



# NEUP Program

Experiments for Modeling and Validation of Liquid-Metal Heat Pipe Simulation Tools for Micro-Reactors

March 04, 2022

**Yassin. A. Hassan** | Texas A&M University

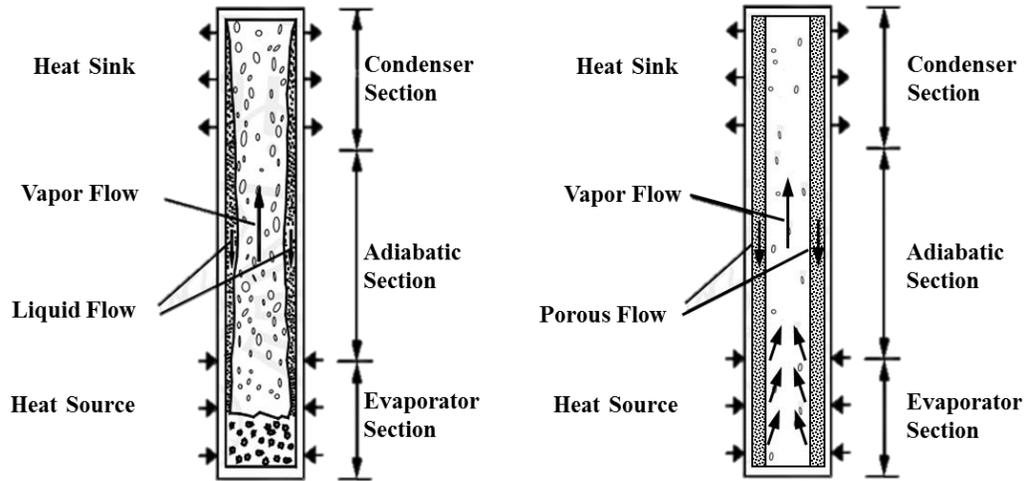
**Joseph Seo** | Texas A&M University

**Daeguen Kim** | Texas A&M University

**Hansol Kim** | Texas A&M University

**Rodolfo Vaghetto** | Texas A&M University

# Overview of the Project



- The heat pipe is a device of very high conductance
- It works passively on the principle of evaporation and condensation of a working fluid so that it can transfer large amount of heat.
- Intensive studies to apply the heat pipe as a primary heat transfer system of the micro-reactor have been pursued.

Single heat pipe test in MAGNET experimental station in INL.



Spacecraft

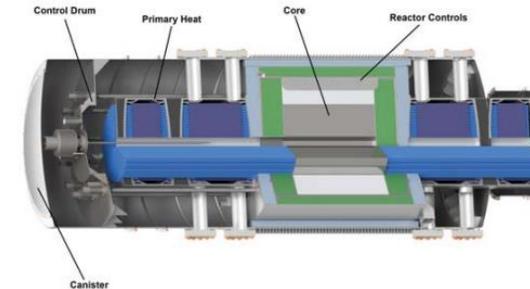


Spacecraft, heat pipes in computer, Alaska pipeline support legs cooled by heat pipe thermosyphons to keep permafrost frozen.  
From: Heat pipe – Wikipedia and wall.alphacoders.com

Computer

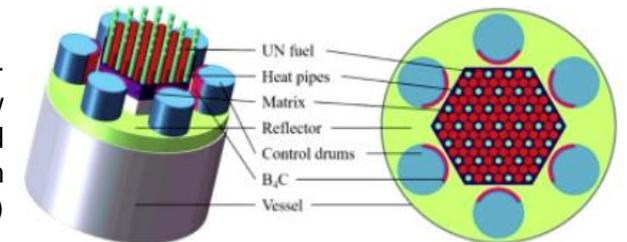


Pipeline



Design of e-Vinci from Westinghouse

Wang et al., Thermal-hydraulic analysis of a new conceptual heat pipe cooled small nuclear reactor system (2018)



# Overview of the Project

**Purpose:** The proposed work aims to produce **high-fidelity liquid-metal heat-pipe experimental data** for the validation of the simulation tool, Sockeye, through both single heat-pipe and integrated heat-pipe experiments.

## Objectives:

### ▪ Single Heat-Pipe Hydraulic Experiment

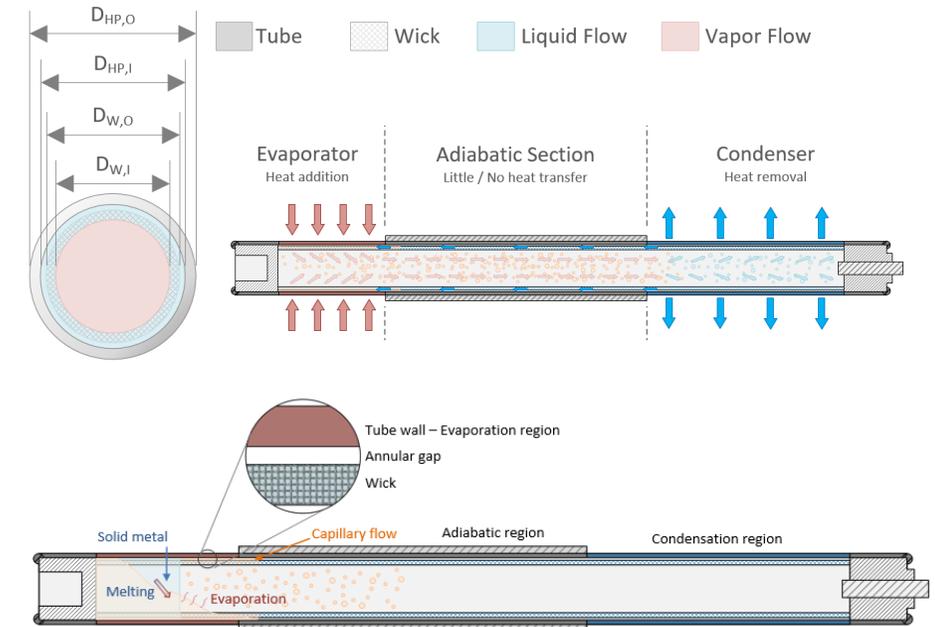
Measurements of **the hydraulic resistance for validation / development of wall friction, wick friction/form loss models.**

### ▪ Single Liquid-Metal Heat-Pipe Experiment

Measurements of **internal temperature, pressure, and phase distribution** for validation/development of heat transfer and flow models in Sockeye.

### ▪ Multiple Liquid-Metal Heat-Pipes Experiment in Hexagonal Arrangement

Investigate the integrated system performance under various operational scenarios such as partial failure of constituent heat pipes and non-uniform cooling/heating.



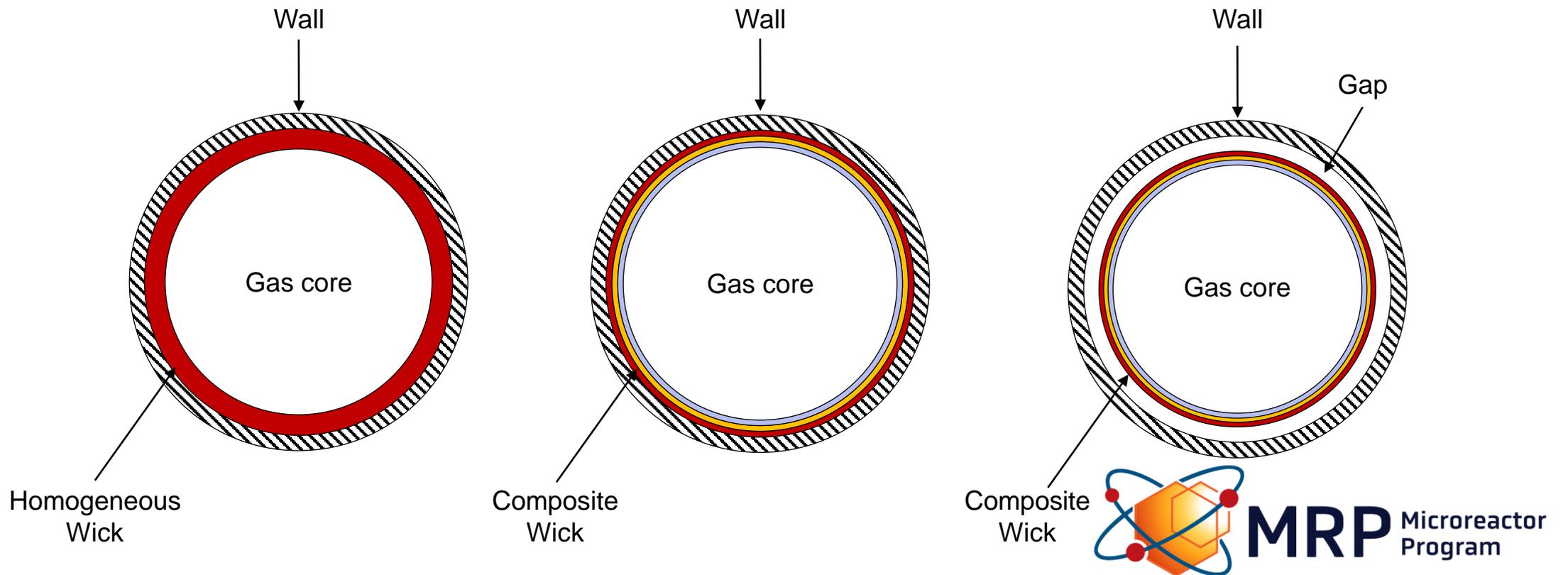
Sodium heat pipe with targeted design

## ➤ Experiments at TAMU

- **Wick Characteristics Experiment**
- Gap Effect Experiment
- Capillary Rising Modeling
- Heat Pipe Fabrication and Experiment
- Heat Pipe Measurement
- Heat Pipe Visualization

# Introduction

- Pore radius, or pore size, is an average size of voids inside the porous media. This parameter should be small to acquire a large capillary pressure difference between the evaporator and condenser region.
- For a heat pipe, the permeability is a parameter of the wick resistance to the liquid flow along the pipe axial direction. Large permeability is needed for achieving a small liquid pressure drop along the wick structure.
- Having a low pore radius and a high permeability is hard to achieve in most homogeneous wick designs (Optimization/Tradeoff problem).
- The composite wick structures provide high capillary pressure by having small pores, while gaining high permeability from large size pores.
- The other way to overcome the tradeoff problem is to introduce an extra flow path for liquids other than wick structures.



# Operating Limitation of the Interest

## Capillary limitation

During heat pipe operation, the working fluid evaporates in the evaporator and condenses in the condenser, transporting the latent heat from one end of the heat pipe to the other.

The liquid condensate is passively returned to the evaporator by capillary forces in the wick.

The maximum power that the heat pipe can transport and still **return the condensate by capillary forces** is the capillary limit.

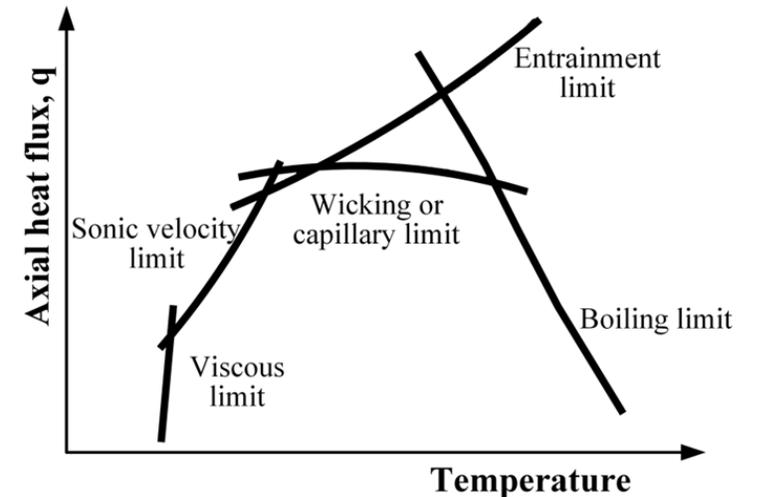
$$\Delta P_c > \Delta P_g + \Delta P_v + \Delta P_l$$

$\Delta P_c$ : Capillary force generated in the wick

$\Delta P_g$ : Pressure drop due to gravitation and acceleration

$\Delta P_l$ : Liquid pressure drop in the wick

$\Delta P_v$ : Fractional pressure drop in the vapor



# Operating Limitation of the Interest

## Capillary limitation

$\Delta P_c$ : Capillary force generated in the wick

$$\Delta P_c = \frac{2\sigma}{r_{eff}}$$

$\Delta P_g$ : Pressure drop due to gravitational acceleration

$$\Delta P_g = (\rho_l - \rho_v) gh$$

$\Delta P_l$ : Liquid pressure drop in the wick (Darcy's law)

$$\Delta P_l = \frac{\dot{m}\mu L}{\rho_l KA_{wick}} = \frac{q}{h_{lv}} \frac{\mu L}{\rho_l KA_{wick}}$$

$K$ : Permeability

$A_{wick}$ : Wick cross-sectional area

$\Delta P_v$ : Fractional pressure drop in the vapor

$$\Delta P_v = \frac{f\rho_v u_v^2 L}{D_v}$$

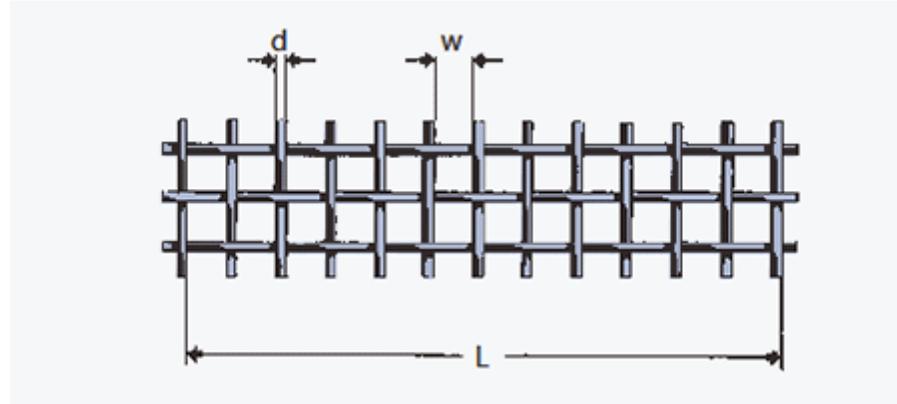
$f$ : Fanning friction factor

$$\Delta P_c > (\rho_l - \rho_v) gh + \frac{q}{h_{lv}} \frac{\mu L}{\rho_l KA_{wick}} + \frac{f\rho_v u_v L}{D_v}$$

$$q_c < \frac{h_{lv}\rho_l KA_{wick}}{\mu L} \left[ (\rho_l - \rho_v) gh + \frac{f\rho_v u_v L}{D_v} - \Delta P_c \right]$$

