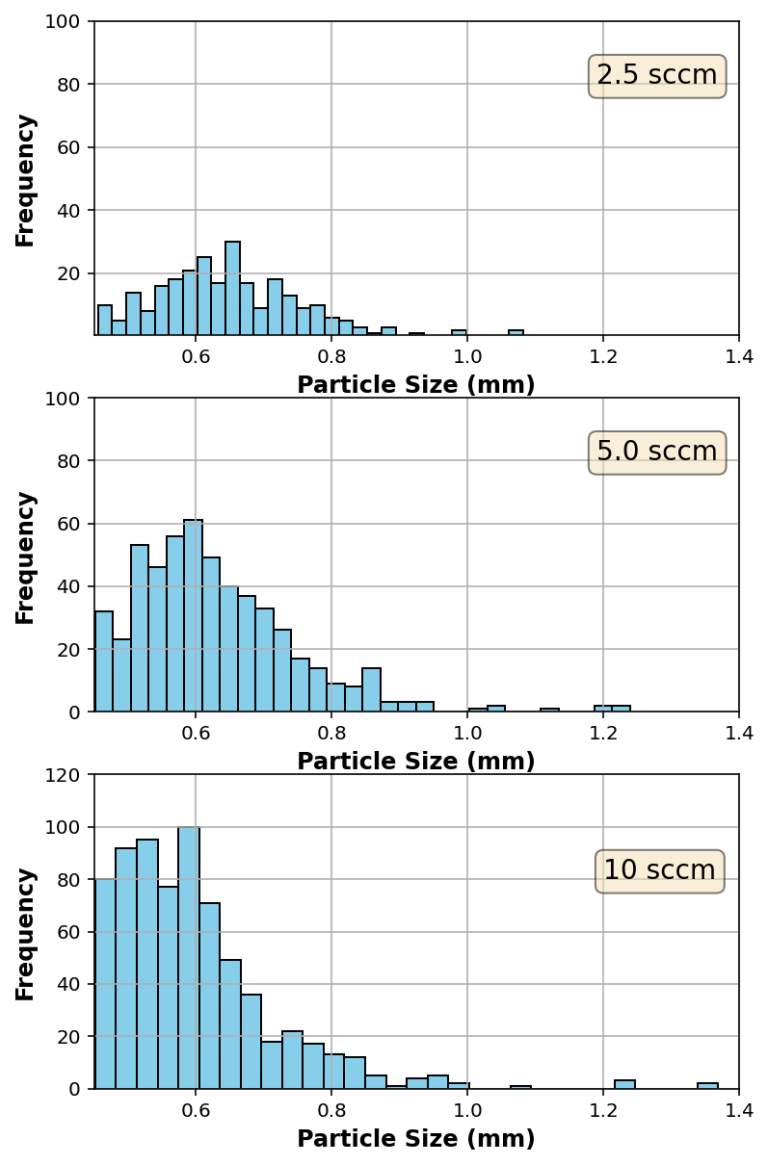


## Aerosol Tracks



# Characterization of Molten Salt Aerosols from Jet Droplets

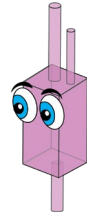
- Flow rate drives aerosol size distribution
- Mean aerosol diameter decreases slightly with increasing sparge rate
- Bubble count scales with flow rate; bubble size does not
- Aerosol-to-bubble ratio decreases at higher sparge rates



