

U.S. DEPARTMENT OF  
**ENERGY**

Office of  
**NUCLEAR ENERGY**



# Materials Surveillance Development

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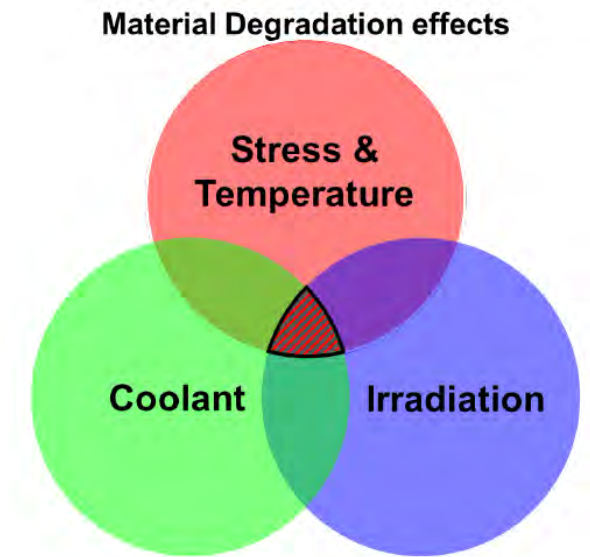
Annual MSR Campaign Review Meeting 2-4 May 2023

# FY23 Work Packages

- **RD-23IN060302, Materials Surveillance Development – INL**
  - Development Team
    - Michael McMurtrey, Heramb Mahajan, Mahmut N. Cinbiz, Tate Patterson, Ting-Leung Sham
    - Kaelee A. Novich (INL Intern, Boise State University PhD student)
  - Experimental Support
    - Austin Matthews, Dave Cottle, Joel Simpson, Caleb Picklesimer
- **RD-23AN060301, Materials Surveillance Development – ANL**
  - Mark C. Messner

# Overview – Materials Surveillance Technology

- **Synergistic material degradation effects in operating reactors**
  - Irradiation
  - Corrosion
  - Stress and temperature exposure (creep-fatigue loading)
- **Limited Information on materials degradation in molten salt reactor environment**
- **Surrogate materials surveillance technology can be used to**
  - Validate conservatism of allowable stresses based on time-extrapolation of failure data (ASME Section III, Division 5)
  - Generate key performance data on materials degradation to support the execution of the Reliability and Integrity Management (RIM) program (ASME Section XI, Division 2)
- **Technology gaps**
  - Availability of surveillance test articles that can induce mechanical damage passively during reactor operation and interact synergistically with materials degradation due to corrosion and irradiation
  - Testing of surveilled test articles, acceptance criteria, and remaining life determination
- **This work bridges these gaps by developing and maturing such materials surveillance technology**



# R&D Goals For the Surveillance Test Article and FY23 Plans

- **Reduce the size**
- **Enhance fabricability**
- **Demonstrate design robustness:**
  - Thermal cycling in air
  - Thermal cycling in molten salt
  - Thermal cycling in molten salt and under irradiation
- **Develop acceptance criteria**
- **Collaboration**
  - Bilateral with JAEA [sodium coolant] under CNWG, started in mid 2022
  - Formalize collaboration with the Canadian Nuclear Laboratories (CNL) [reactor grade helium] through INL/CNL CRADA under US-Canada Bilateral



25-mm diameter,  
300-mm long

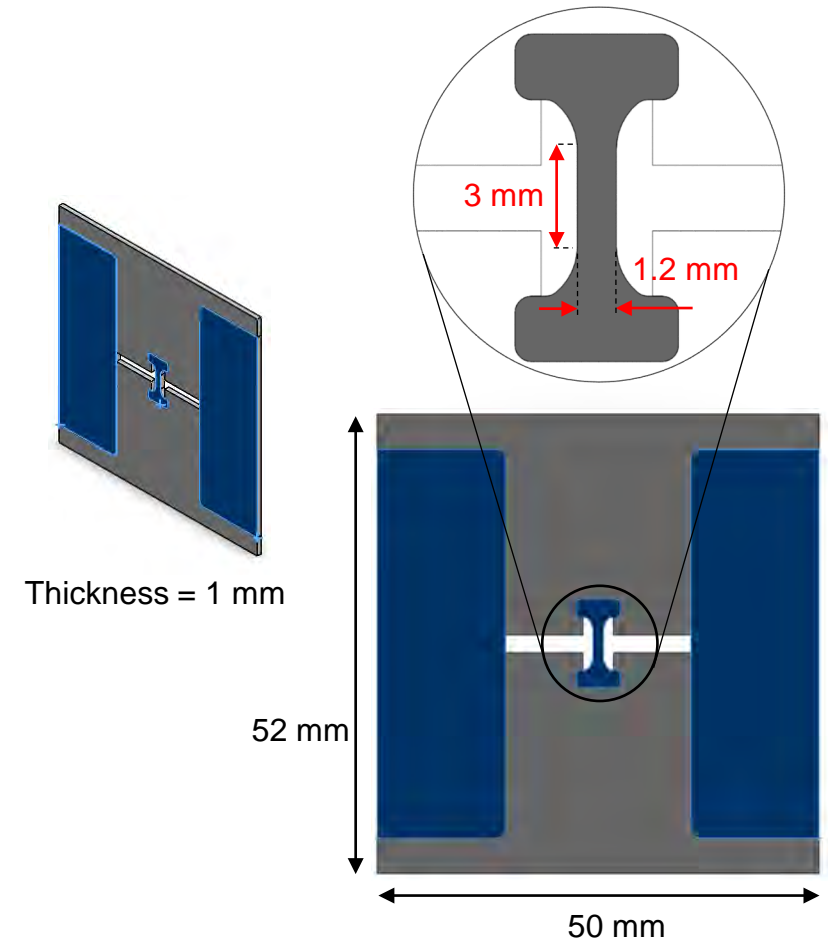
25-mm diameter,  
75-mm long



50x50x1 mm

# New Surveillance Test Article

- **Easier to manufacture**
- **Easier to instrument and monitor during the validation of the technical basis**
- **Smaller and less disruptive to fluid flow/plant operation**
- **Design is more accessible for evaluation and mechanical testing after the test articles are removed from the reactor; also, smaller activated volume**