# Wick characteristics – Single Layer

Metal screen mesh wicks



Wick type	Wire diameter, d [mm]	Opening size, W [mm]	Opening area	$r_{eff}$ [mm] (W+d)/2	Mesh number, N=1/(W+d)	Porosity $\phi$ [-]	Permeability K[m <sup>2</sup> ]
60 x 60	0.1905	0.1397	12%	0.1651	3.028468	0.524	1.89E-10
100 x 100	0.1143	0.1524	30%	0.13335	3.749531	0.647	2.32E-10
200 x 200	0.04064	0.08636	46%	0.0635	7.874016	0.736	7.76E-11
200 x 200	0.05334	0.07366	34%	0.0635	7.874016	0.654	5.44E-11
400 x 400	0.0254	0.0381	38%	0.03175	15.74803	0.670	1.46E-11
500 x 500	0.02032	0.03048	36%	0.0254	19.68504	0.670	9.38E-12

# Test Matrix

The wick combining coarse and fine wick have superior performance since heat pipe performance requires high capillary pressure, and yet still offer low resistance to fluid flow\*

Case	Type	Pore radius, d (um)	Porosity, $\epsilon$	Permeability, K (m2)	Capillary Pressure (Pa)	Maximum Heat input (W)
1	100-mesh (6 wraps)					
2	400-mesh (6 wraps)					
3	60-mesh (6 wraps)					
4	100-mesh (2 wraps), 400-mesh (2 wraps), 60-mesh (2 wraps)					
5	100-mesh (1 wraps), 400-mesh (3 wraps), 60-mesh (2 wraps)	<b>Measured by EXP.</b>				
6	100-mesh (2 wraps), 400-mesh (3 wraps), 60-mesh (1 wraps)					
7	100-mesh (2 wraps), 400-mesh (1 wraps), 60-mesh (3 wraps)					
8	100-mesh (3 wraps), 400-mesh (2 wraps), 60-mesh (1 wraps)					
9	100-mesh (3 wraps), 400-mesh (1 wraps), 60-mesh (2 wraps)					

Calculated from theoretical models

\* Mwaba et al., "Influence of wick characteristics on heat pipe performance", 2006, Carleton University



# Porosity Measurement

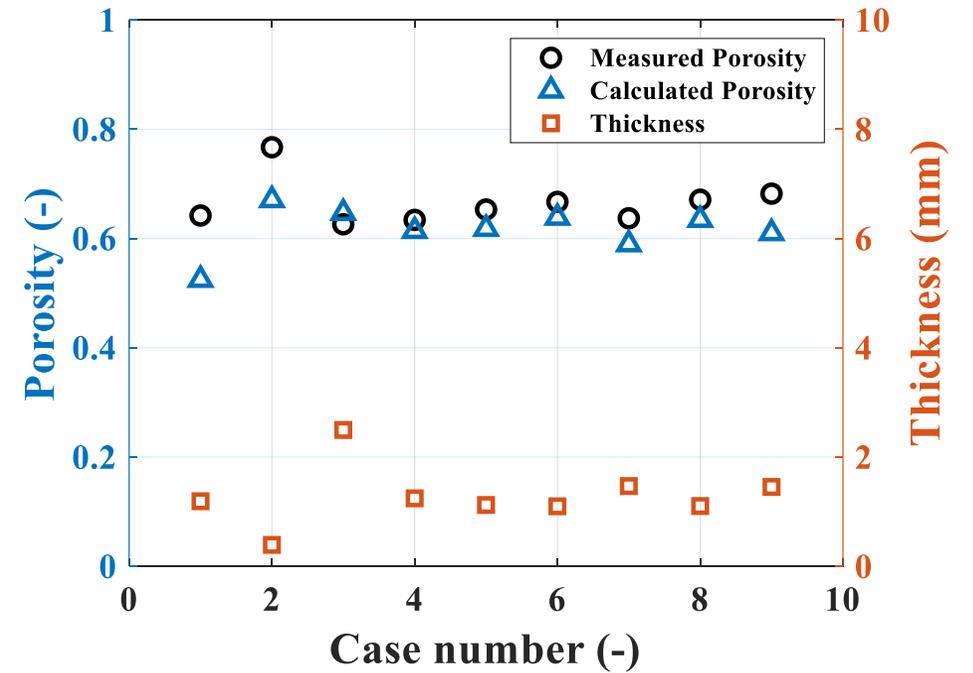


$m_{wick}$



$m_{wick} + m_l$

Porosity of the mesh:  $\frac{1}{\varepsilon} = 1 + \frac{m_{wick}\rho_l}{m_l\rho_{wick}}$



# Wick Characteristics Experiment

The wick with the best performance

composite wick structures were characterized

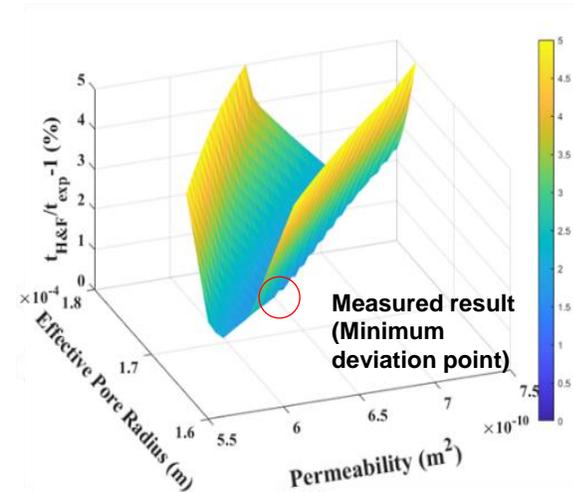
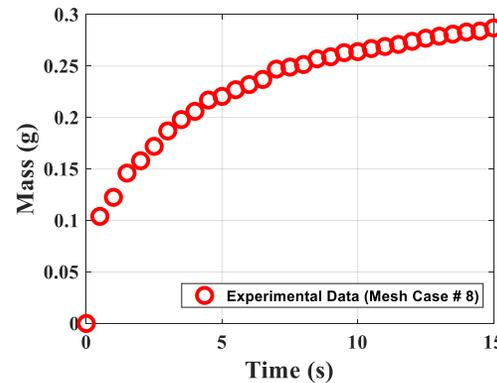
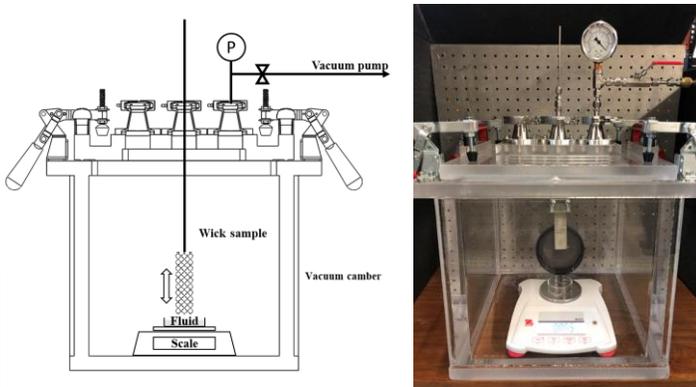
## Porosity measurement



Porosity is calculated from the mass and density of the liquid filling void space of the mesh.

Case #	Total number of layers	Mesh composition			Measurement result			
		100-mesh (inside layer)	400-mesh (middle layer)	60-mesh (outside layer)	Porosity ( $\epsilon$ [-])	Permeability ( $K$ [ $\mu\text{m}^2$ ])	Effective Pore Radius ( $r_{eff}$ [mm])	$\frac{K}{r_{eff}}$ [ $\mu\text{m}$ ]
1	6	6	0	0	0.642	$0.815 \times 10^3$	0.266	$3.064 \times 10^3$
2		0	6	0	0.767	$0.825 \times 10^3$	0.232	$3.556 \times 10^3$
3		0	0	6	0.626	$0.745 \times 10^3$	0.419	$1.778 \times 10^3$
4		2	2	2	0.634	$0.985 \times 10^3$	0.252	$3.909 \times 10^3$
5		1	3	2	0.653	$1.435 \times 10^3$	0.213	$6.737 \times 10^3$
6		2	3	1	0.667	$1.205 \times 10^3$	0.264	$4.564 \times 10^3$
7		2	1	3	0.637	$0.300 \times 10^3$	0.188	$1.596 \times 10^3$
8		3	2	1	0.671	$0.635 \times 10^3$	0.169	$3.757 \times 10^3$
9		3	1	2	0.682	$1.080 \times 10^3$	0.284	$3.803 \times 10^3$

## Permeability and effective pore radius measurement

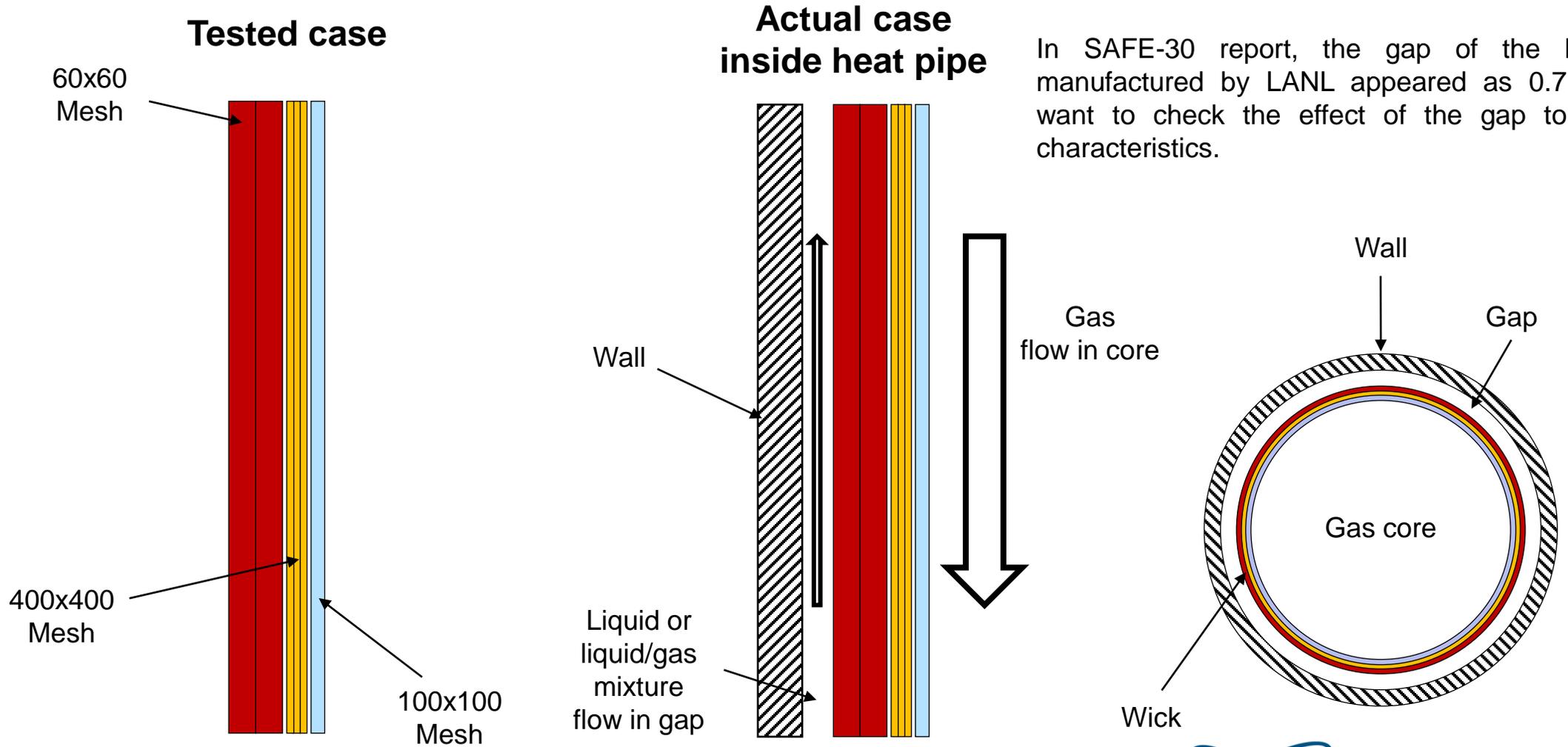


The method by Holley and Faghri (2005) is used.

