



# GAIN: INNOVATIVE MATERIALS RESEARCH WORKSHOP

JUNE 15, 2022



The background features a line art illustration of a nuclear reactor core, showing various fuel elements and structural components in a perspective view.

# AURORA

FAST FISSION BY OKLO

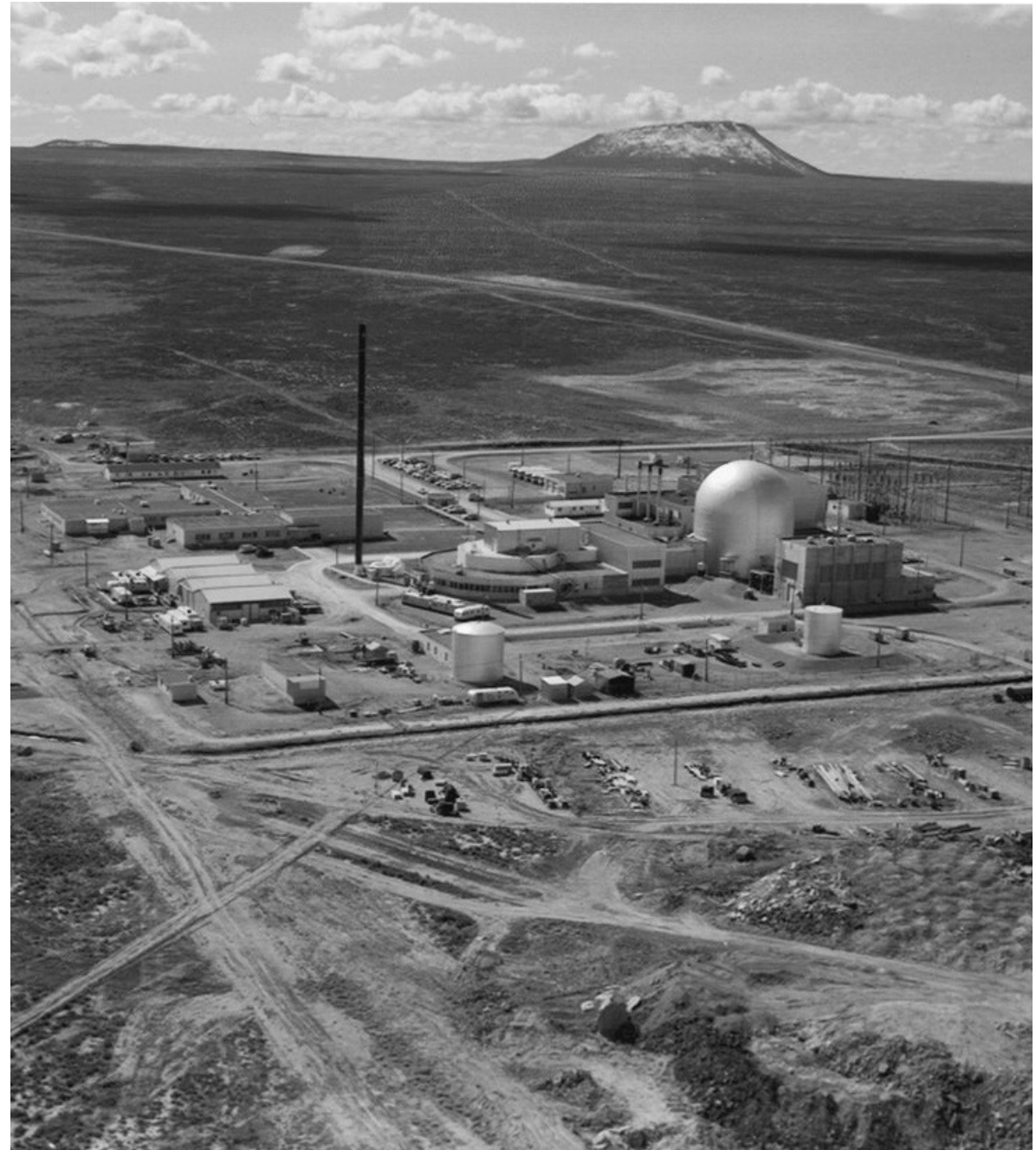


# MAKING REACTORS PEOPLE WANT

- ▷ **Affordable and reliable, 24/7 carbon-free power**
- ▷ **Flexible siting**
- ▷ **Minimal water resources required**
- ▷ **Inherently simple and robust**
- ▷ **Designed for performance**