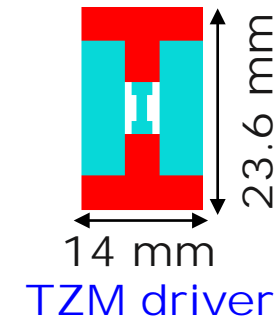


# Comparison of Different Driver Materials in the New Test Article

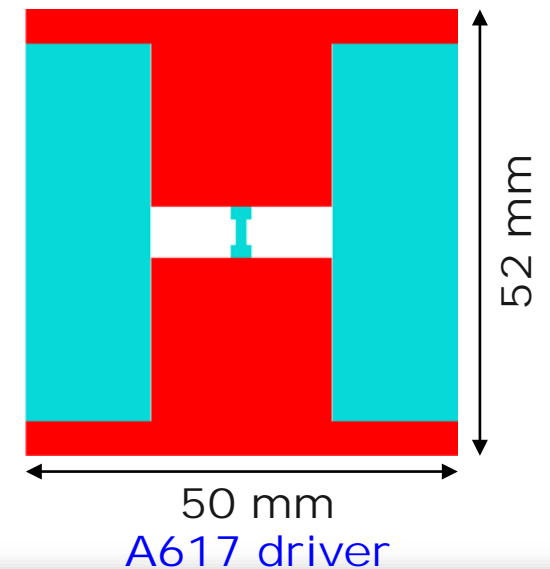
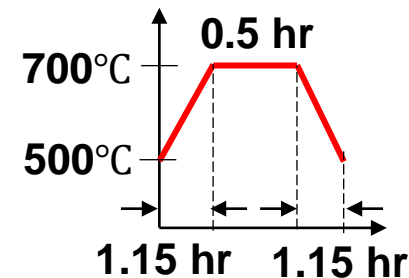
- **Test article design with**
  - Same gauge length and different driver materials
  - Identical test article design parameters
- **Higher expansion mismatch between driver and test material results in**
  - Reduction in the test article size
  - Wider coverage of strain ranges and follow-up factors

## Design parameters

1. Strain range = 0.52%
2. Follow-up = 2.7
3. Temperature cycle
4. Dwell time = 30 min

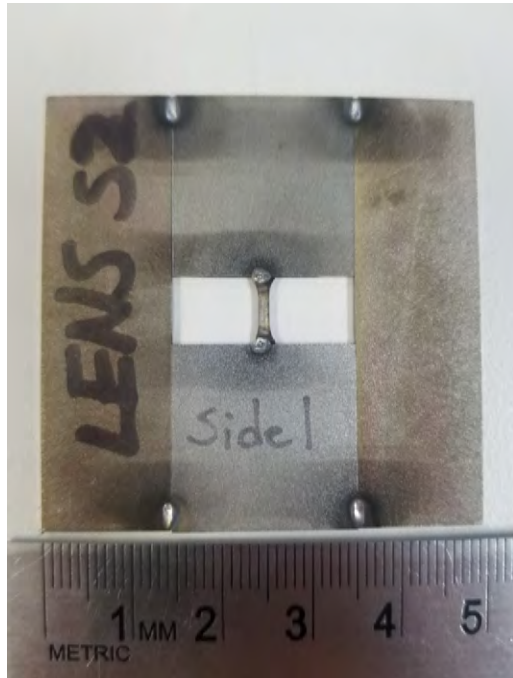


## Temperature cycle



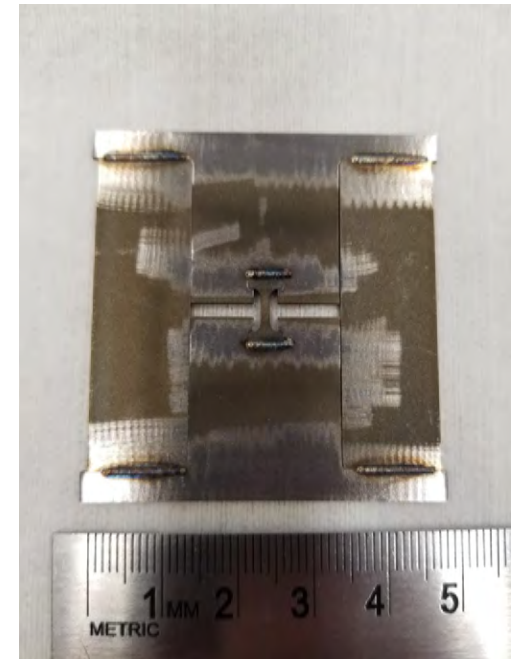
# Welded Flat Test Article, Version 1 and Version 2