## ➤ Experiments at TAMU

- Wick Characteristics Experiment
- **Gap Effect Experiment**
- Capillary Rising Modeling
- Heat Pipe Fabrication and Experiment
- Heat Pipe Measurement
- Heat Pipe Visualization

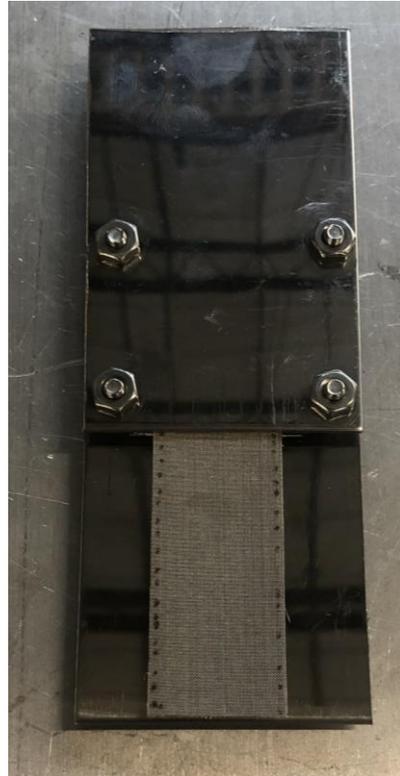
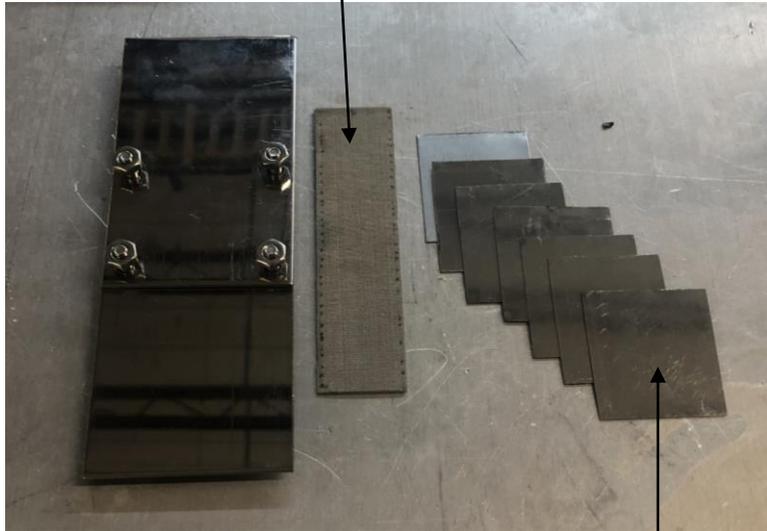
# Wall Effect Investigation



In SAFE-30 report, the gap of the heat pipe manufactured by LANL appeared as 0.7 mm. We want to check the effect of the gap to the wick characteristics.

# Wall Effect Experimental Setup

Wick type #5  
6-layered composite screen mesh



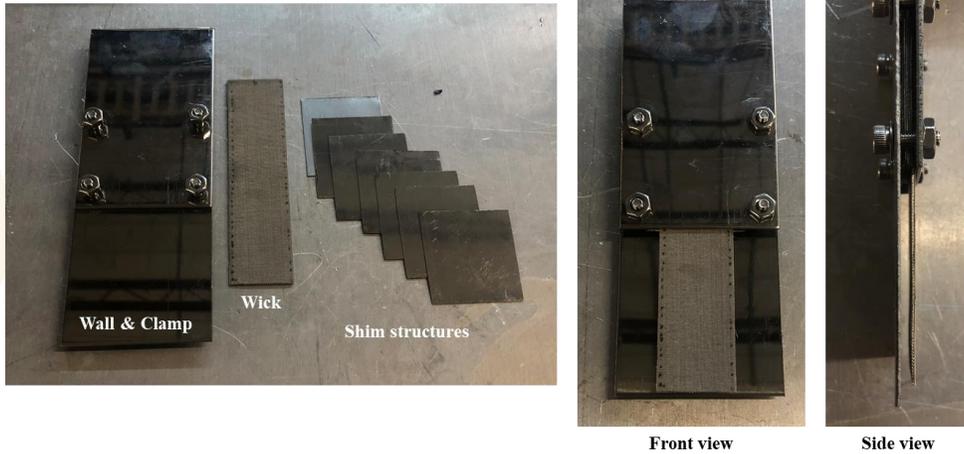
Shim structures with varying thickness  
to control the size of the gap

A Simple setup was prepared to measure permeabilities of a wick structure with different sizes of gap (0.0 mm ~ 30.0 mm) between stainless steel wall and the screen mesh.

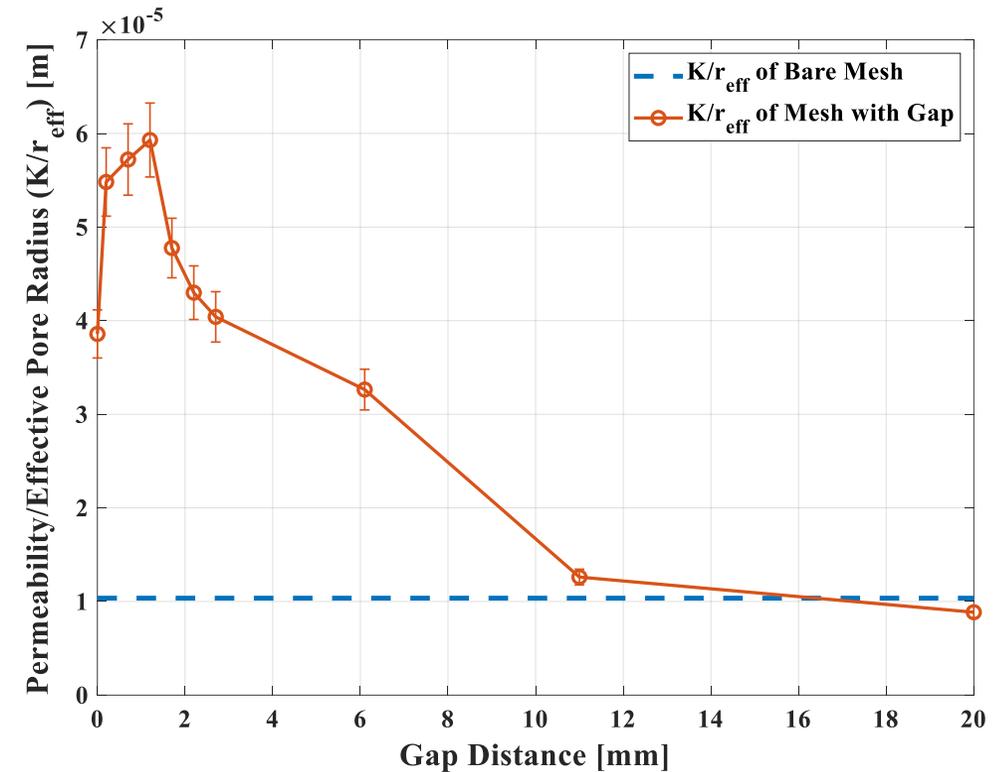
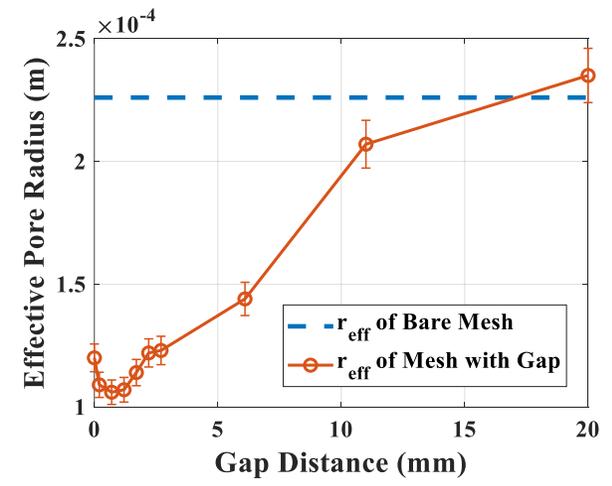
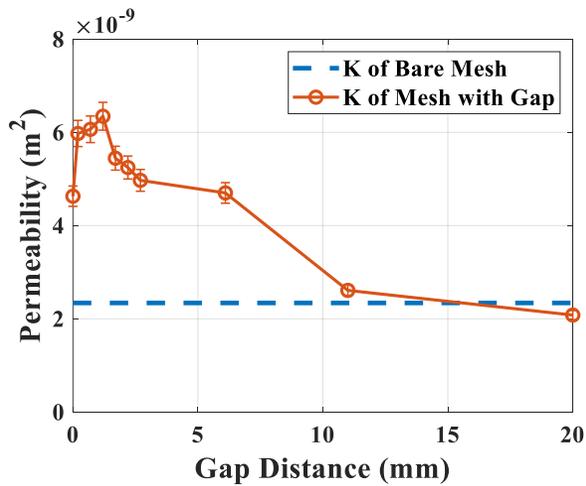
The same method with previous study was utilized.

# Gap Effect Experiment

Wick assembly with adjustable gap between the wall



Wick samples were prepared to measure permeabilities and effective pore radius with different sizes of gap (0.0 mm ~ 20.0 mm) between stainless steel wall and the screen mesh.



Optimal distance of the gap for the annular type heat pipe was found

The result of the measurement is plotted vs. the gap distance.

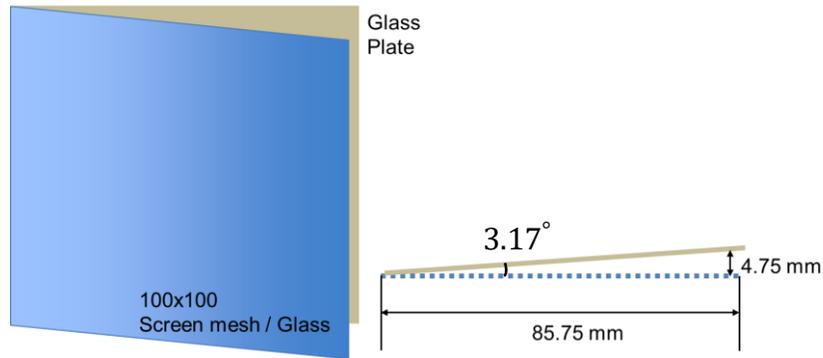
An interesting trend can be found from the result. The  $K/R_{eff}$  increases as the gap increase, a peak at 0.7 to 1.2 mm is observed. As the gap continues to increase, the permeability falls the bare mesh case.

## ➤ Experiments at TAMU

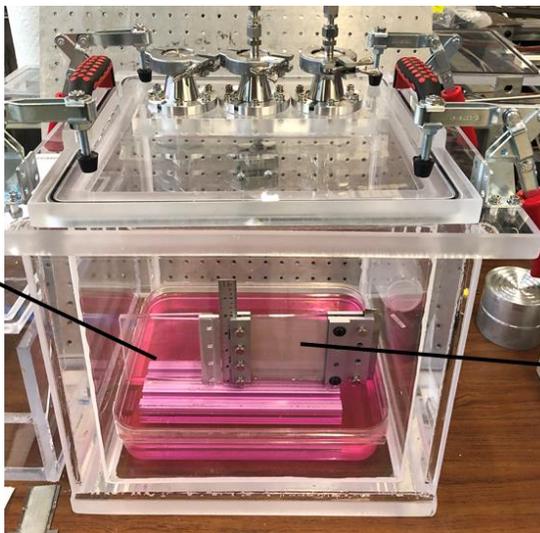
- Wick Characteristics Experiment
- Gap Effect Experiment
- **Capillary Rising Modeling**
- Heat Pipe Fabrication and Experiment
- Heat Pipe Measurement
- Heat Pipe Visualization

# Capillary Rising Modeling

Experimental setup of angled mesh-plate experiment



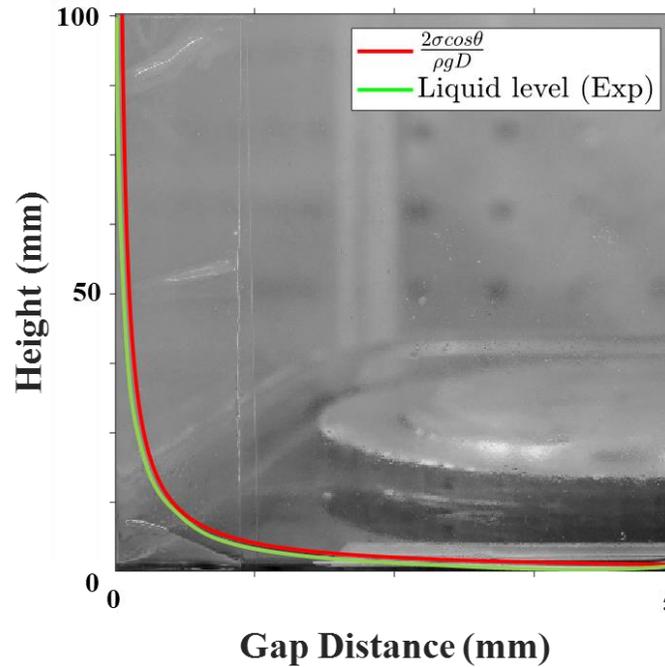
Glass/ Glass



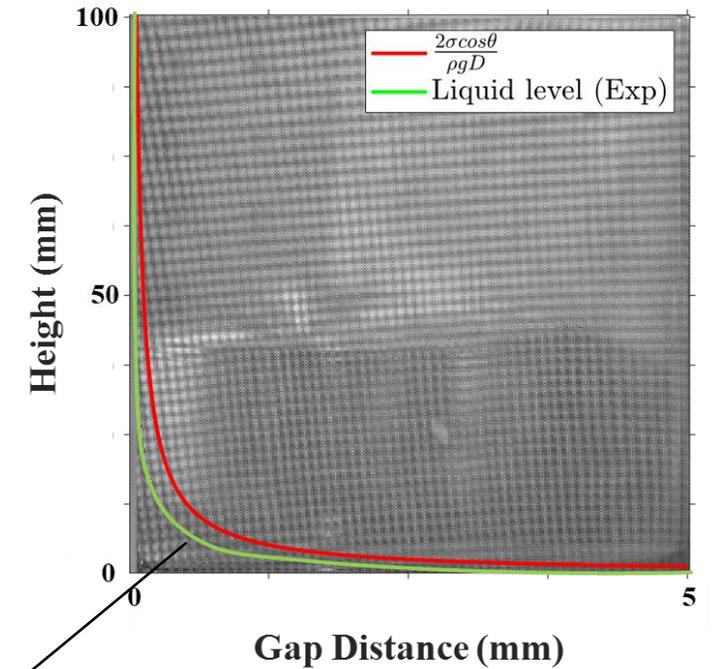
Glass/ Mesh

Contact angle of ethanol on a glass surface

Glass/Glass experiment ( $\theta = 30^\circ$ )