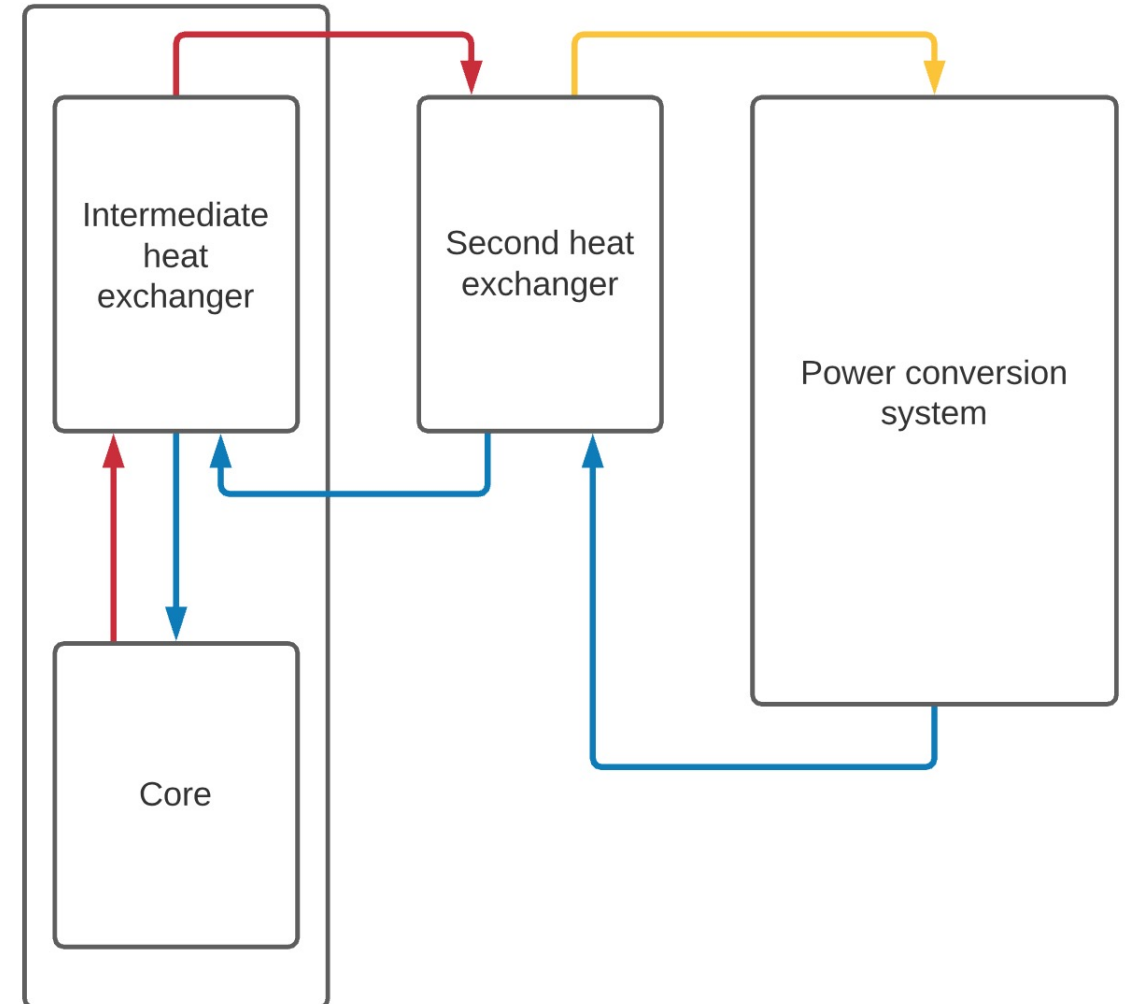
# A RICH HISTORY

The Aurora builds on the legacy of the **Experimental Breeder Reactor II**, a sodium-cooled fast reactor with onsite recycling of used fuel. EBR-II operated from 1964-1994, demonstrating inherent safety characteristics and the ability to recycle fuel.