**Version 1**



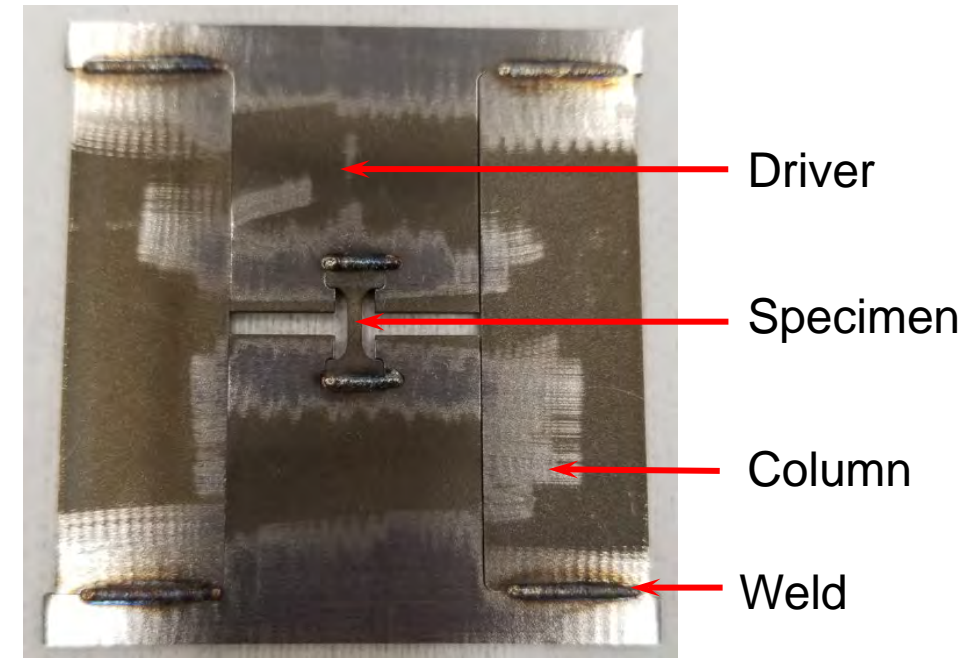
- Two versions of welded flat test articles were examined
- Version 2 improved the weldment location to reduce the stress concentrators at the weldments of version 1 that led to premature failure

**Version 2**



# Test Article Fabrication Through Welding – Version 2

- **Welded using blown powder laser directed energy deposition (laser-DED) system**
- **Continuous wave ytterbium fiber laser**
- **300 W of power with an approximately 1 mm beam diameter**
- **316L powder composition**
- **4.2 mm/s travel speed**





# Interlocking Specimen

- **Designed to be weld-free**
  - Weldments are a potential early failure point
  - Some desirably materials, like TZM, with low thermal expansion coefficients have low weldability
- **Assembled from individual components and bolted together with cover plates**



Arrangement of parts without cover plates

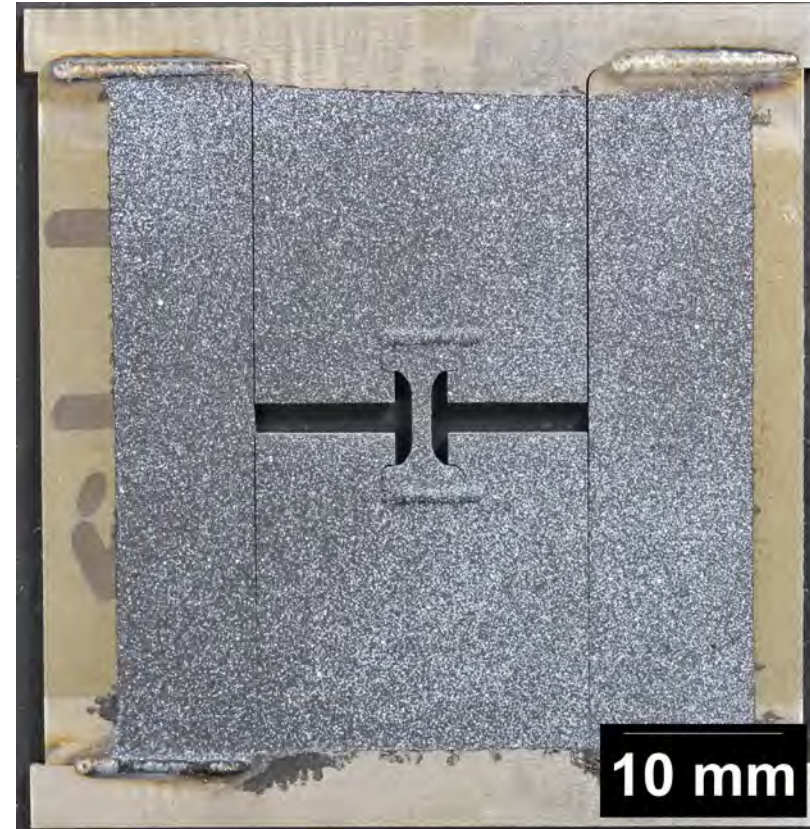


Arrangement of parts with cover plates



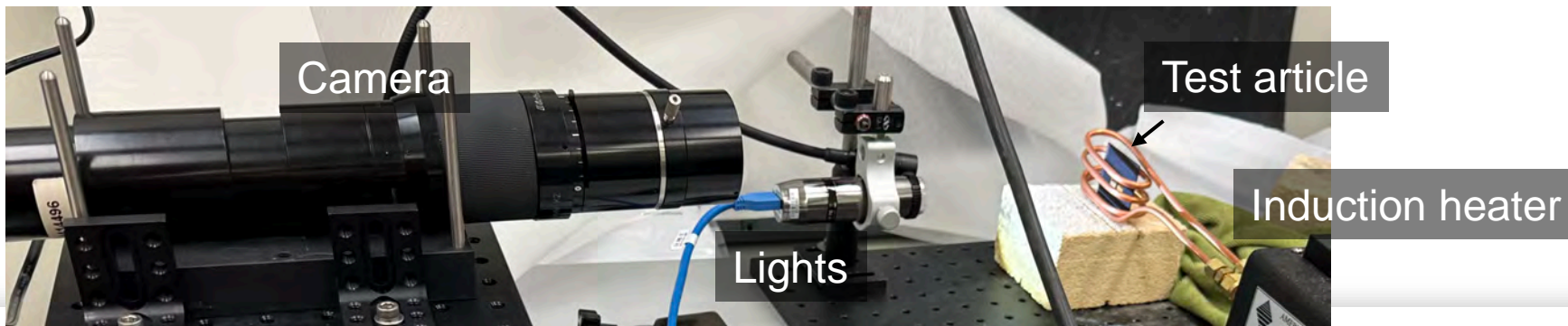
# Local Strain Measurements Through Digital Image Correlation