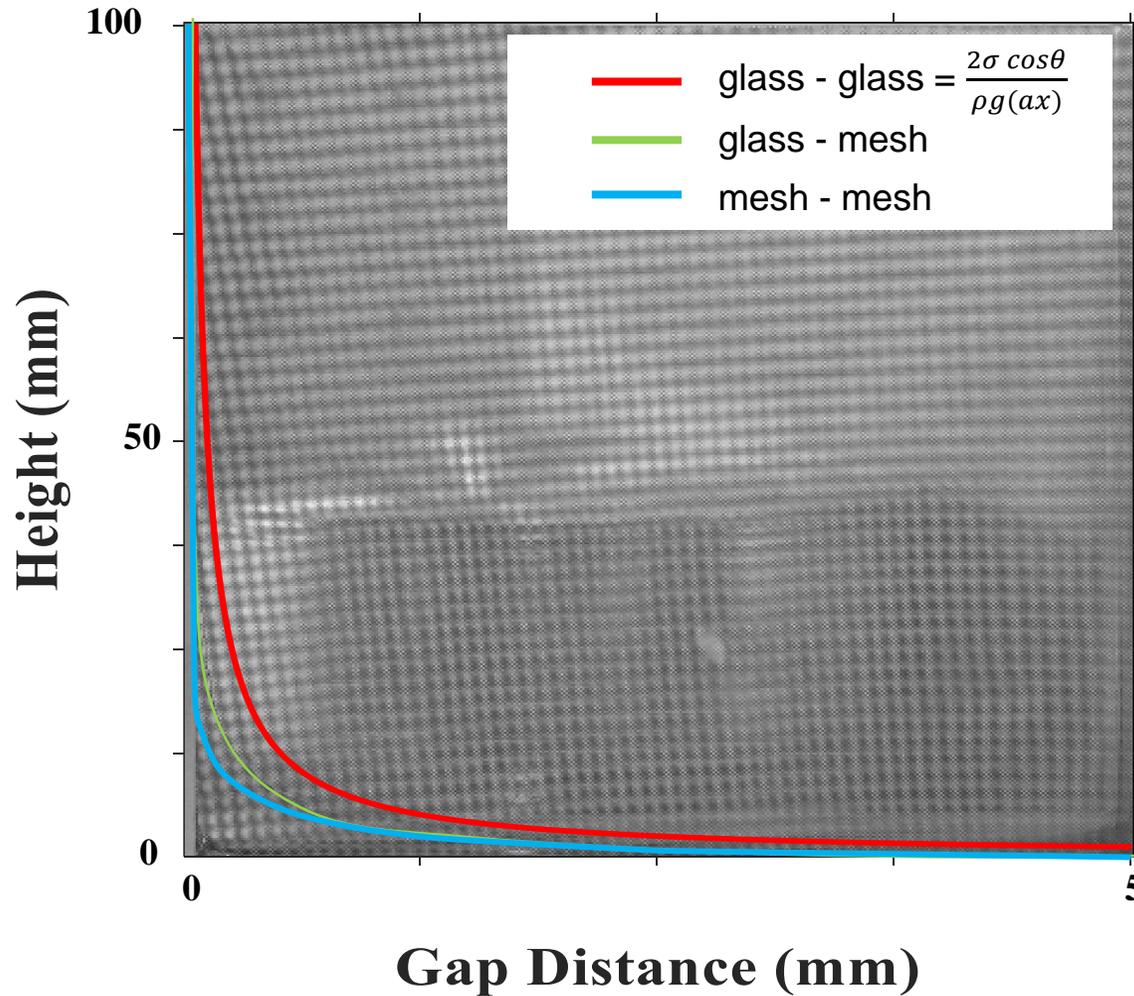
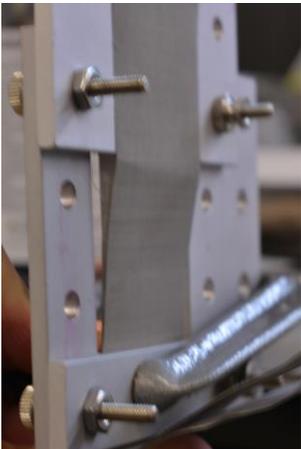
Glass/Mesh experiment ( $\theta = 30^\circ$ )



The rising height of the liquid in a gap between solid/mesh differs from solid/solid case. There is no study on the capillary pressure acting on solid surface/mesh surface. The result might be useful to model the gap effect.

# Capillary Rising Modeling

Mesh-mesh Exp.



Mesh-mesh graph is smaller than glass-mesh.

According to the formula, height is

$$h = \frac{\sigma (\cos\theta_0 + \cos\theta_1)}{\rho g(w)}$$

(where  $\theta_0$  = glass contact angle and  $\theta_1$  = mesh contact angle),

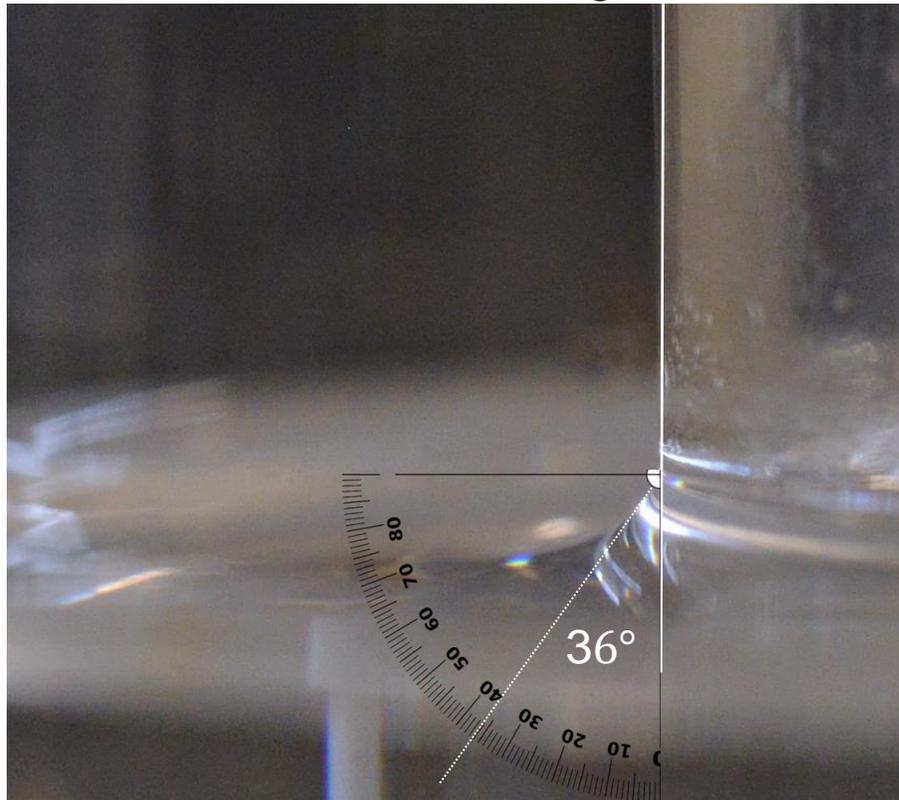
Therefore,

$$\cos\theta_1 < \cos\theta_0, \theta_0 < \theta_1$$

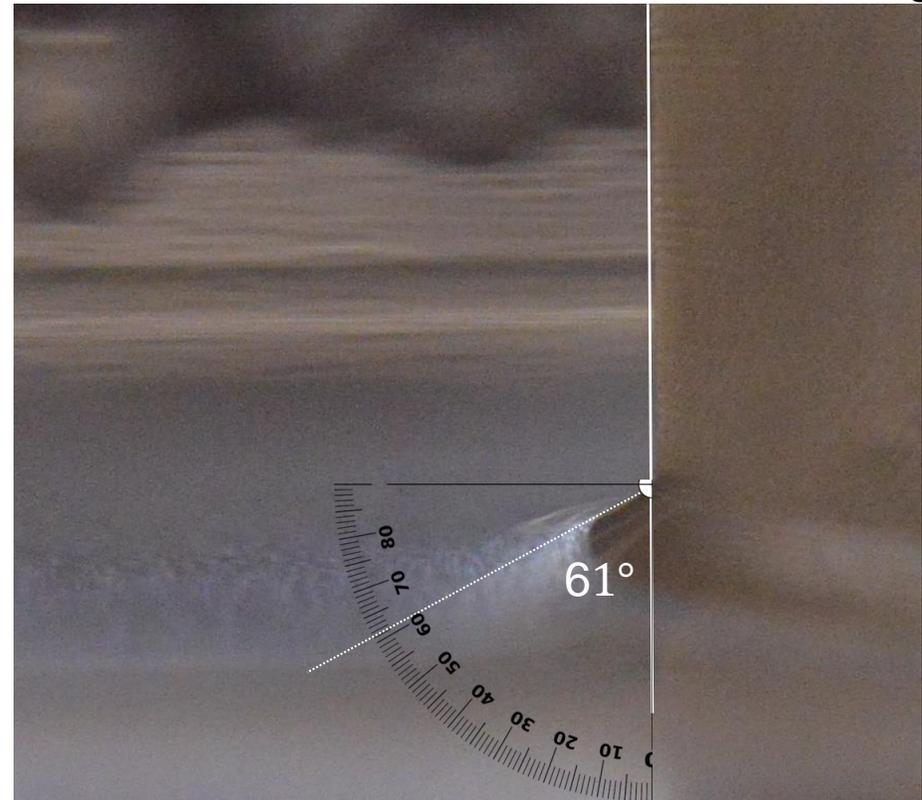
Glass contact angle with ethanol  $\theta_0$  is about  $30^\circ (\pi/6)$ , then **Mesh** contact angle with ethanol would be larger than  $30^\circ$

# Contact Angle Measurement

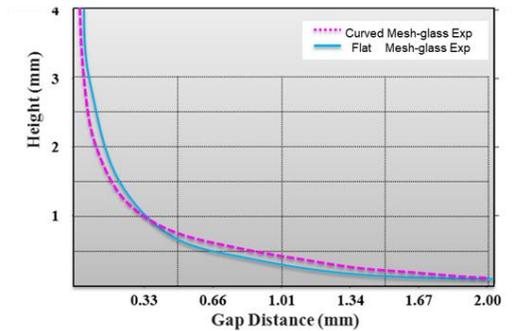
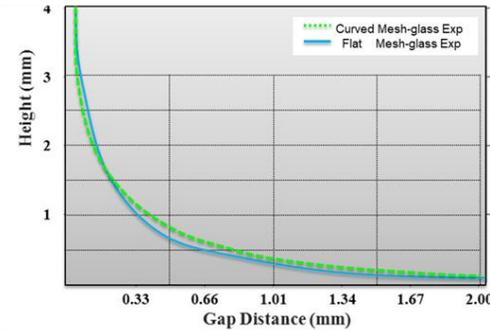
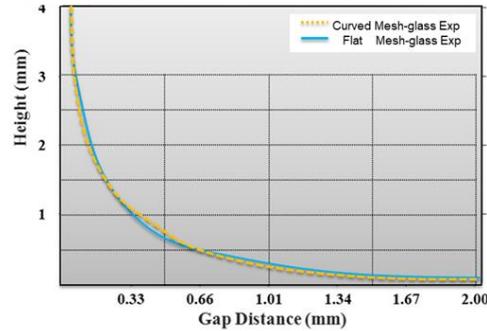
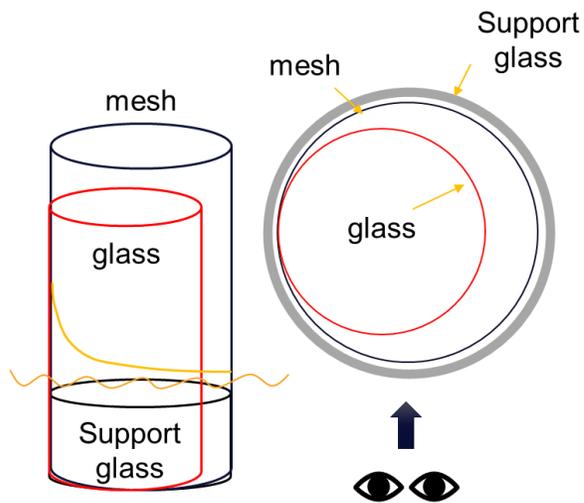
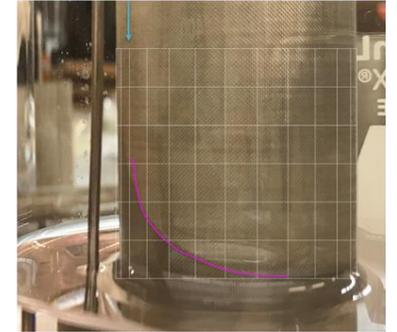
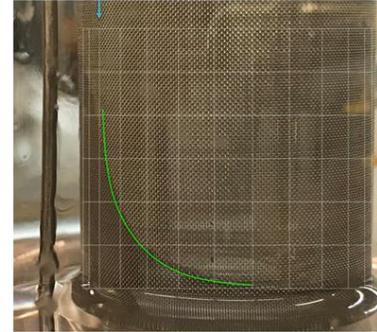
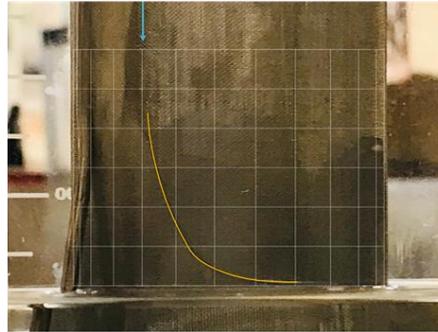
Glass – Ethanol contact angle



Stainless steel mesh – Ethanol contact angle



# Curvature Effect



## ➤ Experiments at TAMU

- Wick Characteristics Experiment
- Gap Effect Experiment
- Capillary Rising Modeling
- **Heat Pipe Fabrication and Experiment**
- Heat Pipe Measurement
- Heat Pipe Visualization