# HOW IT WORKS

- ▶ Heat is generated by fission and transferred to liquid metal coolant
- ▶ Heat is then carried to the power conversion system
- ▶ The power conversion system converts heat to electricity, and can also deliver heat directly



# DESIGN PARAMETERS

Electric capacity	<b>1 to 15 MWe</b>
Thermal capacity	<b>4 to 50 MWt</b>
Temp. of usable heat	<b>500-550 C</b>
Capacity factor	<b>&gt;90%</b>
Licensed operating life	<b>20+ years</b>
Frequency of refueling	<b>10-20 years</b>
Land usage	<b>&lt;1 acre</b>

*Larger designs in development as well*

The background features faint, light gray architectural line drawings of building facades, showing various window patterns and structural elements. The drawings are positioned in the top right and bottom left corners, framing the central text.

# CLADDING & CORE MATERIALS

# CLADDING & CORE MATERIALS

1-5 years

5-10 Years

10+ Years

## Near Term

- Core materials manufactured from existing alloys such as ferritic/martensitic and austenitic stainless steel or legacy super alloys
- **Challenges**
  - Limited Supply Chain Capacity, Capability, and Desire

## Intermediate Term

- Existing alloys manufactured with FCCI barriers
- Incremental improvements of existing alloys
- Commercial availability of new alloys (e.g., refractory metal-based alloys)
- **Challenges**
  - Performance Data
  - Supply Chain Development

## Long Term

- Oxide dispersion Strengthened (ODS) Alloys
- New manufacturing methods
- Advanced fuel forms
- **Challenges**
  - Performance Data
  - Limited to no existing supply chain



# CLADDING & CORE MATERIALS (NEAR TERM)

- Designers with near term deployments have gravitated towards “available” alloys
  - Leverage data from past experiments
  - Tap existing manufacturing capability
- **Challenge**
  - US Supply Chain capacity to produce metal meeting typical “nuclear grade” requirements is limited
- **Opportunity**
  - Refine legacy requirements
  - Develop new suppliers



Designation: A 831/A831M – 95 (Reapproved 2000)

## Standard Specification for Austenitic and Martensitic Stainless Steel Bars, Billets, and Forgings for Liquid Metal Cooled Reactor Core Components<sup>1</sup>

This standard is issued under the fixed designation A 831/A831M; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon ( $\epsilon$ ) indicates an editorial change since the last revision or reapproval.

### 1. Scope

1.1 This specification covers hot- and cold-finished austenitic and martensitic stainless steel bars, billets, and forgings intended for use in manufacturing core components used at high temperatures in liquid metal cooled nuclear reactors.

1.2 The bars, billets, and forgings are intended for machining, welding, hot- and cold-forming operations.

1.3 The values stated in either inch-pound units or SI units are to be regarded separately as standard. Within the text, the SI units are shown in brackets. The values stated in each system are not exact equivalents; therefore, each system shall be used independently of the other. Combining values from the two systems may result in nonconformance with the specification.

1.4 This specification and the applicable material specifications are expressed in both inch-pound and SI units. However, unless the order specifies the applicable “M” specification designation (SI units), the material shall be furnished in inch-pound units.