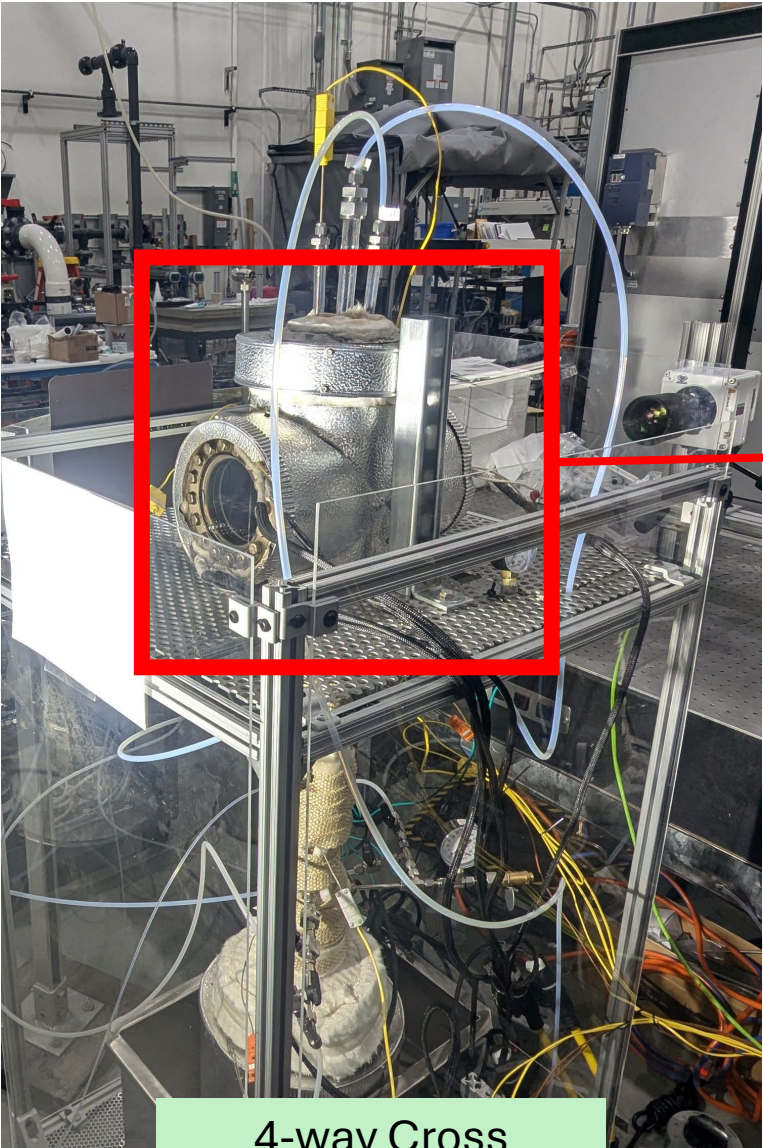
| Sparge rate (sccm) | 2.5  | 5.0   | 10    |
|--------------------|------|-------|-------|
| Bubbles Imaged     | 549  | 1,229 | 2,050 |
| $D_{b,mean}$ (mm)  | 3.02 | 3.00  | 2.99  |
| Aerosols Imaged    | 377  | 708   | 1,071 |
| $D_{p,mean}$ (mm)  | 0.65 | 0.63  | 0.59  |
| $N_p / N_b$        | 0.69 | 0.58  | 0.52  |