- **Speckle pattern applied through spray techniques**
- **Requires line of sight for strain measurements**



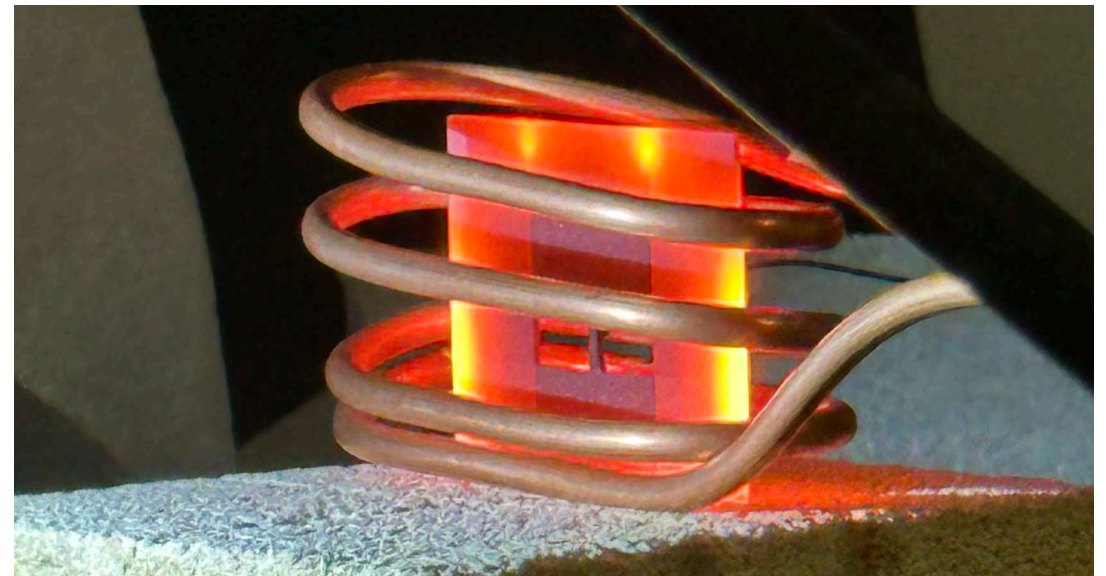
# Induction Heating Tests

- **Allows for easier strain measurements on test article**
- **Drastically increases temperature ramp rate**
  - Furnace test, with a 30-minute hold time at peak temperature, resulted in approximately 10 cycles per day
  - Induction heater, with a 30-minute hold time at peak temperature, was able to perform the full cycle in 36 minutes.



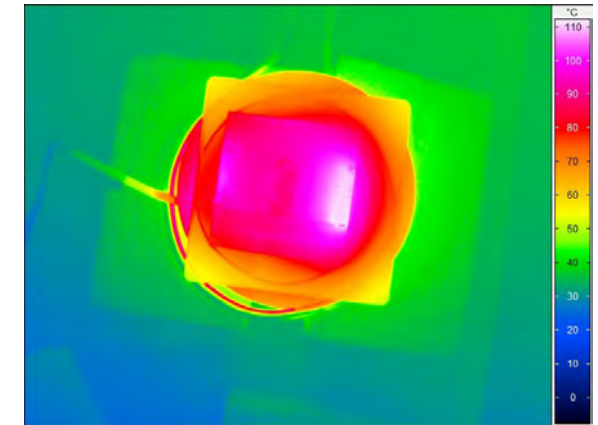
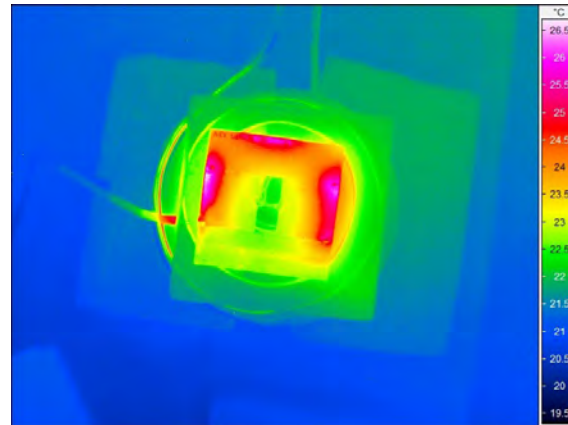
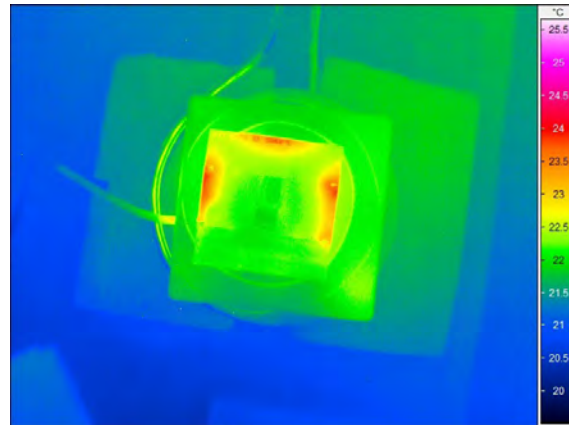
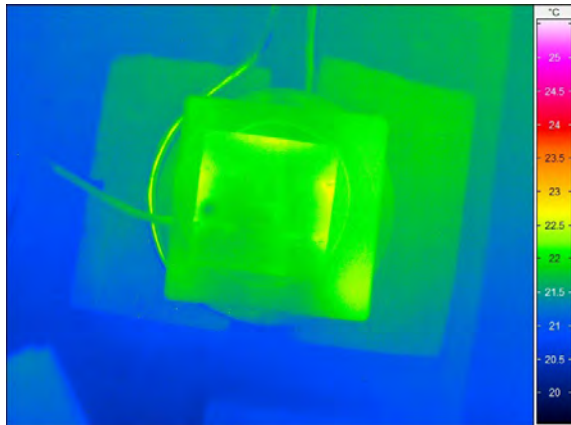
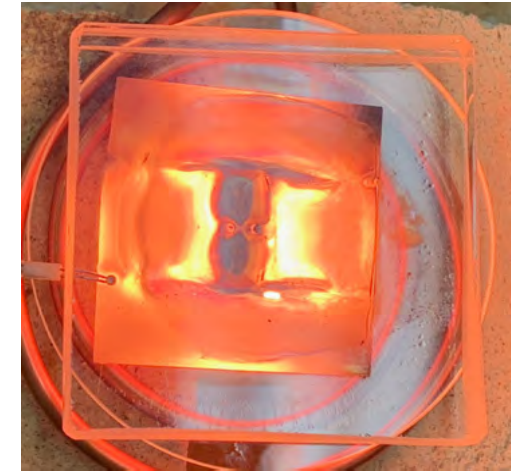
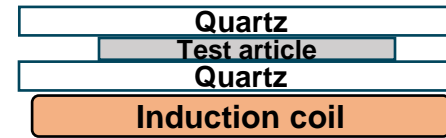
# Induction Heating Coil