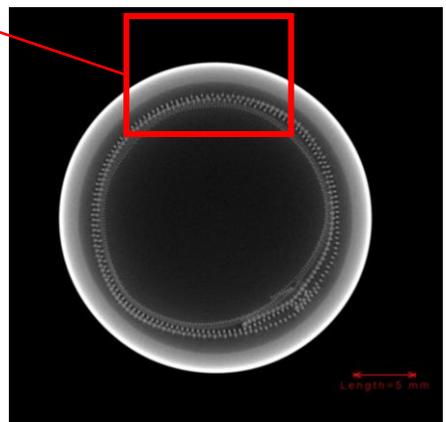
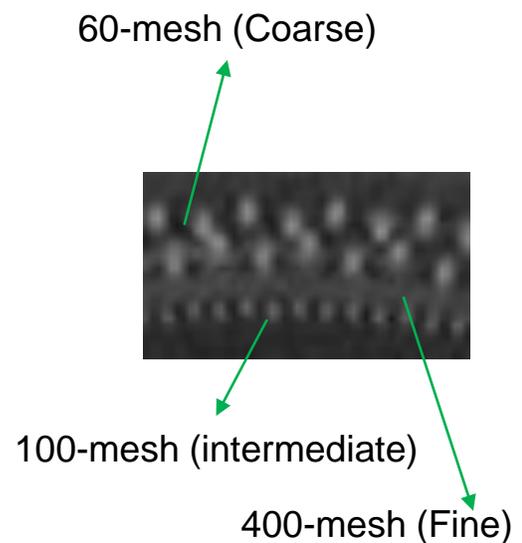
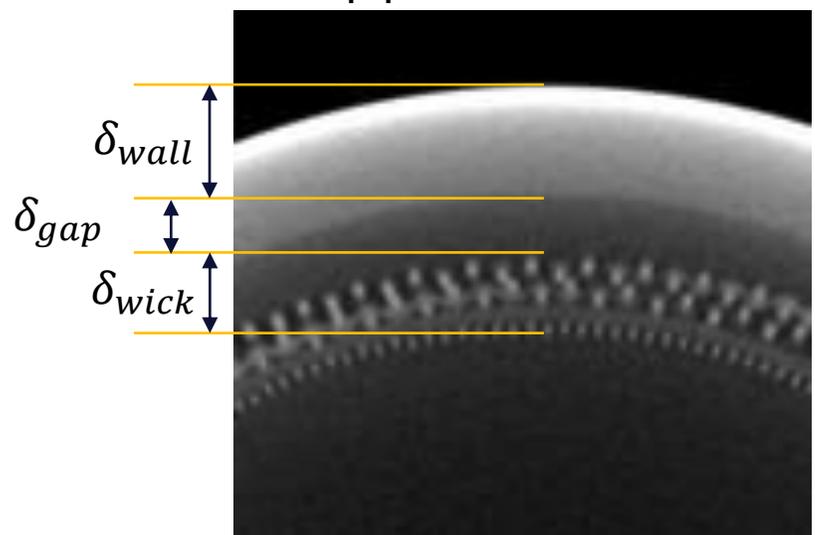
# Stainless Steel Heat Pipe



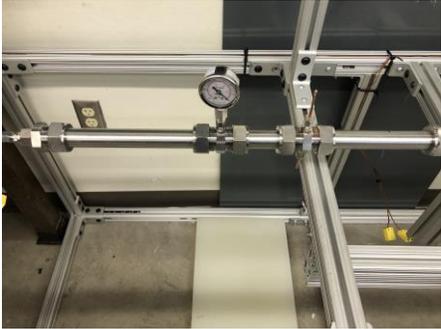
Multi-layered composite screen wick mesh was fabricated.



Micro CT scanning of the heat pipe cross-section



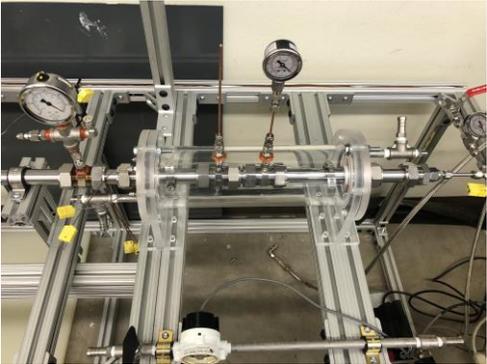
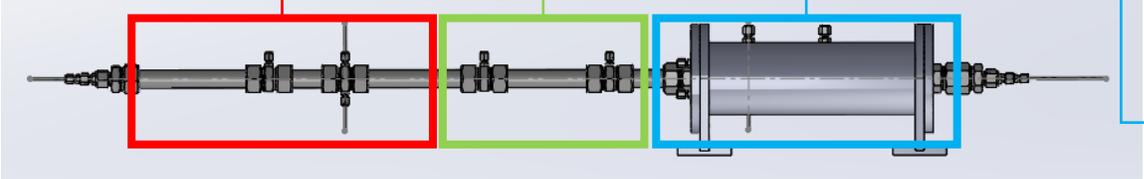
# Heat Pipe Experimental Facility



Evaporator



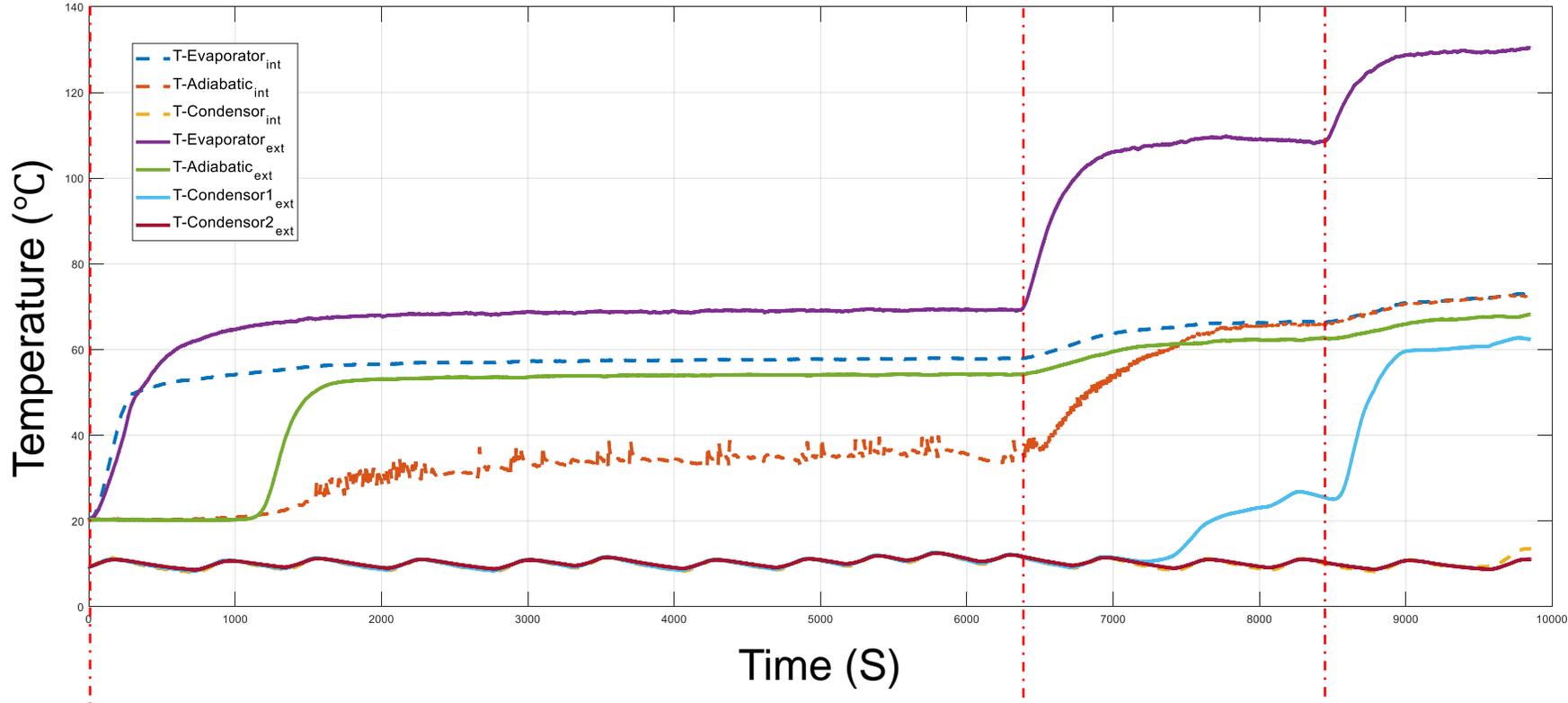
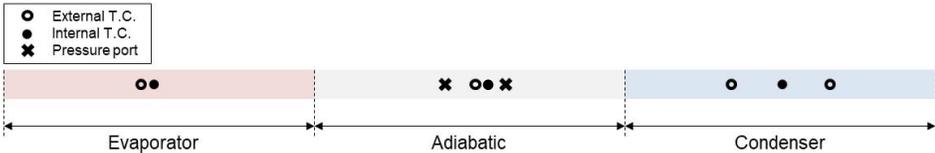
Adiabatic Region



Condenser



# Shakedown Test



Initiate, P = 140.4 W

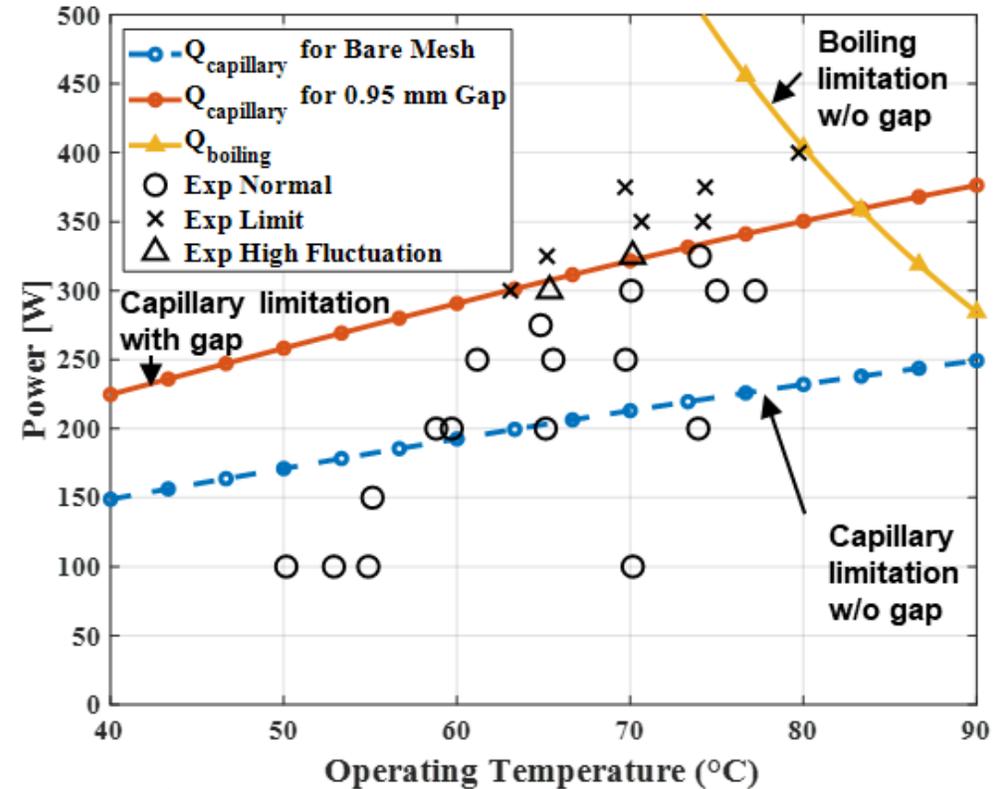
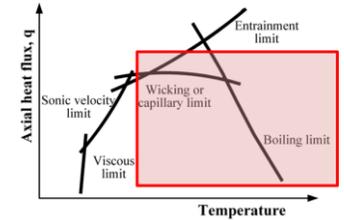
P = 234.0 W

P = 280.8 W

# Heat Pipe Fabrication and Experiment

$$Q_{capillary.gap} = G \cdot Q_{capillary} = G \frac{2\sigma}{r_{eff}} \frac{KA_{wick} h_{lv} \rho_l}{\mu_l L_{eff}}$$

Gap Distance [mm]	G [-]
0	1.00
0.2	1.42
0.7	1.48
1.2	1.54
1.7	1.24
2.2	1.11
2.7	1.05