# Visualization of Insoluble Species and Transport Apparatus (VISTA)

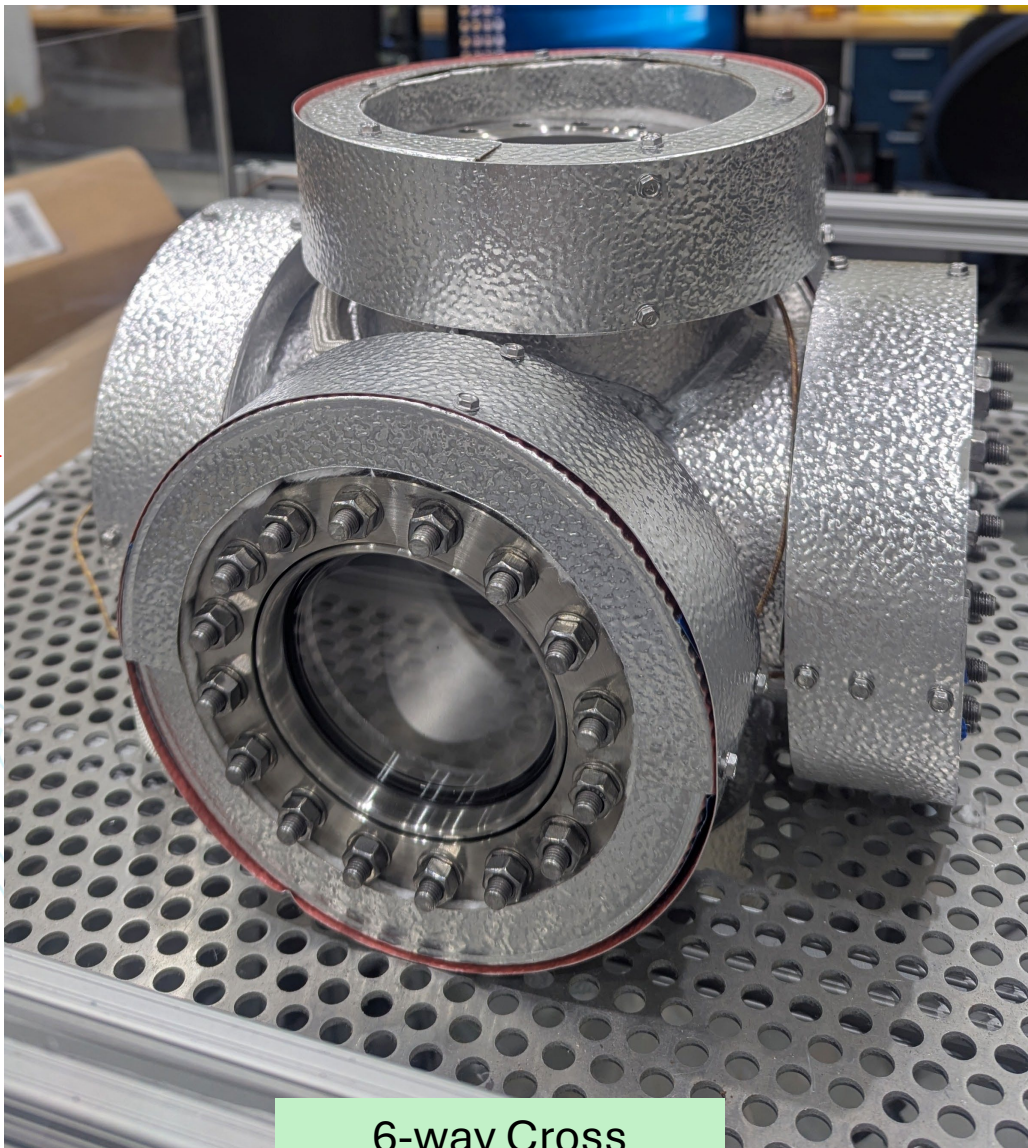


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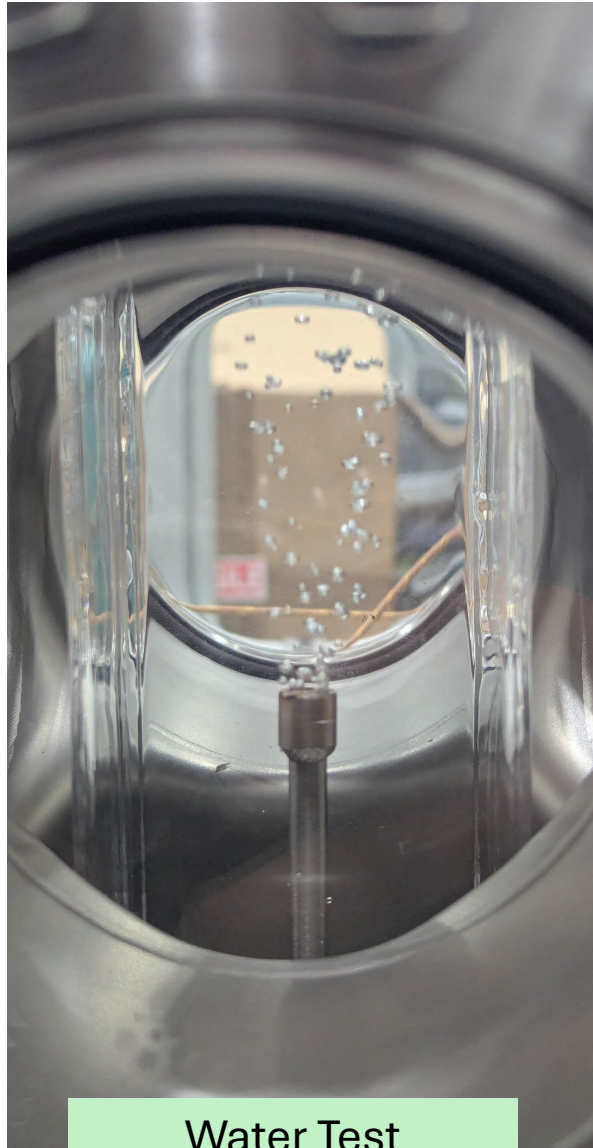
4-way Cross