- **Largest challenge is uniformity of temperature**
- **Significant overheating on edges and at weld joints**



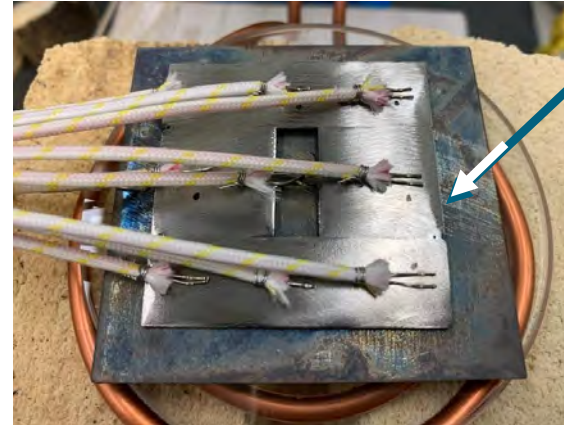
# Pancake Coil Induction Heating

- Uneven heating when specimen heated directly from the pancake coil

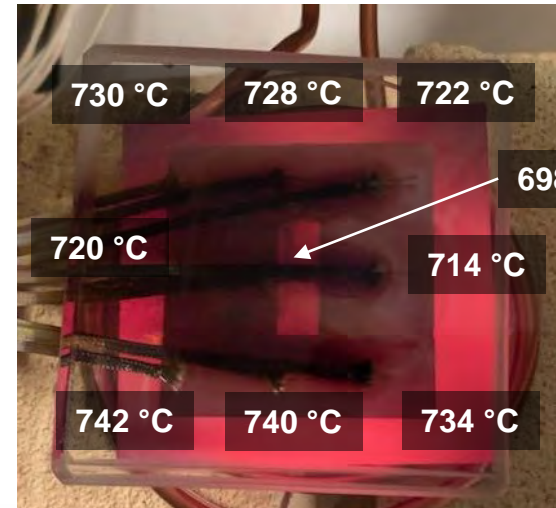
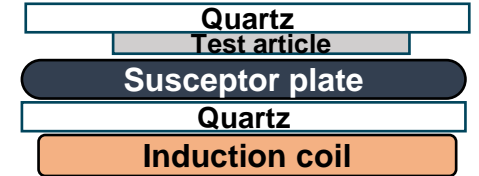


# Induction Heating Pancake

- Pancake coil design was used
- Still significant temperature gradients when test article was heated directly by the coil
- Susceptor plate was placed between the coil and the specimen, helped moderate the temperature
- Further modification of susceptor plate and coil geometries is expected to further reduce the temperature gradient