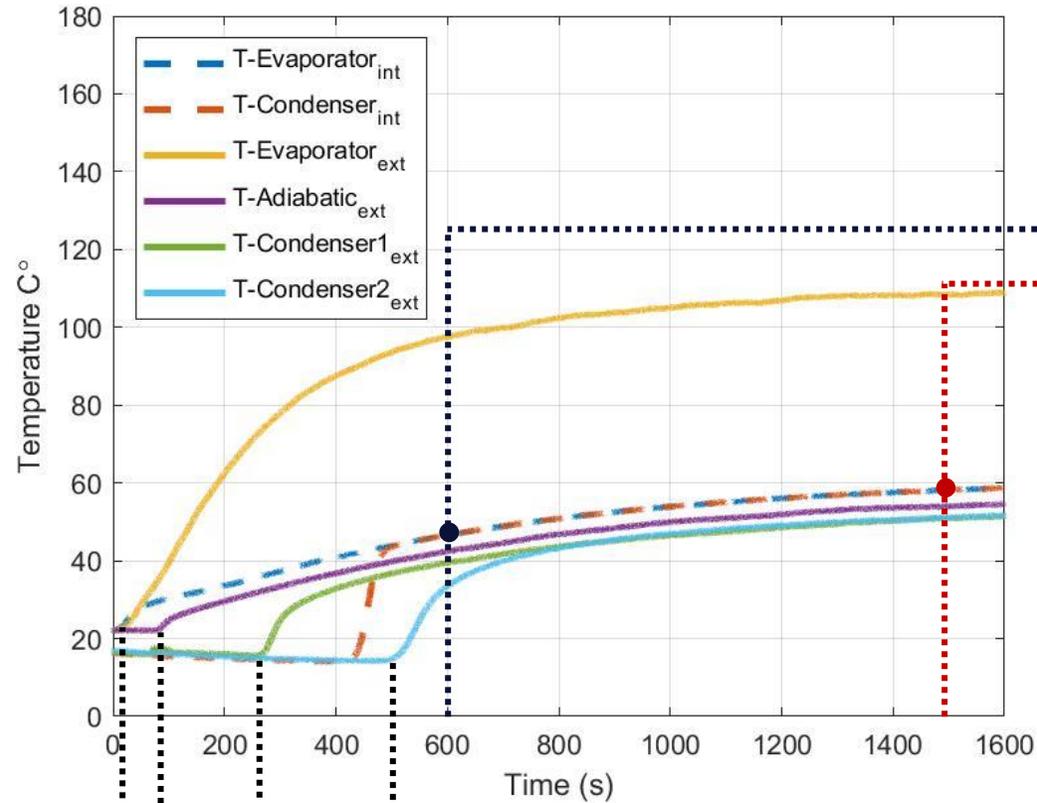
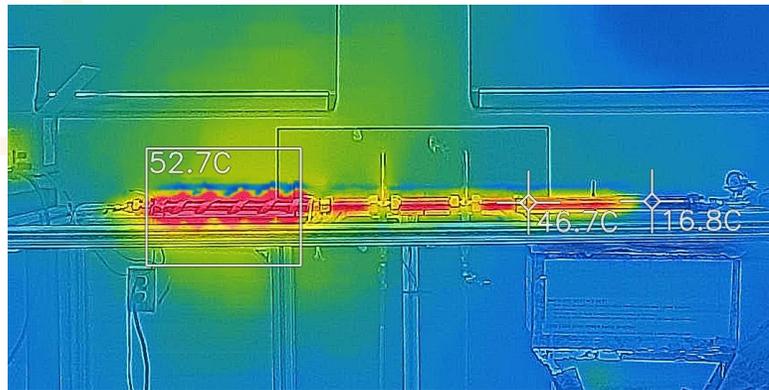


The operating limitation of the heat pipe matches well with the prediction from the result of the wick characterization and gap effect experiment.

## ➤ Experiments at TAMU

- Wick Characteristics Experiment
- Gap Effect Experiment
- Capillary Rising Modeling
- Heat Pipe Fabrication and Experiment
- **Heat Pipe Measurement**
- Heat Pipe Visualization

# Temperature Measurement System

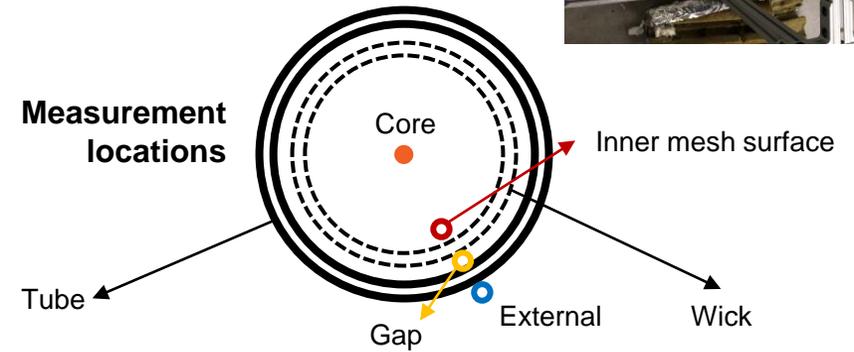


Temperature (C)	Pressure (MPa)	Density (kg/m <sup>3</sup> )
0.028556	0.00061248	999.79
46.974	0.010612	989.33
60.711	0.020612	982.79
69.560	0.030612	977.98
76.223	0.040612	974.08
81.620	0.050612	970.75
86.187	0.060612	967.82
90.161	0.070612	965.19
93.691	0.080612	962.79
96.873	0.090612	960.57
99.777	0.10061	958.51

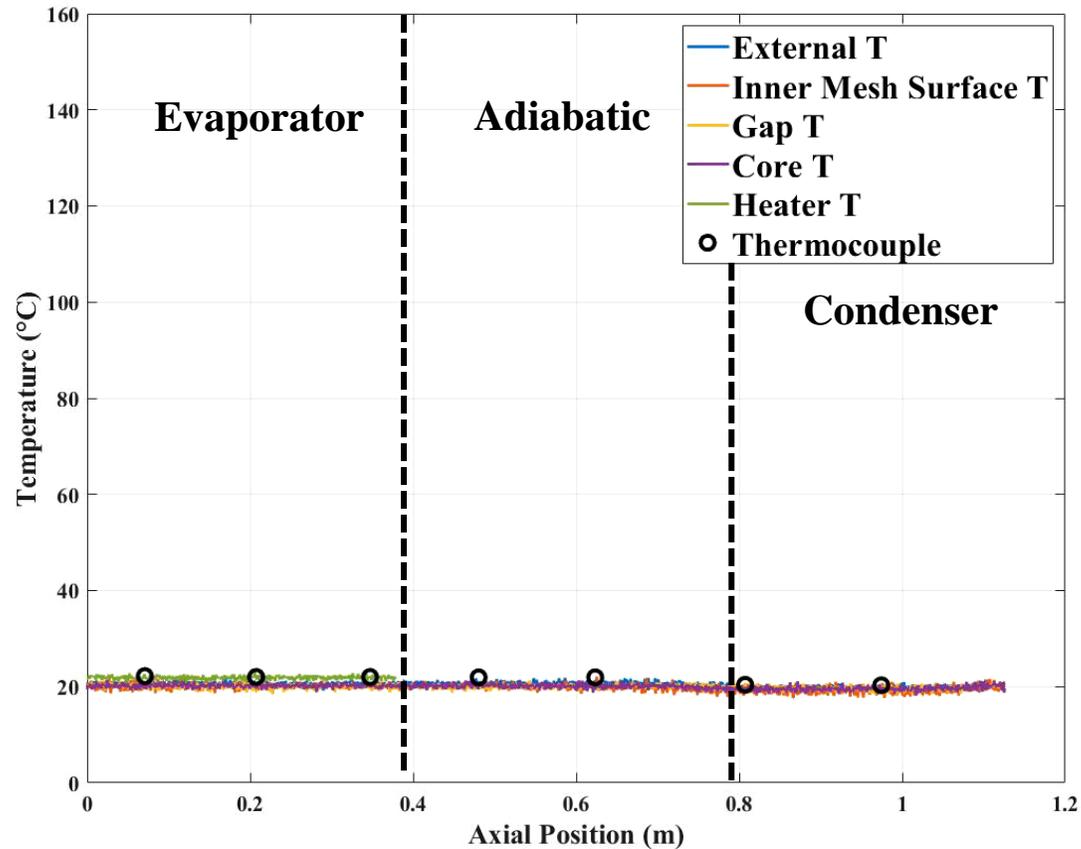


# Distributed Temperature Sensing (DTS)

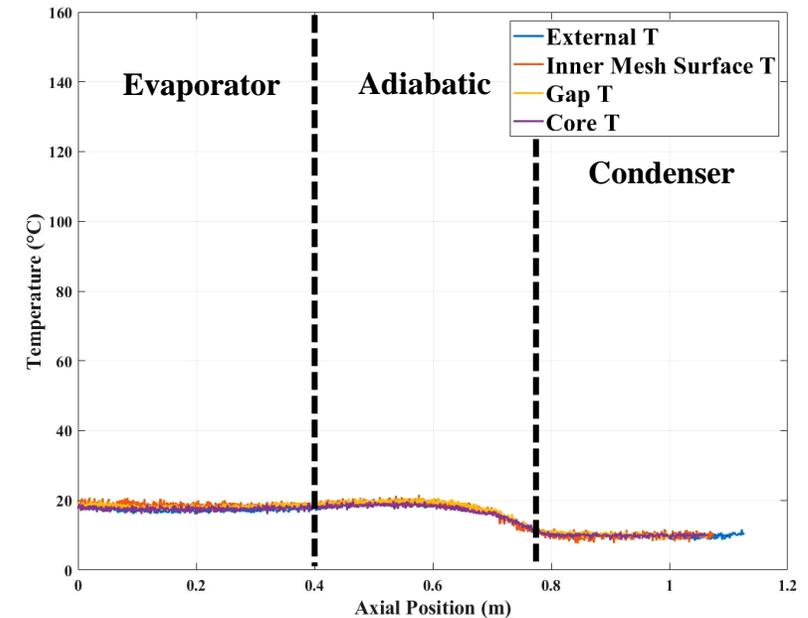
Heater was wrapped on the copper tube for uniform heat transfer to the heat pipe.



Slow start (30W, ~60 mins) of the heat pipe



Rapid start (75W, ~60 mins) of the heat pipe



## ➤ Experiments at TAMU

- Wick Characteristics Experiment
- Gap Effect Experiment
- Capillary Rising Modeling
- Heat Pipe Fabrication and Experiment
- Heat Pipe Measurement
- **Heat Pipe Visualization**

# Flow Visualization of Liquid Metal

TAMU has a capability of transparent heating up to 700 °C and ~101 kW/m<sup>2</sup> of heat flux.



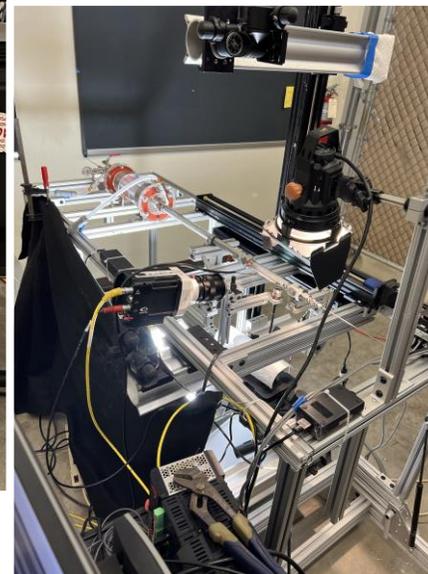
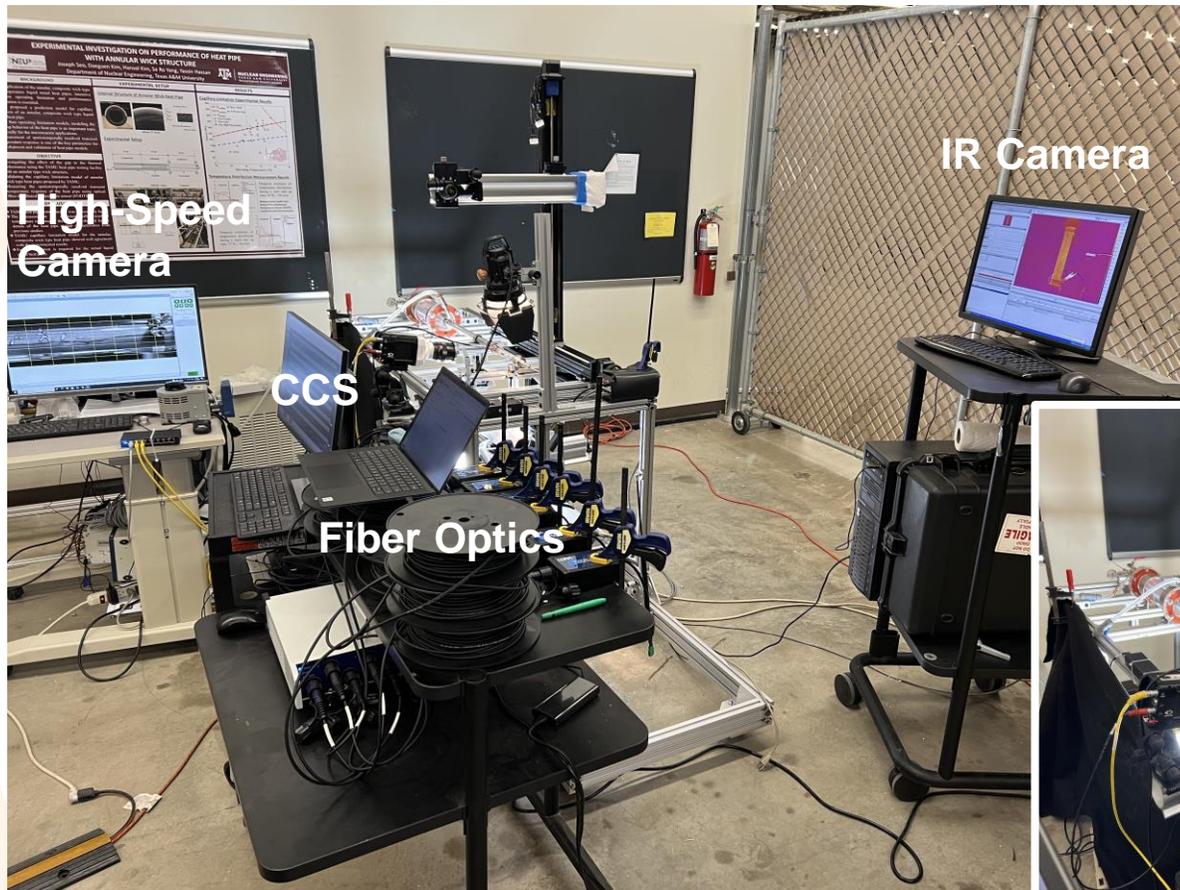
Water boiling experiment using transparent heater.



TAMU is being conducted to perform melting/boiling experiment using the transparent heater.