Current Status



6-way Cross

New Bubblers



Water Test

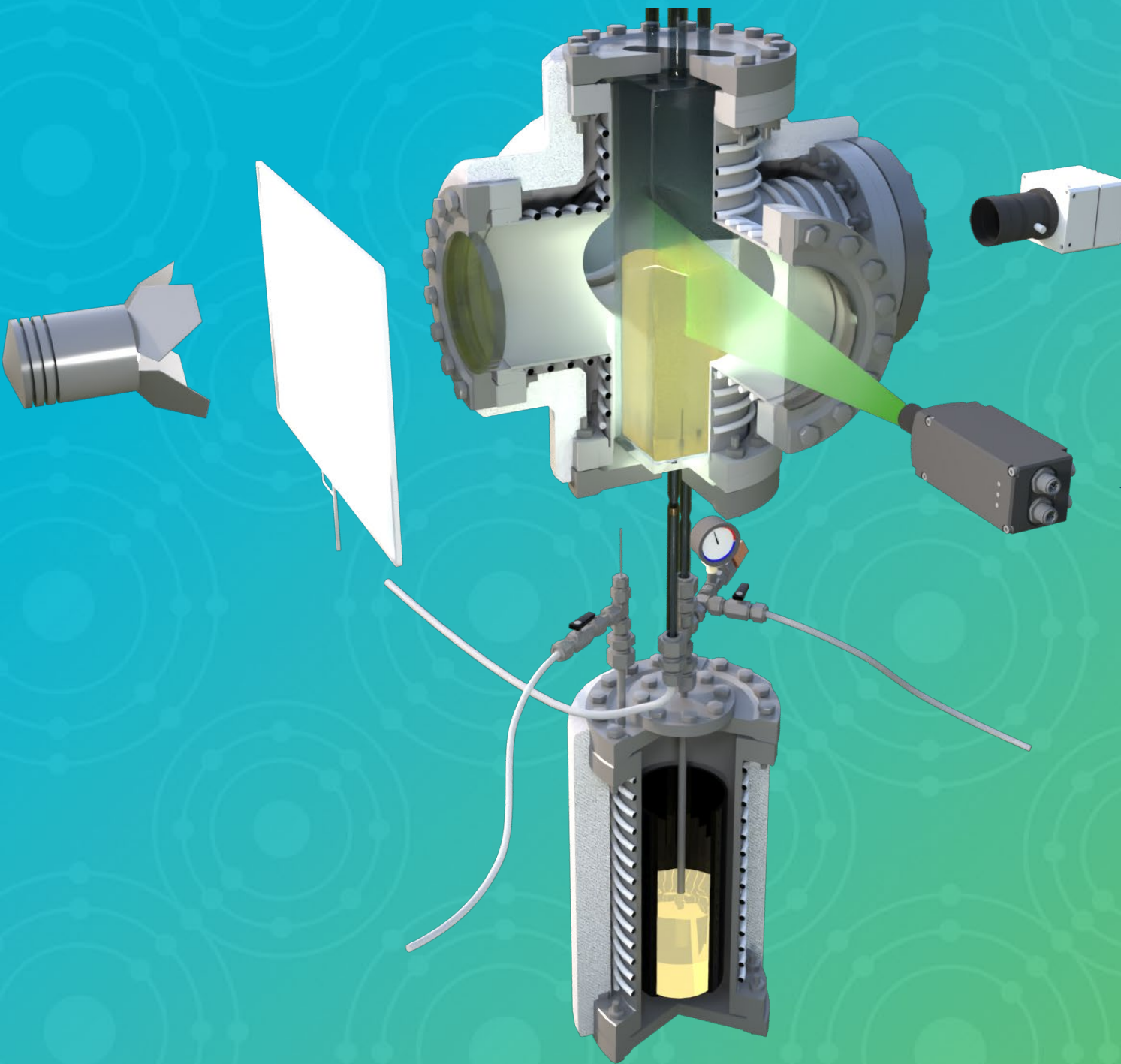
FY26

Plans to introduce insoluble particles to molten salt





# Experimental Data Collection



**FY24**

Established  
Optical  
Measurement  
Technique



**FY25**

Bubble Rise  
Velocity and  
Jet Droplet  
Data



**FY26**

Bubble and  
insoluble  
particle  
(micron)  