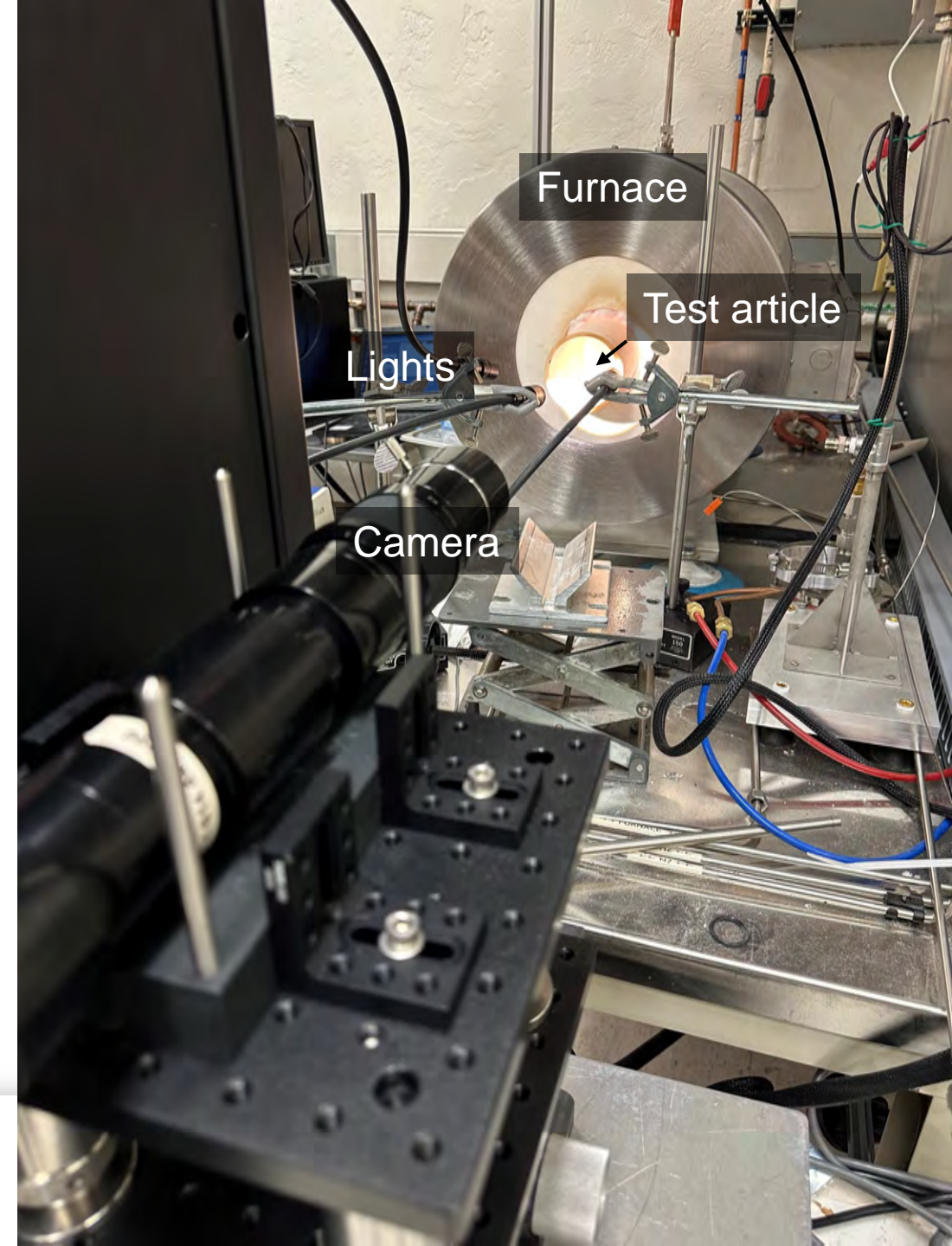
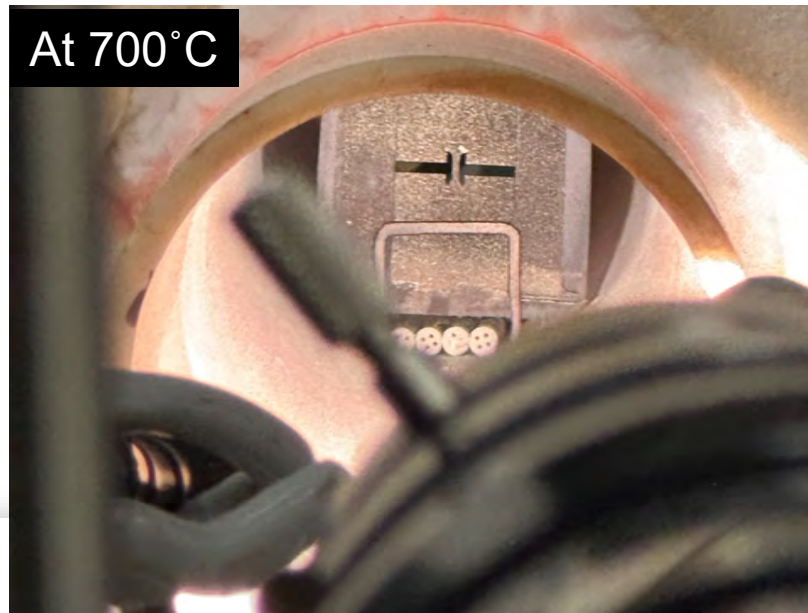
Susceptor Plate



- Thermocouples readings
- Used for validation only
- Will not be welded to actual test article during test