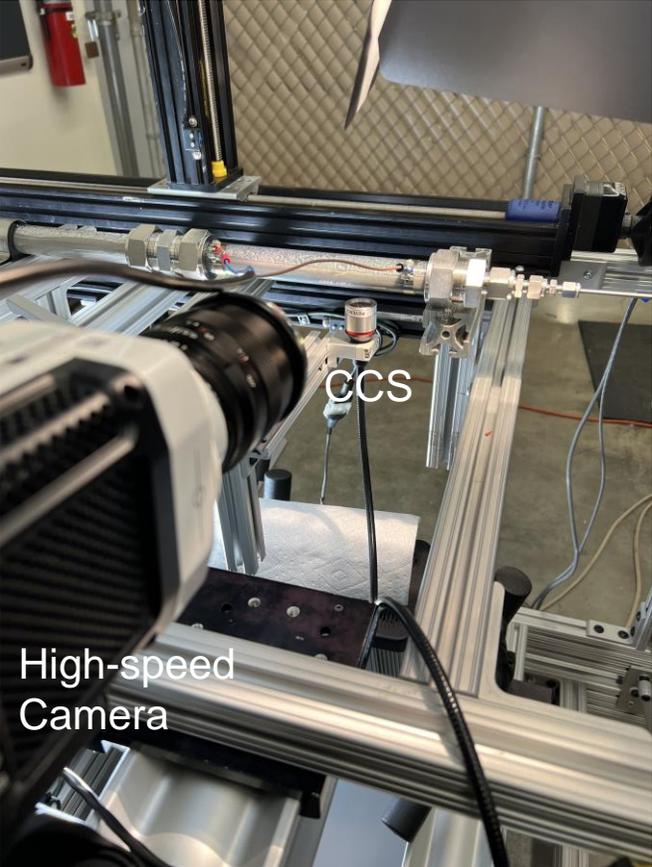
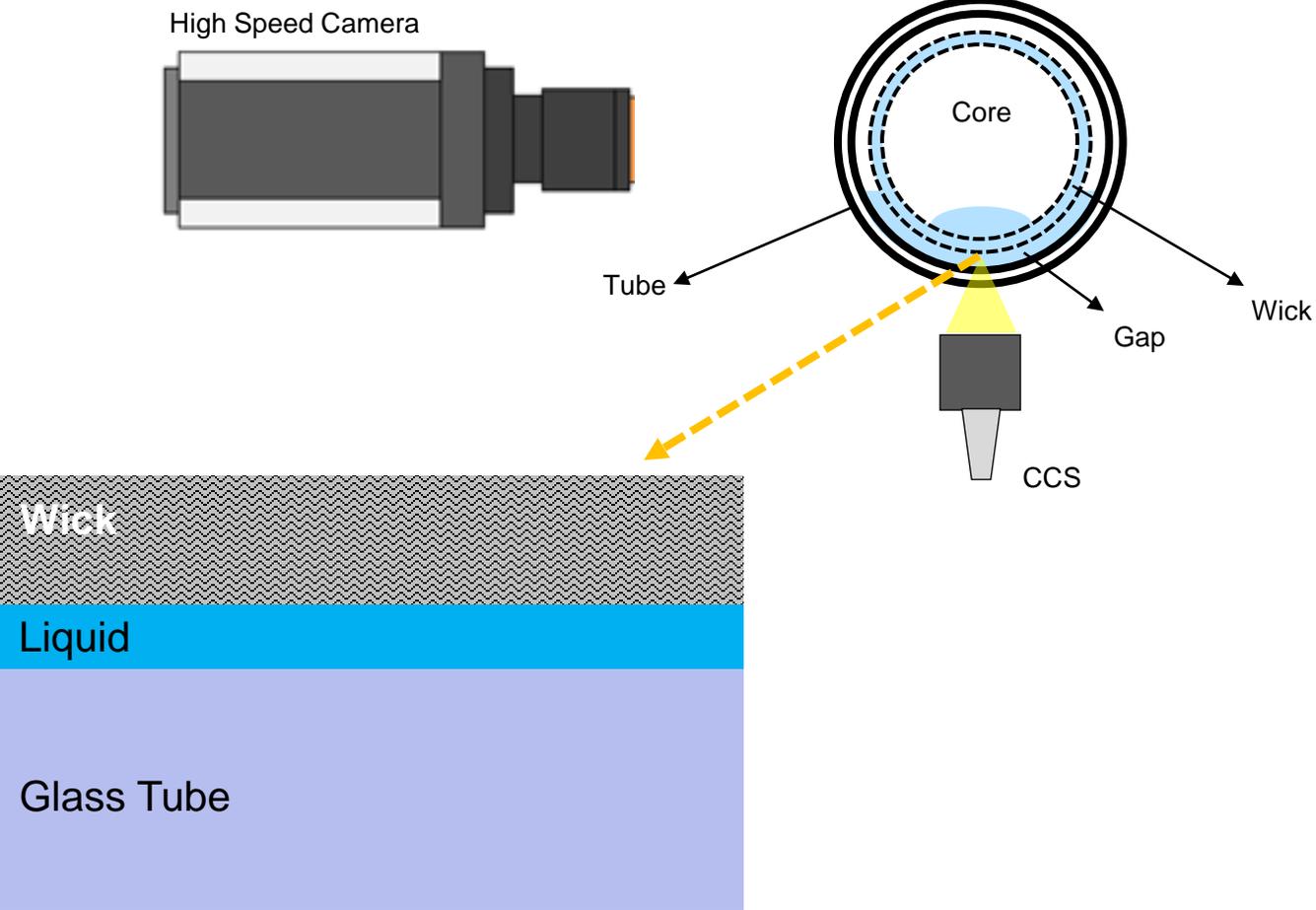
The experiment will allow to obtain information about flow behavior of liquid metal at different operating status of the heat pipe.

# Heat Pipe Visualization Experimental Setup



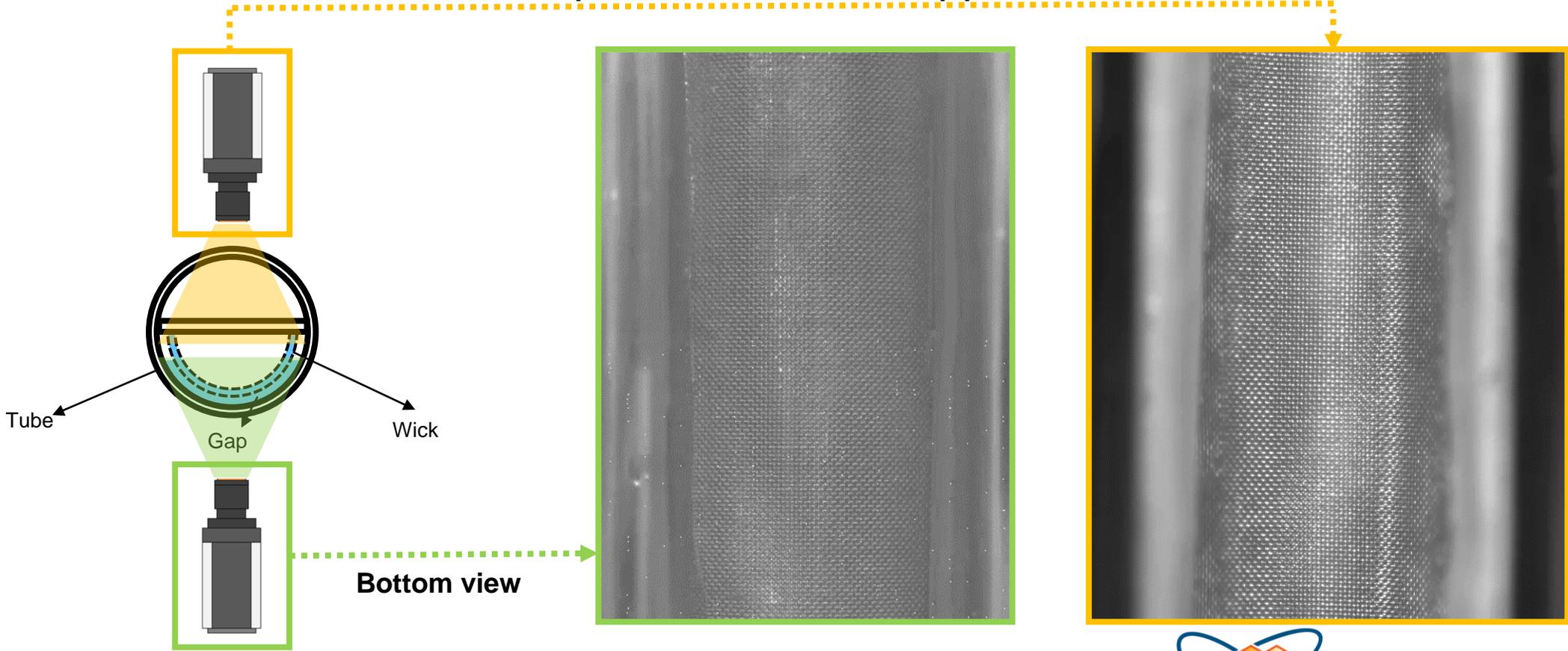
- Visualization using high speed camera and IR camera is conducted.
- Temperature measurement using fiber optical sensor and IR camera is implemented.
- Confocal Chromatic Sensor (CCS) is applied to measure the liquid film behavior.
- 4 gas cylinders were added to adjust inclination angle.

# CCS Measurement & High-Speed Images

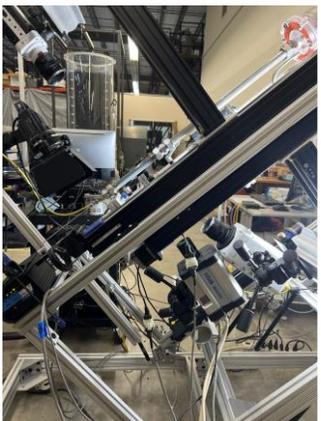
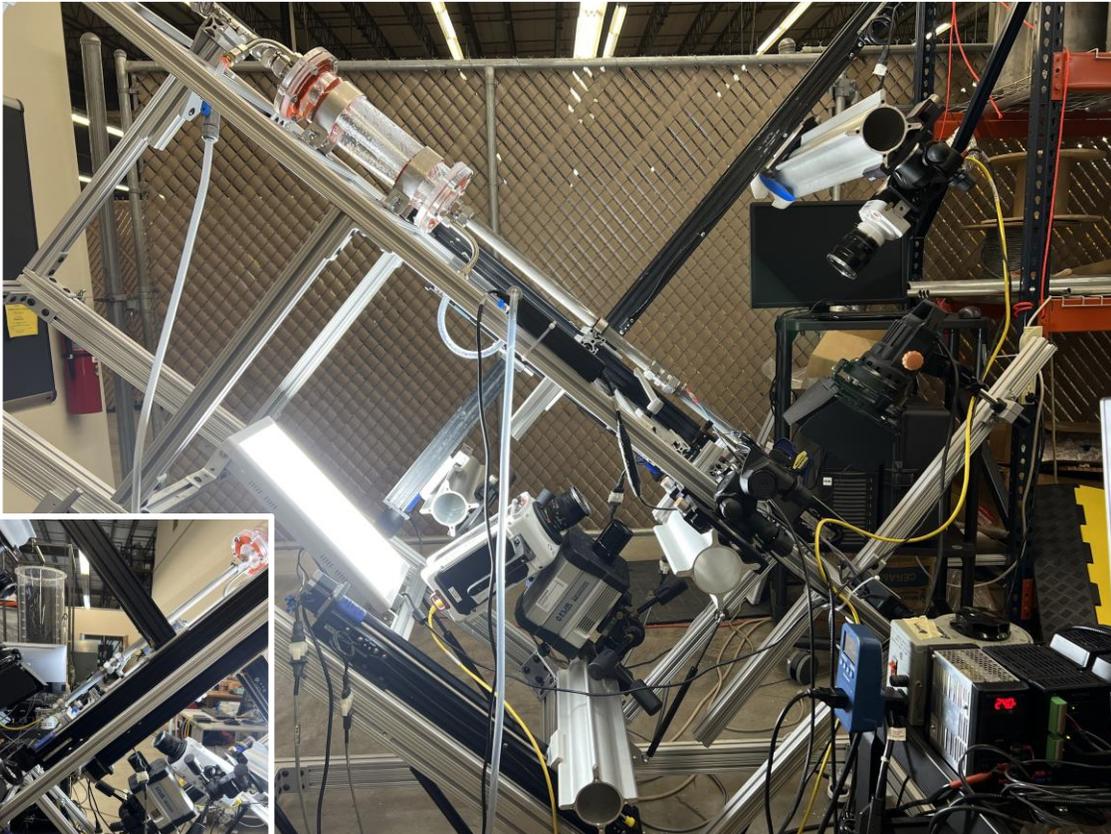


# Boiling Pattern Inside Heat Pipe – Half Wick Exp

Top view of the half wick heat pipe



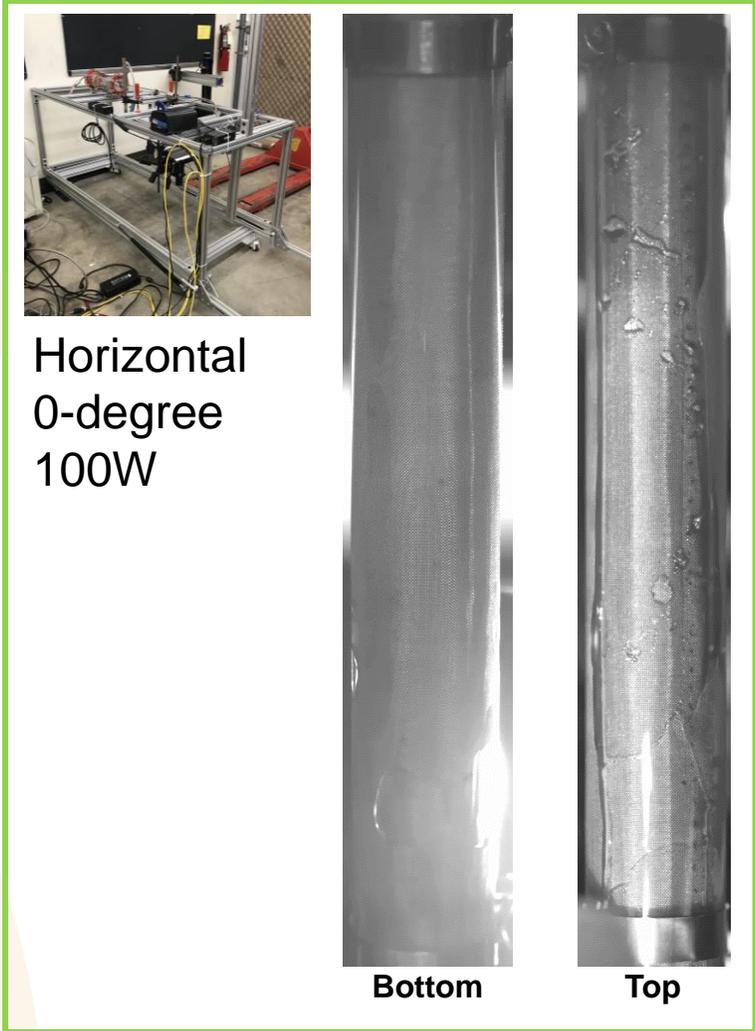
# Heat Pipe Visualization with Inclination Angle