velocity, film  
and jet aerosol  
droplet data,  
off-gas  
composition

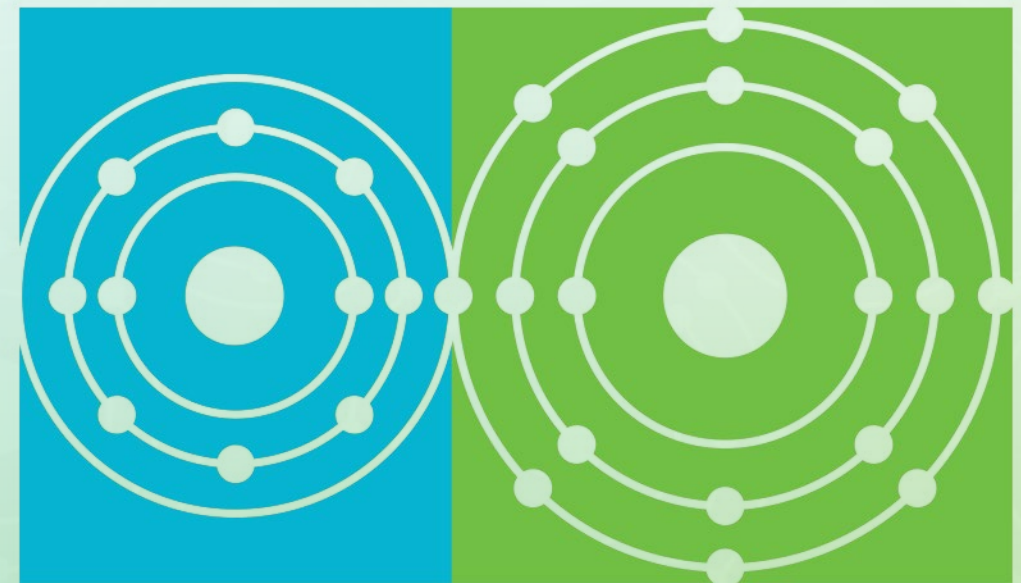
**FY27**

Bubble  
velocity and  
insoluble  
particle (sub-  
micron), film  
and jet aerosol  
droplet data,  
off-gas  
composition,  
stagnant and  
flowing salt



# THANK YOU!

[oread@ornl.gov](mailto:oread@ornl.gov)



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