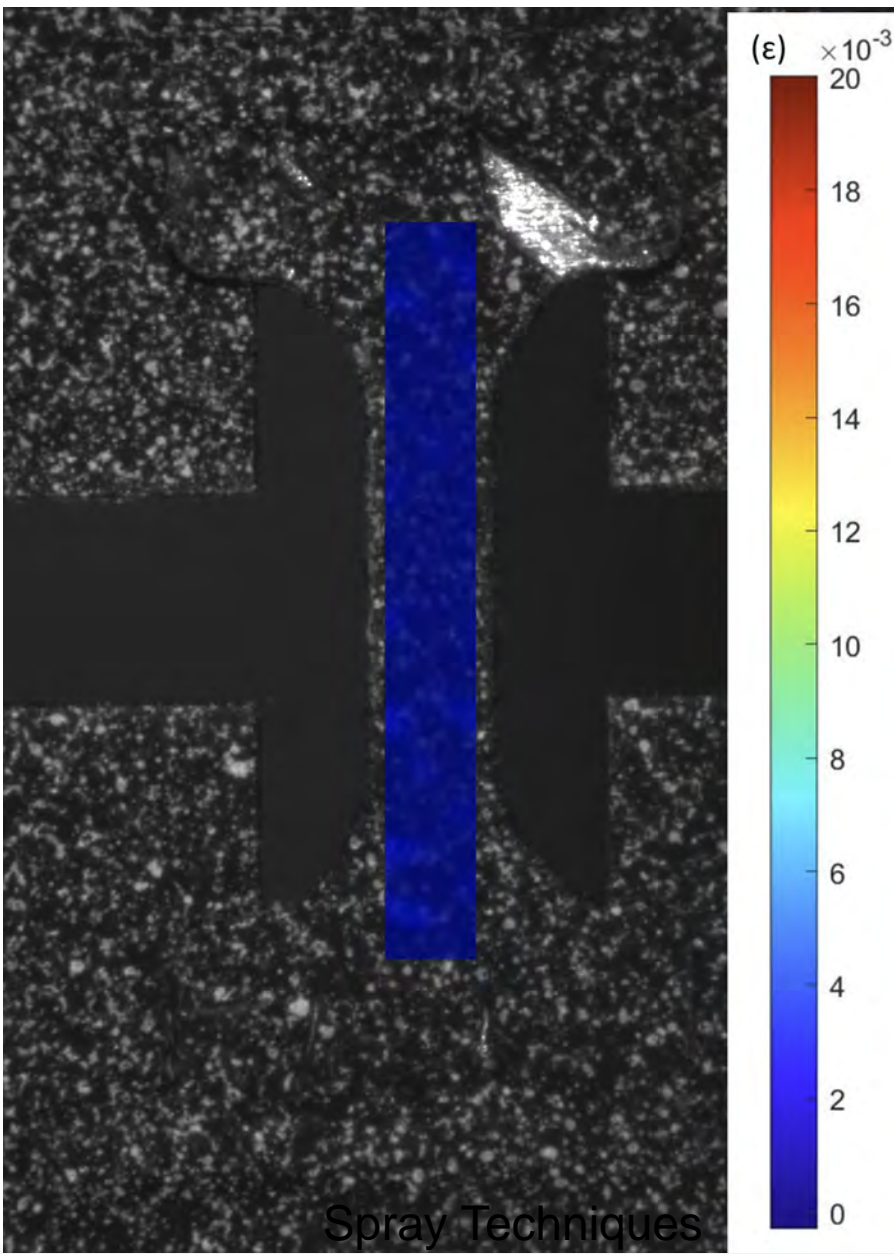
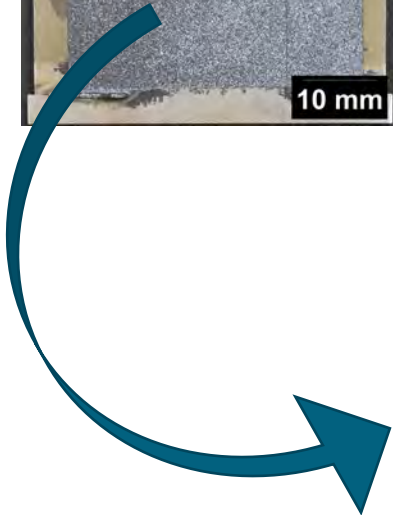
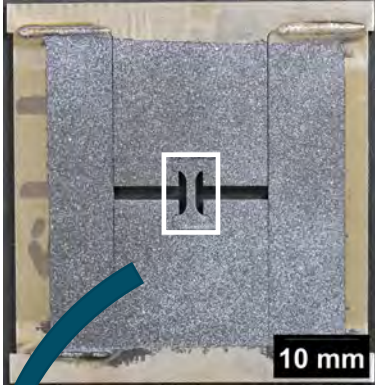
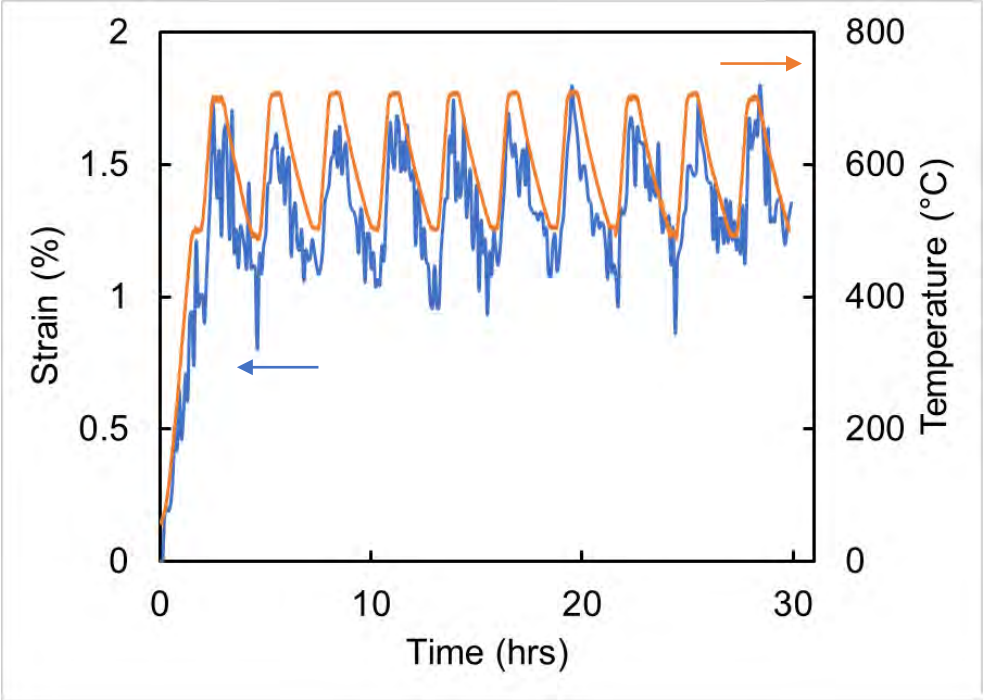
# Furnace Testing