- Visualization of the heat pipe with different inclination angle.
- Temperature measurement using fiber optical sensor and IR camera is implemented.
- Two high-speed camera was set (bottom side and top side)



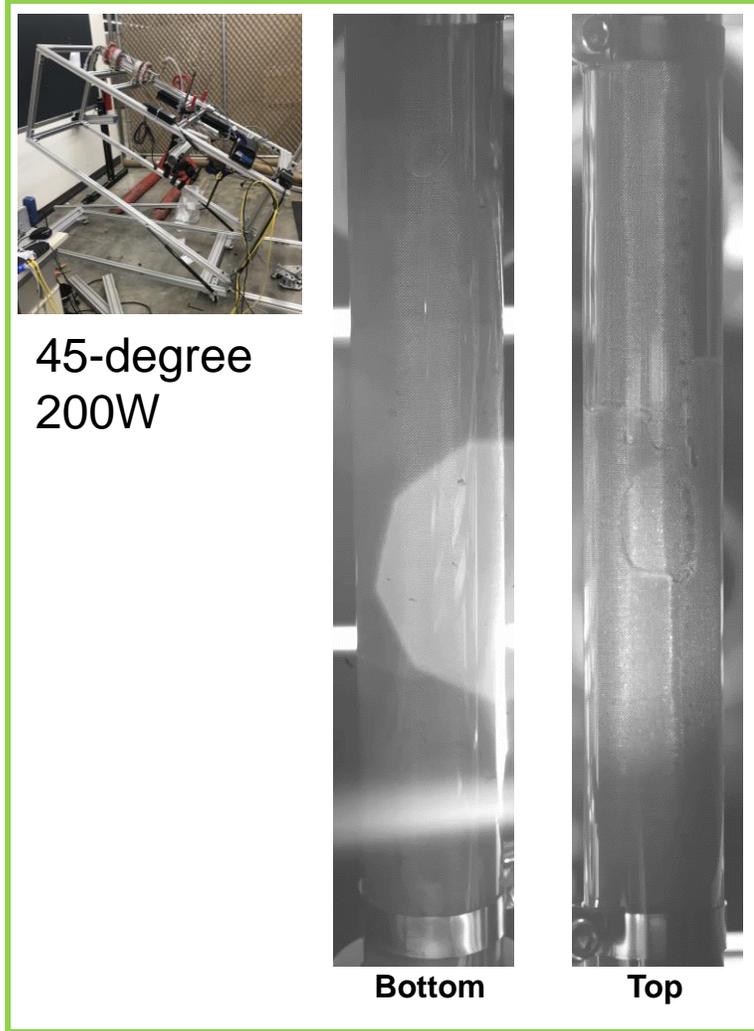
# Heat Pipe Visualization Results



Horizontal  
0-degree  
100W

Bottom Top

This panel shows a horizontal heat pipe at 0 degrees with 100W of power. It includes a small inset photo of the experimental setup on a metal table. The main image consists of two vertical views: 'Bottom' and 'Top'. The 'Bottom' view shows a dark, uniform cylindrical surface. The 'Top' view shows a lighter, textured surface with several small, irregular white patches, likely representing condensation or a specific internal structure.



45-degree  
200W

Bottom Top

This panel shows a heat pipe at a 45-degree angle with 200W of power. It includes a small inset photo of the experimental setup. The main image consists of two vertical views: 'Bottom' and 'Top'. The 'Bottom' view shows a dark cylindrical surface with a large, bright, irregular white patch. The 'Top' view shows a lighter, textured surface with several small, irregular white patches.

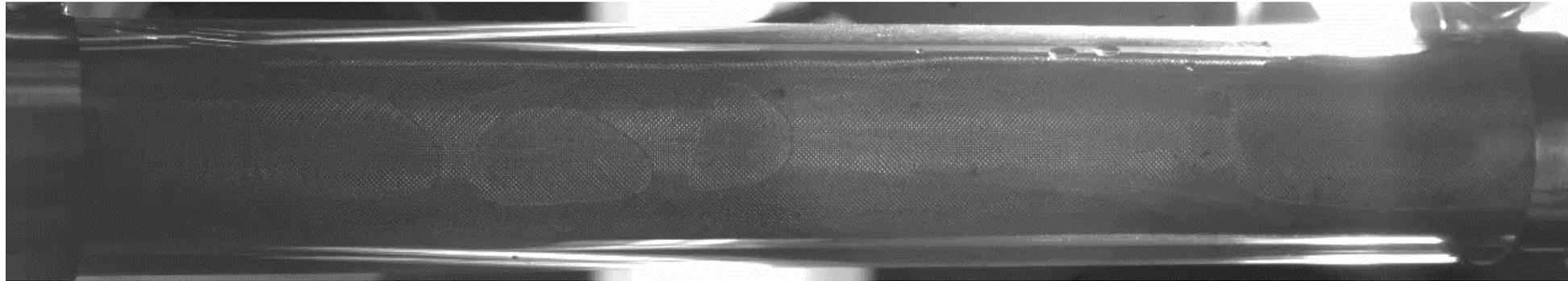


Vertical  
90-degree  
200W

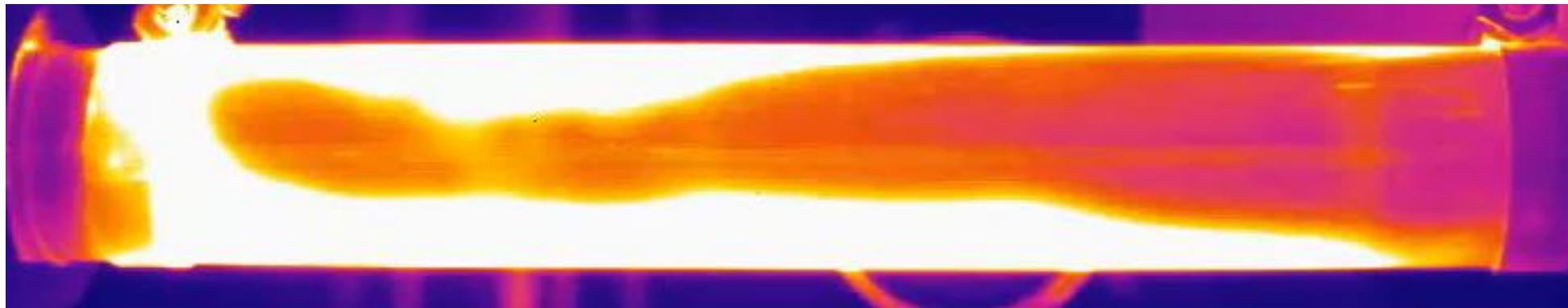
Bottom Top

This panel shows a vertical heat pipe at 90 degrees with 200W of power. It includes a small inset photo of the experimental setup. The main image consists of two vertical views: 'Bottom' and 'Top'. The 'Bottom' view shows a dark cylindrical surface with a large, bright, irregular white patch. The 'Top' view shows a lighter, textured surface with several small, irregular white patches.

# Heat Pipe Visualization Results - Limitation



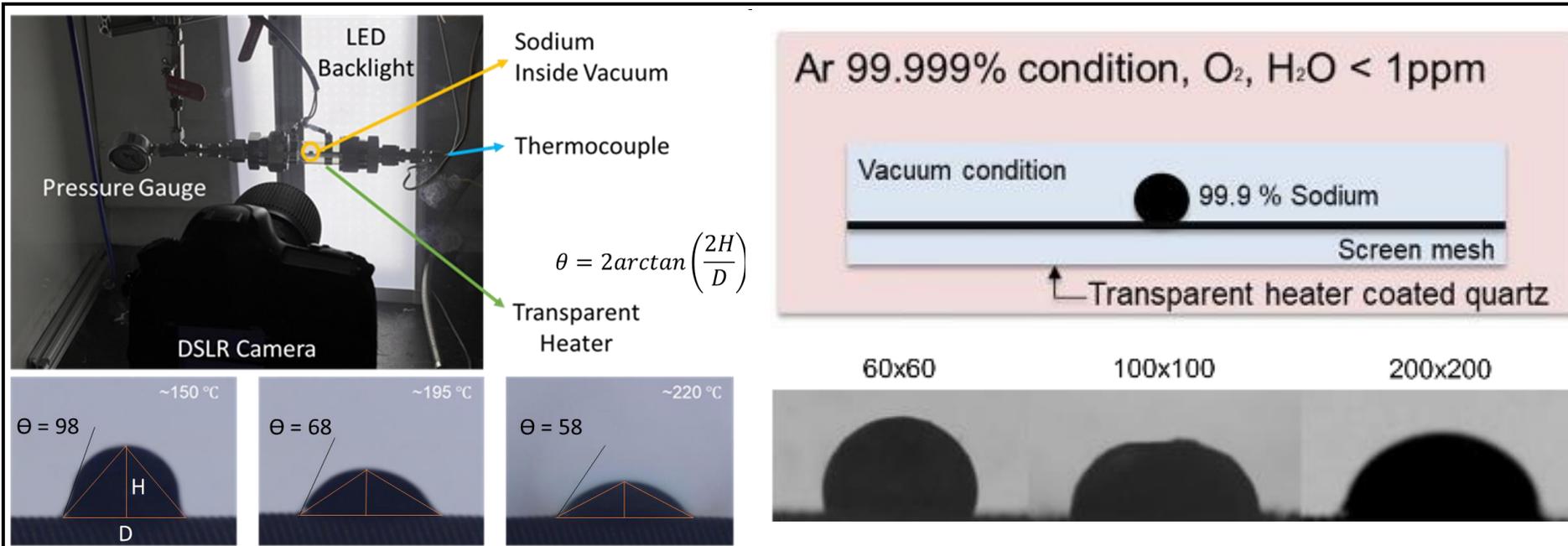
High-speed camera



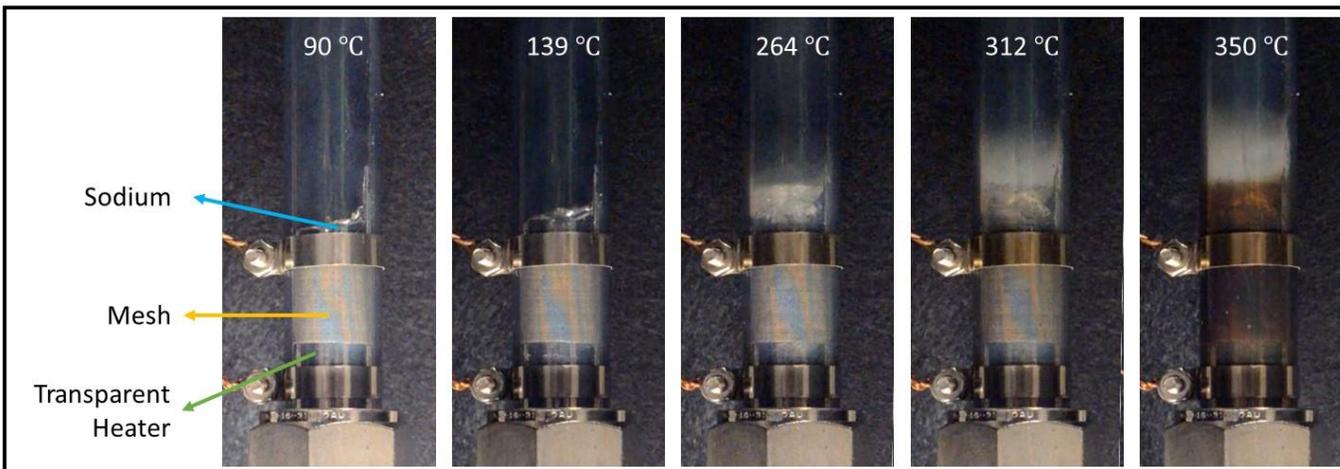
IR camera

200W, 0-degree inclination, rapid start-up

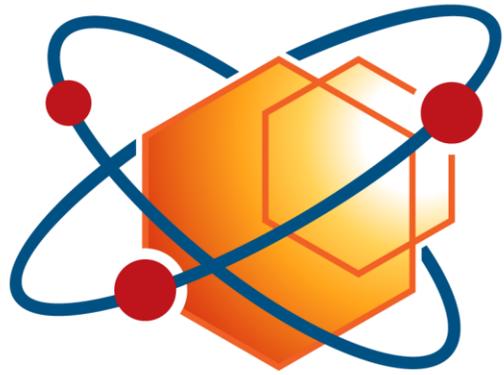
# In Progress – Moving on to the Liquid Metal



The contact angle measurement of the liquid sodium with different material (stainless steel plate and meshes) is being conducted in TAMU.



Visualization of melting/boiling of the sodium in a vacuum condition is under the progress.



**MRP** Microreactor  
Program