### 2. Referenced Documents

2.1 *ASTM Standards:*

A 370 Test Methods and Definitions for Mechanical Testing of Steel Products<sup>2</sup>

A 388/A388M Practice for Ultrasonic Examination of Heavy Steel Forgings<sup>3</sup>

A 484/A484M Specification for General Requirements for Stainless Steel Bars, Billets, and Forgings<sup>3</sup>

A 751 Test Methods, Practices, and Terminology for Chemical Analysis of Steel Products<sup>2</sup>

E 3 Methods of Preparation of Metallographic Specimens<sup>4</sup>

E 45 Practice for Determining the Hardness of Metals<sup>5</sup>

2.2 *ANSI Standard:*

B 46.1 Surface Texture<sup>5</sup>

2.3 *ASNT Standard:*

SNT-TC-1A Recommended Practice for Nondestructive Testing Personnel Qualifications and Certification<sup>6</sup>

2.4 *ASME Standard:*

NQA-1 Quality Assurance Program Requirements for Nuclear Facilities<sup>7</sup>

### 3. Ordering Information

3.1 It is the responsibility of the purchaser to specify all requirements that are necessary for material ordered under this specification. Such requirements may include but are not limited to the following:

3.1.1 Quantity (weight or number of pieces).

3.1.2 Condition (cold-worked, annealed, or tempered).

3.1.3 Finish.

3.1.4 Applicable dimensions, including size, thickness, width, and length (if forgings, include prints or sketches).

3.1.5 Form (bars, billets, etc.).

3.1.6 Grade designation.

3.1.7 ASTM designation and year of issue.

3.1.8 Marking requirements.

3.1.9 Other applicable documents (2.4).

3.1.10 Melting process (4.2).

3.1.11 Approval procedures for conversion of ingots (4.2).

3.1.12 Additional requirements for austenitic grades (4.2).

3.1.13 Additional requirements for martensitic grades (4.2).

3.1.14 Additional requirements (4.6).

3.1.15 Additional requirements (5.1).

3.1.16 Additional requirements (5.3).

3.1.17 Additional requirements (5.3).

3.1.18 Additional requirements (5.3).

3.1.19 Additional requirements (5.3).

3.1.20 Additional requirements (5.3).

3.1.21 Additional requirements (5.3).

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3.1.25 Additional requirements (5.3).

3.1.26 Additional requirements (5.3).

3.1.27 Additional requirements (5.3).

3.1.28 Additional requirements (5.3).

3.1.29 Additional requirements (5.3).

3.1.30 Additional requirements (5.3).

## 4. Manufacture

4.1 *Melting*—Unless an alternative melting process has been specified in Section 9, the process for austenitic grades shall consist of a vacuum induction melt followed by a consumable electrode vacuum-arc remelt. Additions of rare earths during melting are prohibited unless approved by the purchaser.

# CLADDING & CORE MATERIALS (INTERMEDIATE)

- Improvement of existing alloys using metallurgical fundamentals
  - Austenitic Alloys
  - Impact of Manufacturing Variability on Properties
  - Product Form Variations
- Development of a Commercial Source for New Alloys
  - Refractory alloys (e.g., vanadium)
- Fabrication of cladding from existing alloys with FCCI barrier for SFRs

Project No. 09-779

**Development of Diffusion Barrier Coatings and Deposition Technologies for Mitigating Fuel Cladding Chemical Interactions (FCCI)**

Fuel Cycle R&D  
Dr. Kumar Sridharan  
University of Wisconsin, Madison

In collaboration with:  
Idaho National Laboratory

Frank Goldner, Federal POC  
James Cole, Technical POC

Journal of Nuclear Materials  
Volume 560, March 2022, 153492

ELSEVIER

Void swelling of conventional and composition engineered HT9 alloys after high-dose self-ion irradiation

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**Abstract**

Ferritic/martensitic (F/M) steels are being considered as potential structural materials for next generation nuclear reactors, and variants of the alloy HT9 are some of the most promising candidates. In this study, two conventional and two composition engineered HT9 alloys were irradiated using 3.5 MeV Fe<sup>2+</sup> up to 600 peak displacement-per-atom (dpa) at 450 °C. Void swelling and microstructure

## Assessment of the Propensity of Low Creep Ductility for Optimized Grade 92 Steel



ORNL/TM-2018/972

Lizhen Tan

9/7/2018

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