- Temperature ramped to 700°C
- Temperature hold at 700°C for 30 minutes
- After hold, cycled to 500°C, then back to 700°C



# Furnace Test Results

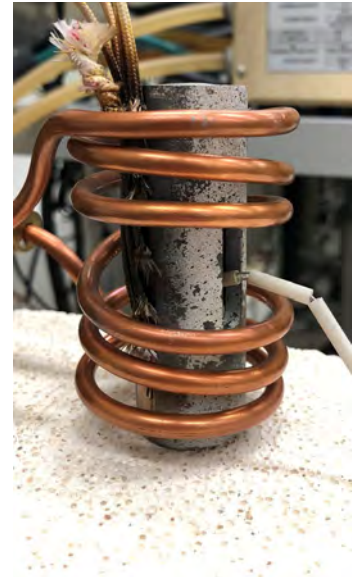
- **Strain map from first ten cycles**





# Induction Heating of Cylindrical Test Article

- Uneven heating noted on the outer casing
- Modified coil design is capable of fixing this, however, internal specimen temperature was also noted to be significantly cooler than casing
- This specimen design is better suited for furnace testing



# “Measuring” Remaining Life

- **Samples exposed to long-term service in MSR environment**
- **Periodically removed**
- **What type of testing can we do to determine “remaining life” = how long the material would have lasted under service conditions?**
- **Limitations:**
  - In-situ monitoring of samples may be limited – can’t continuously monitor mechanical behaviour
  - Samples may be irradiated when removed from reactor
  - Test should be short – will want answer quickly/during outage to make operation decisions

# Surrogate Materials Surveillance Protocols

|  | Creep/steady load   | Cyclic load (traditional)                                     | Cyclic load (no damage)  |
|--|---|---|--|
| Mechanical properties data from temperature and stress | Creep to failure (including strain measurement)               | Creep-fatigue to failure                                      | Short term creep-fatigue deformation                                   |
| In-reactor surveillance test articles                  | Steady mechanical, thermal, and environmental                 | Cyclic mechanical, thermal, and environmental                 | Cyclic mechanical, thermal, and environmental                          |
| “Out-of-pile” testing of surveilled materials          | Creep – subscale samples or indentation                       | Cyclic  | Cyclic   |
| Models for inferring damage in the surveilled material | MPC Omega – analytical formula to relate creep rate to damage | Damage inference using established creep-fatigue damage model | Damage inference with no assumption on damage model                    |
| Remaining life determination and acceptance assessment | Remaining life (time to expected failure)                     | Remaining life (cycles to expected failure)                   | Remaining life (cycles to failure) assuming linear damage accumulation |

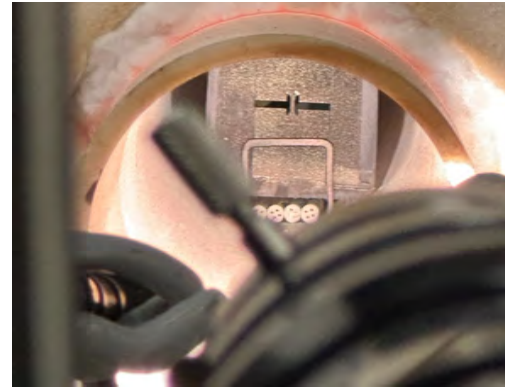
# Creep-Fatigue Remaining Life Assessment

- **Knowns:**

1. Original sample response before in-reactor service (irradiation and corrosion) – for example furnace test an instrumented specimen
2. Mechanical response after in-reactor service – furnace test an instrumented sample for a few cycles

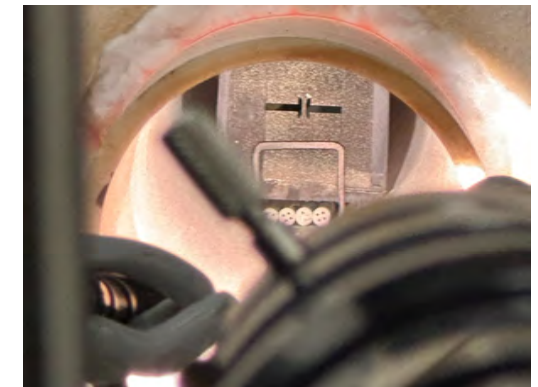
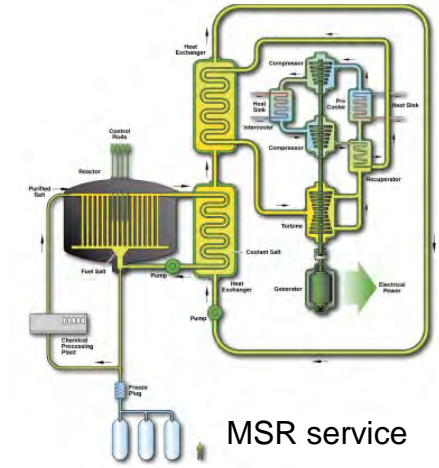
- **Unknowns:**

1. Mechanical response while in service
2. Amount of material property degradation/damage



Furnace test samples *before* MSR service – establish baseline mechanical properties

Can we infer how much damage the sample accumulated?



Furnace test samples *after* MSR service – establish damaged mechanical properties





Thank you

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